RADIO-ELECTRONIC ENGINEERING EDITION

RADIO & TELEVISION NEWS

FEBRUARY 1953

IN THIS ISSUE

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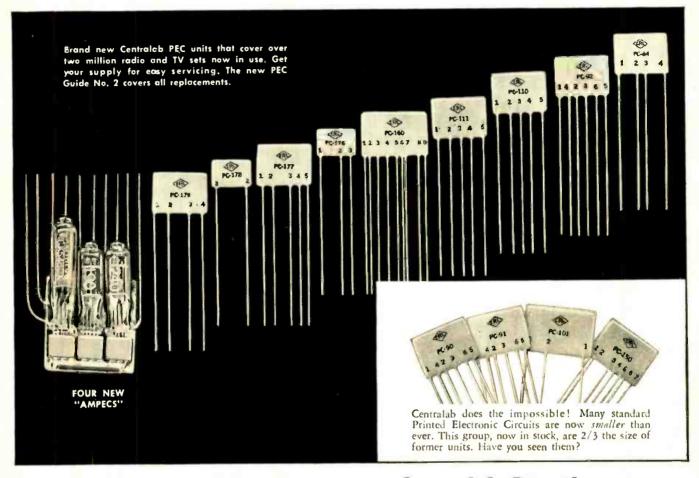








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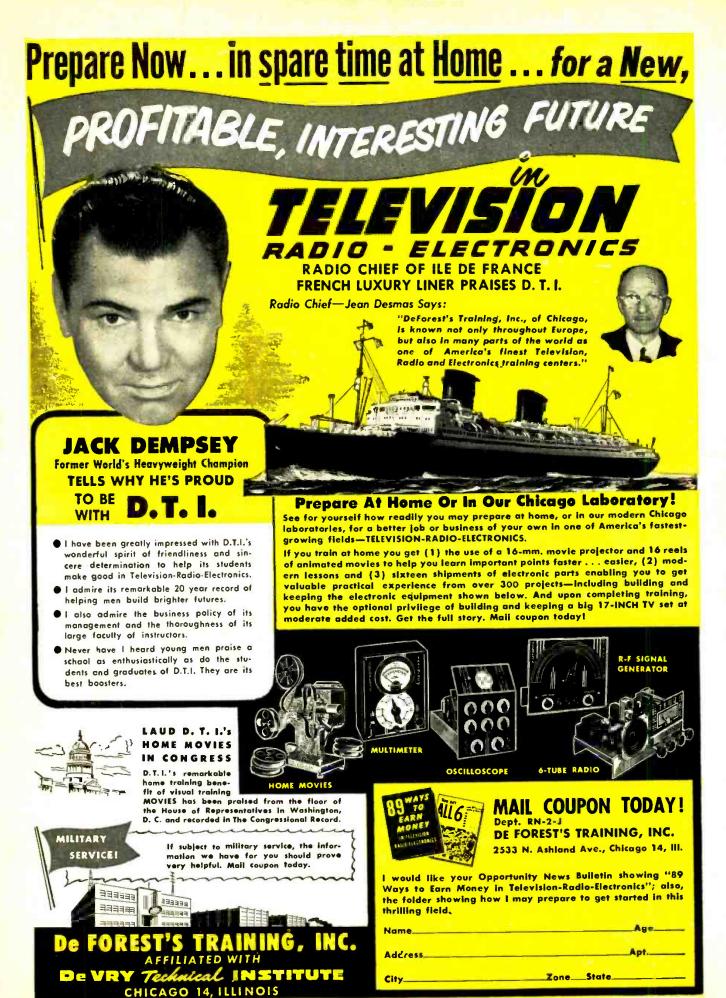
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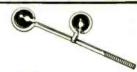
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THE TELEVISION SERVICE OPERATOR

MANY letters coming to our desk are from technical trainees attending classes in our trade schools and colleges. These students, generally, state that they are learning radio or television theory and practice as preparation for a career in the servicing business. Typical questions asked include: "What do I need to start a service shop?", "Should I specialize in television service exclusively or should I consider both radio and television?" and "What test equipment will I need for television servicing?"

It is a well established fact that television installation and service requires considerably more test instruments and other equipment than does radio. Such equipment can be very costly and, in the case of the independent service technician, almost prohibitive in areas of limited clientele. TV test equipment must be sensitive and accurate. In many cases it is too massive or heavy for home servicing and belongs on the test bench where it can be conveniently and effectively used. A well-equipped shop is a prerequisite for television servicing.

The service shop, however well equipped, is but one link in the chain of equipment required by the progressive service operator. Successful TV service contractors have learned that to cope with the many problems that arise in TV areas they must not only have a well trained staff of technicians but that their men must be properly equipped with the tools of the trade.

Paul Forte of the Television Contractors Association recently named several important components that are required to render good service. They include a panel truck or specially fitted car. In it must be carried a supply of tools, equipment, and spare parts that are in most common need. When a television set can't be repaired with these facilities, the car or truck must be suited so that a chassis and/or cabinet can be brought back to the shop for bench work. Such vehicles cost money and represent another investment on the part of the service contractor.

Since there are, roughly, about eighty different makes of television sets and thousands of models, the effectively operating contractor must have a complete library of diagrams, schematics, and service notes. These cost money, and taking care of them, adding to them, and using them costs time and money. Without them no man can claim that he is ready to service television.

A service operator cannot properly

function unless he has records of all service calls. These are not things he keeps in his wallet. He's got to have files and forms and he's got to have somebody work on them to keep them up-to-date. That means he has to have an office and someone in it to handle service requests and dispatch them promptly. These things cost money, a cost that can't be borne by the independent technician. If he does bear them, then he isn't an independent technician any longer; he's either a contractor or a service operator.

He must have special equipment and facilities for installations which include the erection of antennas. This, definitely, requires a truck. He can contract the antenna installation to someone else but that is hardly a good method of conducting a business. Trucks, too, cost money and are an integral part of the investment that must be put into a television service operation, as well as into the cost of service.

Since he's dealing with expensive television equipment in the customer's home, he has to carry Public Liability and Property Damage Insurance. He has to carry other insurance on his vehicles, test equipment, parts stock, and other facilities. It costs more money! It's all part of the investment that goes into a properly handled service business.

If the so-called independent technician says he doesn't need these things in order to maintain himself in the television service business, he is kidding himself. Certainly he won't kid the public, upon whom he depends for business.

There is little time, if any, for the aggressive technician to relax and sit back with a hope that he can keep pace with the fastest growing industry in our time. Instead, he must constantly keep abreast of new developments, in addition to performing his routine tasks as each day passes. He must continually study new circuits, new products, new applications, and new techniques.

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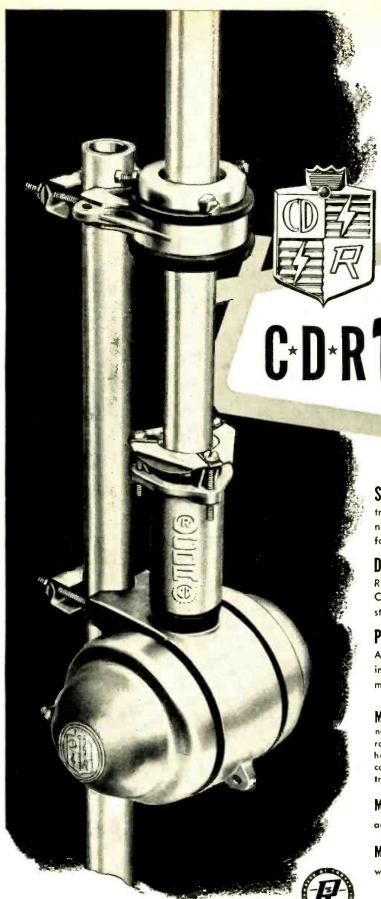
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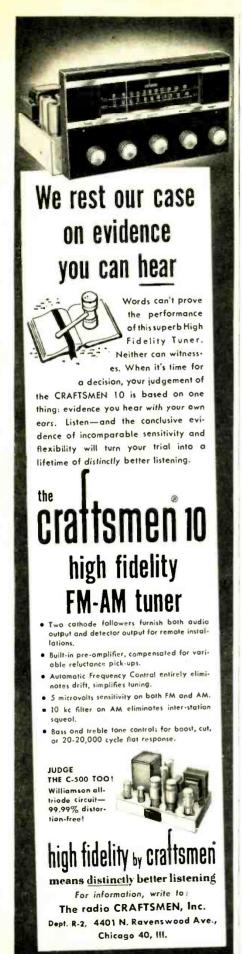
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* Presenting latest information on the Radio Industry.

By RADIO & TELEVISION NEWS' WASHINGTON EDITOR

THE PROJECTED TV SPAN across the nation, with stations in practically all of the states, often enthusiastically described by many in Washington and industry, seemed to be well on its way to becoming a firm reality, as the closing days of '52 appeared. With nearly 140 grants already issued to new TV operators in four-fifths of the states, and sincere promises from the Commission that hundreds more in all states would soon receive building permits, the prospects for the robust growth of TV looked bright indeed to everyone.

Whereas, only a few months ago, a few states seemed to be favored in the allocation race, nearly all were now receiving a share of the rich prize. The interesting expansion is illustrated in the partial listing of grants issued, at this writing, in the table on page 70.

In studying the table it will be noted that some existing TV areas, with v.h.f. stations, have received new stations which will be operated on the higher bands. One such market is Philadelphia, which now has three stations, and will soon have a u.h.f. station operated by WIP on Channel 29. Other cities in the new and old role are Greensboro, North Carolina and Johnstown. Pennsylvania. Here, Channels 57 and 56. respectively, will compete with the present very-high installations. The Channel 29 grant to the "City of Brotherly Love" was the first u.h.f. authorization to a major metropolitan center and represented an important trend in approvals from the processing staff. It had been felt that grants of this type would be delayed and perhaps not issued until '53. The earlier issuance was described as a major change in philosophy toward large city high-low band operation which would serve to spark sales of TV sets in areas believed riding close to a saturation point among viewers. In Philadelphia, dealers and distributors beamed when the high channel announcement appeared in the local papers. Notwithstanding the fact that the new station will not be placed in operation for some time, interest soared and sales jumped.

THEATER TV, which had a very brief airing during the late winter months of '52, became steeped in gloom as the official hearings began in '53. Many in

the theater industry felt very doubtful about the ultimate success of allocations of channels for theater circuits

According to the general counsel for motion picture exhibitors, the Commission has shown little enthusiasm for the assignment of channels to the theater. He indicated that most of the questions asked by the Commission during the hearing seemed to indicate that the legislators were not too keen about the proposed system. It was hoped, he said, that the facts presented during the lengthier hearings will convince the Commission that the theaters should have the requested channels, and as soon as possible.

THE ROARING DEBATE in the hearing offices of the Commission concerning the merger of ABC and Paramount, which it was generally felt would taper off with the release of Hearing Examiner Leo Resnick's approval of the merger. flared up with the objections filed by the broadcast bureau of the Commission.

The Resnick report was an extremely interesting document, covering every phase of the case and revealing some intriguing data on Paramount's role in the television industry. It was noted that the motion picture producer began to study the possibilities of TV as early as 1937, when it invested in Du Mont. They then applied for experimental television licenses in both Los Angeles and Chicago from which developed the present stations KTLA and WBKB. The transmitters for these stations were said to be among the first built, and the antenna and transmitter at Mount Wilson near Los Angeles was noted as being the first to be established at that focal point.

The report also indicated that the flicker maker has been instrumental in the development of video recording and large-screen TV, too. They have developed a camera and projector which can record TV images almost instantaneously, after they are received, on film said to be suitable for almost immediate projection on large screens used in theaters. In addition to these activities in TV, it was said, the company has become interested in color TV, through participation in the company formed by Dr.



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the speaker, with no messy confusion of wires, in the living room. No accessories connect directly to the remote control. All inputs connect only to the main amplifier. The savings in cabinetry and of installation labor are obvious and very real to those who take advantage of this new complete remote control design.

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Write for Catalog

Ernest Lawrence, who has developed a simplified tri-color tube, which will soon be demonstrated in New York again; the original model was shown a vear ago. According to Resnick. Paramount has invested well over a half-million dollars in this color tube, and \$300,000 in another TV development, a subscription system, which employs a coin box to unscramble scrambled pictures as they are received over a wire or otherwise.

As this column is being prepared, the merger issue is still deadlocked and appears to be a long way from settlement.

LONG DISTANCE overseas transmission is not only a project of our Voice of America, but many European countries, too. In Belgium, two 100-kilowatt transmitters are used for French and Flemish transmissions.

Several types of antennas are used; curtains directed toward the Belgian Congo and rhombics also directed to this zone and to this country, too. A reversible rhombic is also used to beam signals to Scandinavia.

TV is attracting the attention of many new European countries, reports from the continent indicate. In Norway, a substantial sum of money has been appropriated for experimental tests on a 7-megacycle and 625-line system. It is expected that the tests will last about two years.

Extensive tests are also being conducted in Spain over the Chamartin de la Rosa station. Under consideration are the erection of TV stations at Barcelona and Bilbao.

France will expand its TV activities, and by 1958 will probably have a nationwide service featuring their 819line system.

A NOVEL LISTENING plan is in use in Northern Rhodesia, according to EBU. About ninety community receivers are hooked up for group listening in the Lusaka area.

In the early summer of '52 a 15kilowatt short-wave transmitter was placed in service in Rhodesia. In addition, a mobile recording unit was sent out and covered over sixteen-thousand miles, making over 1300 discs of tribal choirs and other native music.

Community listening has also been reported to be very popular in Ceylon. By the end of September of 1950, 825 receivers had been installed at different community centers, rural development society offices, preaching halls, schools, temples, cooperative stores,

Community broadcasting has also been used in Bombay, Madras, and Delhi. Today there are over 4000 receivers in operation all over the country.

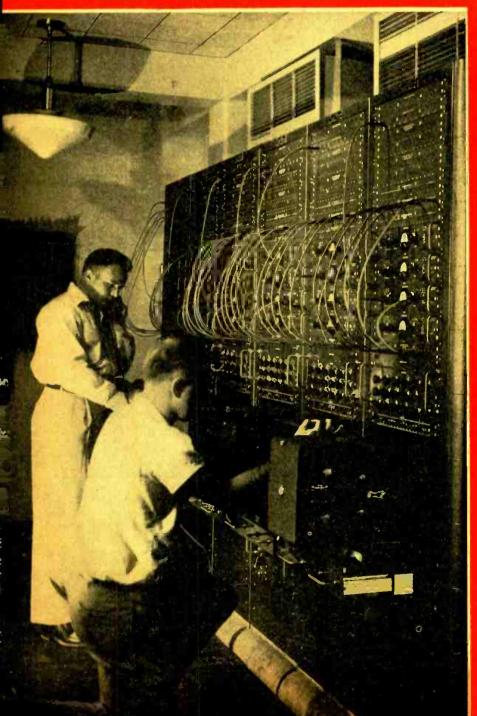
Most receivers are operated from batteries and thus maintenance is a problem. To provide battery power, a network of battery-charging centers is used. In Madras, there are 67 such

(Continued on page 147)

RADIO & TELEVISION NEWS



TELEVISION • RADAR • ELECTRONICS • RESEARCH • COMMUNICATIONS • MICROWAVES



FEBRUARY, 1953

GUIDED MISSILE DATA RECORDING

A THERMOCOUPLE A.F. WATTMETER

ULTRASONIC MICROSCOPE

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Edited by H. S. RENNE and the Radio & Television News Staff

Technicions making final escillograph calibration adjustments on guided missile data recording equipment at Patrick Air Force Missile Test Centes. Mr. J. Wynn. Jr., co-author of article on P. 3, is at left.

www.americanradiohistory.com



HQA, HQC, HQD CASE 1 13/16"Dia. x 1 3/16"High



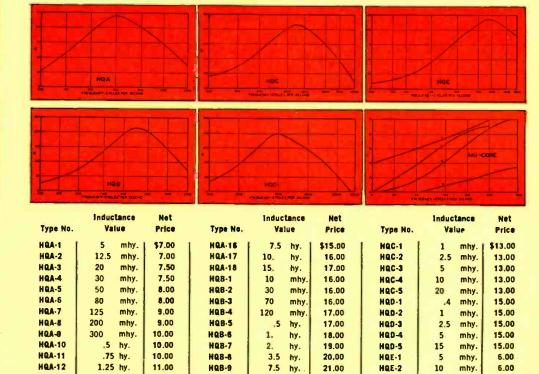
HQB CASE 1 5/8"x 2 5/8"x 2 1/2"High



HQE CASE 1/2"x 1 5/16"x 1 3/16"High

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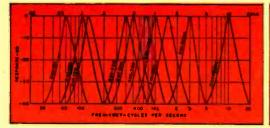
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HQB-11

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BM1-750	HMI-1000	LMI-5000	LML-2500
BMI-1000	HMI-3000	LMI-10000	LML-4000
			1 ML-12000



GUIDED MISSILE DATA RECORDING

JAMES B. WYNN, JR.*
and
SAM L. ACKERMAN**

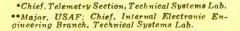
Air Force Missile Test Center Patrick Air Force Base

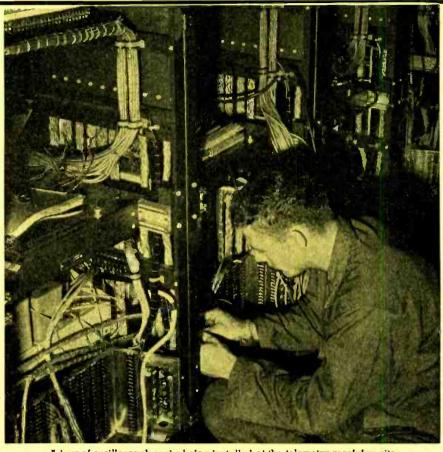
HOSE in nearly every craft or profession have at one time or another had the occasion to record data. In the fields of electricity and electronics, perhaps the furthest advances have been made in precision data indicating and recording of scientific phenomena. The recording oscillographs, utilizing galvanometer elements, provide an ideal means for observing and recording static and dynamic data, and will be the main subject of this article. Auxiliary or accessory equipment recently developed to provide flexibility and standardization of installation and operating techniques at one of the advanced missile radio telemetry stations at the Air Force Missile Test Center, Patrick Air Force Base, Florida, will be discussed in detail.

The Recording Oscillograph

For those not familiar with this type of recorder, it may be well to describe in some detail the fundamental aspects of this instrument. No doubt the oscillograph which would normally come first to mind would be a conventional electronic unit with a scope tube on the front, similar to the common TV set, and with a camera focused on the oscilloscope tube. However, as mentioned before, the equipment to be discussed uses a galvanometer as the active indicating element. The recording oscillograph is really quite simple -it is composed of a light source, a mirror moved by a sensitive meter movement to reflect the light, and a photosensitive medium to record the reflected light beam.

A review of the recording galvanometer oscillograph manufacturers listed in business guides indicates that this is a multi-million dollar enterprise. However, only a few of the available manufacturers produce recorders satisfactory for extensive use, and for precise measurements in the field of missile or aircraft testing. Most of the reasons for this will become self-evident, and a survey will show that





A bay of oscillograph racks being installed at the telemetry receiving site.

Photographic oscillographs are widely used to record data obtained from telemetering systems.

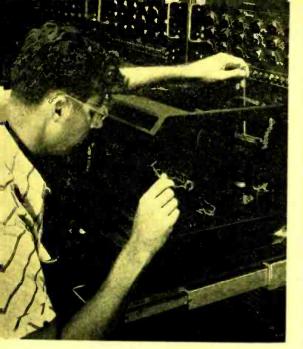
some of the mechanical and electrical characteristics of a few far surpass the others.

The Galvanometer

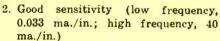
The galvanometer element, which on occasion may have been presented too mysteriously, is in reality a d'Arsonval meter movement without any pointer; a small mirror replaces the pointer. The movement of a current-carrying wire in a magnetic field is one of the basic concepts of electromagnetic theory and this principle is utilized in converting the electrical energy into mechanical energy in the galvanometer. Degree of force or motion produced is mostly dependent upon the flow of electrons, the number of turns of the conductor, and the strength of the magnetic field. Thus, with the present design, a compact element exists which very conveniently converts the flow of electrons to the proportional movement of a mirror. The moving beam of light reflected from the mirror is then projected on a ground glass screen for viewing, calibration and setup purposes, and is simultaneously projected onto photographic material to preserve the data permanently.

Main components required to make up the galvanometer are: a coil of wire, a suspension for positioning the coil of wire, a mirror, and a case or shell. Of course, the galvanometer must be positioned in a magnetic field for operation, but this magnet is separate and external for operational reasons. A photo-optical system is used in conjunction with the mirror since it provides the means for producing a record without extracting any appreciable energy from the galvanometer. Characteristics of the galvanometers in general use conform to the following:

1. Small size (approximate dimensions: \(\frac{1}{6}'' \) to \(\frac{3}{16}'' \) by \(\frac{2}{16}'' \) to \(2\frac{1}{6}'' \))



A technician is adjusting the position of a galvanometer in the oscillograph.

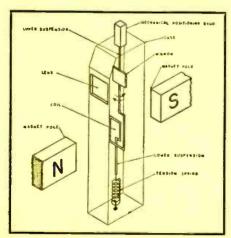


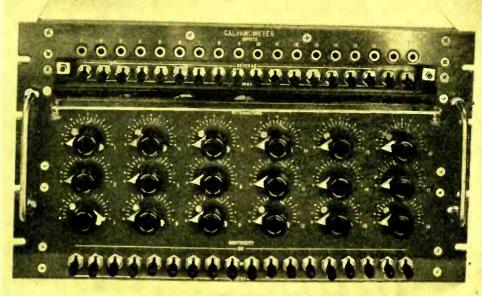
- 3. Wide frequency response (0-2000 cps)
- 4. Rugged construction (suitable for field, mobile or airborne installations)
- 5. Accuracy (1%)
- 6. Replaceability (electrically and mechanically interchangeable)
- 7. Cost (\$100 to \$150 each)

Damping

The suspension of the galvanometer is a free moving element, so that its action under forced vibration follows all the theory and formulas pertaining to such motion. Of primary concern to the user is the motion of the element when a signal is applied. The mass of the movement and its inertia will distort the motion of the recorded output in relation to the input if rapid changes occur. Thus, the damping

Pictorial cutaway illustration of a typical D'Arsonval galvanometer element.





Front view of galvamometer panel, showing function controls as well as polarity switches which are recessed and normally protected by the hinged cover plate.

characteristics of the element as associated with its circuitry should be understood.

Basically, two fundamental damping mediums are used: (1) fluid damping, i.e., the suspension rotates within a viscous fluid, and (2) electromagnetic damping, which utilizes the back emf generated by the coil moving in a magnetic field. Actually, any galvanometer has additional damping effects produced by both mediums since the air in which an electromagnetically damped galvanometer moves produces some of the fluid damping effects, and the source impedance of a fluid damped galvanometer furnishes electromagnetic damping. The total damping is the arithmetical sum of all the per-unit dampings of the particular system.

Damping is used mainly to control the frequency response but it also introduces a phase shift (very slight), protects the galvanometer from violent overswings, and controls the time required to respond to sudden changes in current.

Normally, 0.64 per-unit damping or 64% of critical damping is used since it produces maximum frequency range with minimum inherent error. Unfortunately, many users procure galvanometers and standard shunts without realizing that circuitry associated with the galvanometer may at times seriously alter the damping characteristics.

Frequency Response

Whether electromagnetic or fluid damping should be used is mainly determined by the frequency response required and the driving current available. The electromagnetic type is generally more desirable since it normally has higher sensitivity and a far lower temperature coefficient. With the pres-

ent manufacturing techniques, it can be shown by the following basic formula that the limiting factor for electromagnetic galvanometers is the frequency response:

$$R = K/F$$

where R is the shunt resistance in ohms, K a constant of construction and installation, and F the frequency.

From the above, it is easy to understand how the shunt resistance R becomes lower in value as the frequency F is increased. Table 1 has been prepared from values in one of the instruction manuals furnished with a commercial recording oscillograph. Actually, the shunt resistance will never become zero but its value will become less than the internal resistance of the galvanometer and its low sensitivity will render it useless, fluid damping then being necessary.

The present oscillographs utilize a magnetic block to provide proper flux density for all the galvanometers in the instrument. Thirty-six galvanometer element installations are common in blocks of about four or five inches long. The frequency response range, linear \pm 5% at 64% of critical damping, of commercially available galvanometers is from 0-2000 cps. Greater sensitivity is obtainable by selecting elements—whenever possible—that have a flat re-

Table 1. Relationship between response, the shunt resistance, and sensitivity.

Frequency Response (cps)	Shunt Resistance (ohms)	Sensitivity (ma/In.)
0- 60	350	0.033
0-100	180	0.035
0-180	83	0.040

sponse range limited to the intelligence frequency to be investigated. By considering the theory of galvanometer operation, it is easy to realize that since the flux density is a constant, more force will be produced by a constant current if the number of turns is increased. Unfortunately, more turns increase the mass, so the natural frequency is low. Conversely then, reducing the number of turns will increase the natural frequency but reduce the force or degree of rotation of the mirror.

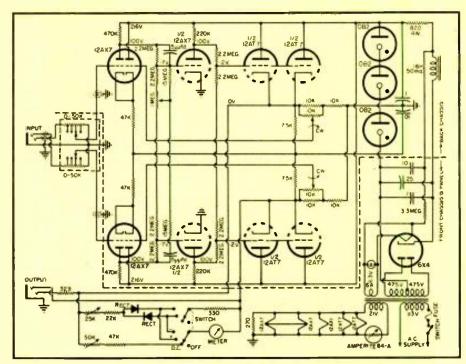
Data received at telemetry stations is generally stored on magnetic tape, which is played back after the test has been completed, and is recorded directly on a recorder which produces a visual and permanent record. In the oscillograph recorder, the photosensitive paper travels at a constant speed while an accurate time base is recorded, and the information is presented as a trace deflection proportional to the intelligence data. The usefulness of the record is threefold-an experienced engineer can view a record after a flight and, reading it as a graph, estimate performance; he can read data accurately by tabulating each period of time required; or if the data are to be fed from magnetic storage into electronic computers, he can determine which portions are worth while tabulating or printing and at what rate it should be accomplished.

Applications

Utilization of recording oscillographs to record data in telemetry installations at the guided missile test ranges has become a necessity. Merely to place them on benches or tables is most inefficient and not in keeping with the present "state of the art." If varying work loads exist whereby "setup conditions" have to be changed occasionally, the work becomes very difficult and discouraging. In fact, where lack of standardization is apparent, so much individualism creeps in that set procedures cannot be adhered to. The result is eventually disastrous. Sooner or later, while under pressure or while training new personnel on the job, the time will come when the signals supposedly connected to the instrument will be missing from the record.

The early oscillographs were developed to enable seismograph recordings to be made in geophysical exploration, and they still find wide application in that field. In these early models, small pickups would indicate amplitude and the recorder itself would apply a time base so that small exploding charges could be set off to indicate terrain configuration.

Radio telemetry is one of the prime users of oscillographs today, and has



Circuit diagram and parts values for the galvanometer amplifier.

fostered or made practical many of the improvements on oscillographs which have been adapted in the past few years. Recording oscillographs are in use in the majority of telemetry systems as one of the means of recording data, and they will be found on most of the missile test ranges. Some of the ranges employ 20 to 40 such instruments.

The recording oscillograph, when used by itself, can be operated on a laboratory bench or table. While the instrument is only 12-14" high, 10-12" wide and 18-24" deep, it requires a considerable amount of free space for cabling, galvanometer adjustment, changing drive speed, magazine loading and operational viewing. In fact, every side must be accessible except the bottom and the back. Unfortunately, to provide accessibility, many instrumentation installations merely space them wide apart in rows on tables. Thus, all the engineering planning of the installation is lost somewhere in a maze of cabling that resembles a conglomeration of short-circuited onearmed bandits. The small oscillograph now requires a floor area of about nine square feet.

Oscillograph Racks

Because of experiences gained from the other missile test ranges, the engineers in the AFMTC's Technical Systems Laboratory felt that it was necessary to develop and fabricate oscillograph recording racks for installations of elaborate telemetry facilities, and furthermore, that centralized recording techniques should be employed. The final AFMTC design provided for all

information from as many as three 16-channel or six 8-channel FM/FM telemetry systems to be available for "set up" at each oscillograph.

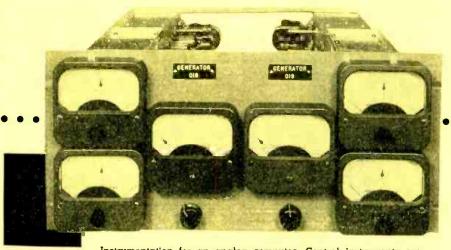
Each oscillograph rack is complete in itself. Separate panels are provided for each group of data outputs from the telemetry stations. This permits easy expansion or adaptability to other types of instrumentation for standardization. The basic design parameters were to provide proper installation and

(Continued on page 28)

Typical oscillograph record with trace lines and timing markers identified.



A THERMOCOUPLE A.F. WATTMETER*



J. D. RYDER and M. S. McVAY University of Illinois



Instrumentation for an analog computer. Central instruments are electronic voltmeters and outer vertical pairs are wattmeters.

By using electronic amplification, many disadvantages of the thermocouple for measuring power are overcome.

UDIO-FREQUENCY power measurements have usually been made by dissipation of the power in a known resistive load, since few audiofrequency wattmeters have been available. Numerous proposals appear in the literature covering low-burden electronic instruments which usually employ some form of square-law circuit, as in Fig. 1, but practical forms of the instrument have rarely appeared.

Usual Theory

It can be seen that the input to diode (or triode) V1 in Fig. 1 is:

$$e_1 = e - iR_1$$
 (1)
and the input to diode V_2 is:

$$e_1 = e + iR_2$$
 (2) where e is the instantaneous value of voltage applied to the load, and i is the instantaneous value of current flowing to the load. Resistors R_2 are assumed small and equal.

In the usual manner, if the diodes

Fig. 1. Basic form of the square-law

circuit used for power measurement.

have identical volt-ampere curves given by:

$$i = a_0 + a_1 e + a_2 e^2$$
 . . . (3) then the anode current of V_1 is:

The anode current i_2 of V_2 differs only in that the two negative signs become

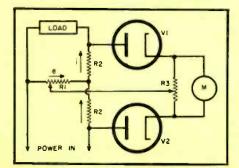
The output or load circuit is acted upon by the difference of currents i, and i, and it is apparent that all positive terms appearing in both equations will cancel, leaving only a result equal to twice that of the negative terms in (4). Thus:

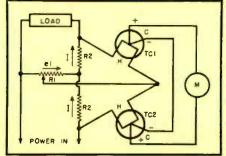
$$i_{out} = i_s - i_1 = 2a_1iR_1 + 4a_2eiR_1$$
 (5)

If the applied electromotive force is sinusoidal, or $e = E_1 \sin \omega t$ and i =I sin $(\omega t + \theta)$, where θ is the power factor angle of the load, then the output current is:

$$i_{out} = 2\alpha_1 I R_2 \sin (\omega t + \theta) + 4\alpha_2 E_1 I R_2 \sin (\omega t) \sin (\omega t + \theta). (6)$$

Fig. 2. Schematic diagram showing basic principles of thermal converter.





If $IR_2 = E_2$, the above becomes by ex-

$$i_{out} = 2a_1 IR_2 (\cos \theta \sin \omega t + \sin \theta \cos \omega t) + 2a_2 E_1 IR_2 (\sin \theta \sin 2\omega t)$$

If this difference current is applied to a d.c. or average reading instrument M, only the last term of (7) will deflect the meter, since the first two terms represent a.c. currents. These may be bypassed around M by a suitable capacitor.

If $IR_2 = E_2$, then the instrument M is deflected by a d.c. current of value: which is proportional to the average load power, angle θ being the load power factor angle. Thus meter M becomes an indicator of average load power.

Reasons for Dissatisfaction

Certain assumptions have been made in reaching the above results, and these are:

- (a) The two tubes have identical voltampere curves, or pass identical currents for all values of applied voltage.
- (b) The matching of (a) exists throughout the life of the tubes. and for all values of heater voltage.
- (c) The tube volt-ampere curve is accurately expressed by (3), and no higher power terms are present.

In practice, it has been impossible to find or to maintain tubes or crystals meeting these assumptions, such that power measurement accuracies of better than 5% can be achieved without severely restricting the load current or voltage to a very small range. Two tubes or two crystals may be matched to equal quiescent currents or values of a_0 , by adjustment of the tap on R_3 , but balanced currents will probably not be obtained at other applied voltages. This action, of course, indicates unequal values of a_1 and a_2 .

*This article is based on a paper presented in Chicago at the 1952 National Electronics Confer-ence, held Sept. 29, 30 and Oct. 1.

Controls may be added for additional individual adjustment, usually taking the form of resistors in the circuit. However, it should be noted that coefficient a_2 of (3) appears in the results of (7) and (8). Any additional resistance added to the circuit for adjustment purposes has the effect of linearizing the circuit, reducing the value of a_2 , and thus lowering the sensitivity of the circuit when used as a wattmeter.

Since three coefficients appear in the series (3), three independent adjustments are theoretically needed. These additional adjustments may be obtained by use of triodes or pentodes with grid bias controls, but the over-all result is not changed—to achieve and maintain a match of volt-ampere characteristics over an applied voltage range of possibly 50 to 1 is not a practical matter with commercial tubes.

Use of Thermocouples

It should be noted that the important property required of this circuit is its ability to square, or cross-multiply, the input voltages, since it is only the squared term of (3) which leads to the result of (7) or (8). Another electrical device that inherently employs this squaring property is the thermocouple, as its output is obtained from heat or i'R input to its heater.

Actually, the thermocouple has been employed for many years as a squaring device in a wattmeter, sometimes used in the electric utility industry. When so used, the device is known as a Lincoln "thermal converter" wherein a d.c. electromotive force is generated proportional to load watts, this d.c. electromotive force then being telemetered or transmitted over telephone lines to a distant point where the power is indicated or recorded.

The desired squaring property is present in the thermocouple together with certain disadvantages, such as limited overload capacity, slowness of response, low heater resistances, and thus rather large current inputs. By using electronic amplifiers and techniques in the thermal converter circuit, it is possible to overcome all of these disadvantages except the slowness of response. This can be controlled to some extent by the selection of very small thermocouples of low heat capacity, and an anticipating electrical circuit can be added if needed.

Thermal Converter

The principle of the thermal converter is illustrated in Fig. 2, from which it can be seen that this unit is fundamentally the same as the electronic unit of Fig. 1. Thermocouples are employed to square the respective sum and difference input voltages, and to subtract the outputs, leaving a net

current through the microammeter M which is proportional to power in the load circuit. In Fig. 2, H indicates heater connections, C the couple connections; vacuum-mounted thermocouples are preferred.

There is one objection to the use of the simple circuit of Fig. 2. Theory indicates that the circuit has maximum power sensitivity when voltages E_1 and E_{z} of (8) are equal. Since it is not usually desirable to make the series voltage drop of IR: equal to the line voltage E_1 because of excessive losses, some form of amplification of voltage $E_2 = IR_2$ is desirable. In order to reduce the loading effect of the wattmeter on the circuit to a minimum, an electronic amplifier is indicated. It should be pointed out, however, that the amplifier will only be required to be linear, all squaring or nonlinearity of characteristics being a function assigned to the thermocouples.

The Wattmeter Circuit

The circuit of the amplifier incorporated between the shunts and the two thermocouples is shown in Fig. 5. A 50:1 step-up transformer is used across the shunts, as this seemed an easy way to obtain isolation and a voltage increase. Shunt values are chosen to produce 20 millivolts at full-load current, and the line voltage is taken off the shunted potentiometer at a point providing one volt maximum. It is realized that the use of good transformers is necessary at this point if wide frequency response is to be obtained. However, if a poor transformer is used, its performance can be considerably improved by shunting the secondary with a loading resistor.

The first amplifier stage is conventional. The second stage employs two

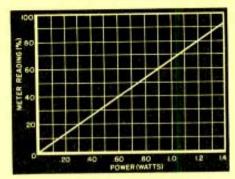


Fig. 3. Typical calibration curve.

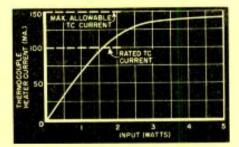
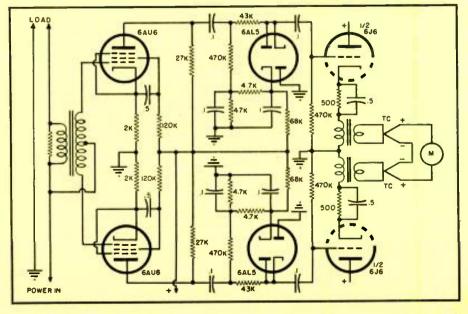


Fig. 4. Performance of vacuum tube limiters in preventing the thermocouples from burning out.

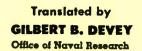
6J6 tubes, with halves paralleled, and with cathode-follower output. This form of output provides much wider frequency response from a given transformer than if the more usual plate output were used. In this case, the transformers are needed for matching the relatively low-resistance thermocouple heaters (2 ohms, 100 ma.) to the 6J6 tubes, and low-cost tube-to-voice coil transformers were found to be satisfactory.

It should be noted that this is not a push-pull amplifier since the two side channels are amplifying different signals $(e - iR_2 \text{ and } e + iR_2)$, and no cou
(Continued on page 20)

Fig. 5. Schematic diagram and parts values for the complete instrument.



ULTRASONIC MICROSCOPE*

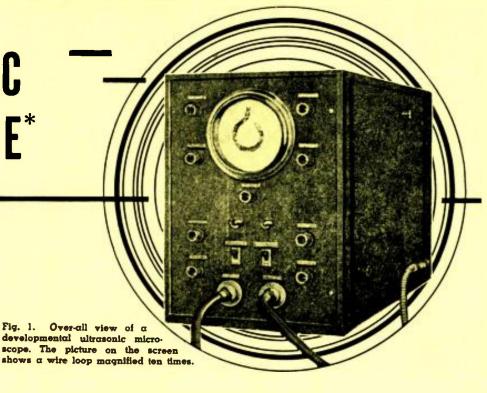


THE successful development of ultraacoustics and the obtaining of very
short ultrasonic waves, of the order
of the wavelength of visible light, has
led to the development of an ultrasonic
microscope with which it is possible to
view the picture of an object in magnified scale. Inasmuch as nearly all bodies
in nature are transparent to ultrasonic
waves, the ultrasonic microscope is expected to have a very wide field of application. Its principle of operation
may be found in the proposal of S. Y.
Sokolov in 1936 (U. S. patent 2,164,125,
issued June 27, 1939).

Operation of the ultrasonic microscope may be described as follows. A narrow beam of ultrasound is bunched (Fig. 2), and radiated by a piezoelectric quartz plate (1) to illuminate the object under examination (2). Reflections of the ultrasonic beam from the object fall on an acoustical collector lens (3), the focus of which is set for reception at (4), consisting of a piezoelectric (e.g., quartz) plate.

The reception plate is located at the base of the tube (8). The narrow beam of the cathode rays (7), inside the cathode ray tube, falls on the inner surface of the narrow plate and dislodges secondary electrons, which are then collected by the anode (9).

Under the action of the charge, the image on the inner surface of the narrow plate comes from the region of the ultrasound, and secondary electrons are emitted when the surface of the plate is made to undergo a change. This change of secondary emission results in greater current acting on the anode (9), the magnitude being increased by special amplifiers and passed to the modulator arrangement of the cathode of the tube (6). Then the intensification of the cathode beam in the tube (6) causes a fluctuation which conforms to the variation of secondary emission from the



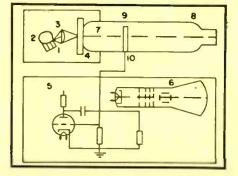
Ultrasonic waves have been successfully used as the source of illumination in a microscope.

surface (4). This is accomplished by the television method of synchronism of motion by lines and frames of the cathode beams of the tubes (6) and (8). The screen of the cathode tube (6) then shows the semblance of a picture as distributed by the electrical charge on the receiver plate (4).

Piezoelectric charges appear on the surface of the quartz plate at the same points where deformation has taken place. Therefore, a picture is distributed on the surface of the quartz plate in exact conformance to the ultrasonic field in the focal plane of the lens (3).

Inasmuch as the configuration of the ultrasonic field in the focal plane in its line of conformance portrays the object, this object is immediately seen on the screen of the tube (6). Transposition of the object understandingly gives the appearance of transference of its image to the screen.

Fig. 2. Diagram illustrating the principle of operation of the microscope.



Magnification of the image, given in the description of the system, is determined by the ratio of the linear dimensions of the cathode tubes (6) and (8). Calculations show that in the ultrasonic microscope magnification approaches the order of tens of thousands of times. The resolving capacity depends on the cross-sectional area of the cathode beam in the tube (8), parameters of the piezoelectric plate, and length of the ultrasonic waves.

Experiment shows that a frequency of 10° cycles can be obtained without particular difficulty and that there is a good possibility of obtaining a frequency of 10¹° cycles. In water, the length of ultrasonic waves at a frequency of 3 x 10° cycles is equal to 5 x 10⁻° cm., i.e., the wavelength of visible light. At that frequency, the resolving power of the ultrasonic microscope may reach an extreme, close to the resolving power of the optical microscope.

For capillary waves, the speed of diffusion is considerably less; and the wavelength accordingly is much smaller than the wavelength of visible light. Consequently, if the radiation type of capillary waves can be obtained at higher frequencies in the future, there will be an opportunity to increase the resolution capacity of the ultrasonic microscope by one or two orders to compare with the best optical microscope.

The objects under examination can be illuminated with a continuous ultrasonic beam as well as with single im-

^{*}Translated from an article entitled "The Ultrasonic Microscope" by S. Y. Sokolov which appeared in the Russian Journal "Progress in Physical Science," Vol. XL. Jan., 1950.

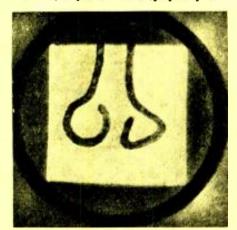
pulses. For amplification of the secondary emission, it is expedient for the inner surface of the receiving plate to be covered by a special layer which possesses great secondary emission.

The method of obtaining a visible picture may be altered, as shown in Fig. 3(A). Here, the piezoelectric quartz plate (1) serves as the base of the vacuum triode (2). An ultrasonic beam falls on the outer surface of the piezoelectric plate (1), the inner surface of which is covered by a photosensitive layer. Under the action of the ultraviolet beam (3), uniformly illuminating the inner surface of the plate, photoelectrons are emitted which-accelerated by the application of an electrical field-pass through the system of magnetic and electrical lenses (4) and fall on the fluorescent screen (5). On the screen, as in the usual electron microscope, only the image of the source of electrons may be seen-in this case, the image of the distribution of photoelectric emission from the surface of the piezoelectric plate (1). Distribution of photoemission on the surface of the plate is in precise conformance to the distribution of the piezoelectric charge, which reproduces the configuration of the ultrasonic field. On the screen (5), the image of the ultrasonic field can be seen; this is a repetition of the image of the object, established by the ultrasonic field, in conformance with the magnified scale.

The resolution capability in this case is dependent on the length of the ultrasonic wave, on the thickness and dielectric property used in the piezoelectric plate, and on the construction of the lens system. Ultraviolet radiation, illuminating the quartz plate, can be replaced by a homogeneous electron cluster.

Another version of the ultrasonic microscope is illustrated by Fig. 3(B). This, as in the preceding version, depicts the object received in magnified scale on the screen (5). However, in

Fig. 4 Utrasonic microscope image of metallic loop immersed in opaque liquid.



this scheme, the screen (5) consists of a thin plate on which a photosensitive mosaic layer is drawn, causing secondary electrons under the action of falling electrons to be collected on the annular anode (6). Electrons in the beam (7) fall on the screen (5) and, as in the usual television tube, move line and frame, equalizing in such a manner on the screen (5) as to form an image of the object by electrical potential. The change in secondary-electron emission is amplified and passed to the second tube, in which the cathode beam movement is synchronized with the cathode beam (7). In this case, the image of the object is received on the screen of the second tube.

It should be noted that the capabilities have to be determined not only from the facts mentioned above but also by additional factors of another kind, primarily by the complexity of the vibrations of the quartz plate which is excited by different types of ultrasonic beams: the action of these beams induce not merely longitudinal waves but also transverse and surface waves, which will distort the image. Use of the quartz plate is accomplished by special cuts and choice of the proper method of strengthening (border conditions), which may be diametrical, and the surface waves in the quartz plate are greatly attenuated to increase the clearness of the picture. Applications for the ultrasonic microscope evidently are diversified enough and have sufficient possibilities to warrant rapid growth in this field.

Now to the description of the experimental performance of the ultrasonic microscope in scientific laboratories:

In Fig. 4, a metallic object is shown immersed in an opaque liquid (magnified ten times).

Figure 5 illustrates a glass rod and glass tube of equal dimensions. In the rod, the clear space shows ultrasonic waves partially suppressed. The tube displays uniform illumination, as the

Fig. 5. Image of glass rod (left) and tube (right) in a homogeneous field.



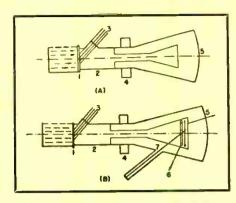


Fig. 3. Two alternate versions of the ultrasonic microscope. (A) Image is formed by acceleration of secondary electrons from treated surface of quartz plate 1, (B) Image is formed by electron beam 7 which scans element 8.

ultrasonic ray does not pass across the tube. Therefore, the shape, with the help of the ultrasonic microscope, may be distinguished by the presence of a capillary.

In Fig. 6, the rod and tube are again shown, illuminated by a different type of ultrasonic ray. This discriminates between particles illuminated with different intensities and therefore depicts alterations.

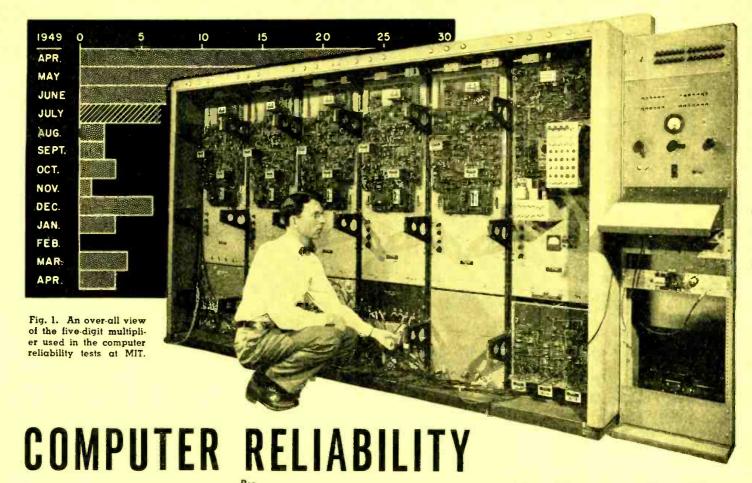
With the ultrasonic microscope, especially good observations may be made of structures. It must be determined which structure of the ultrasonic wave will give exactness of transmission without a type of deformation. When the radiating quartz plate oscillates in the fundamental mode, and no object is being examined, a light even spot is obtained. For oscillations above the fundamental, a nonuniform illumination results.

In the ultrasonic microscope, the object conforms to the tube, bound with the ultrasonic wave, and the image conforms to the transmission tube, on the screen of which the object is seen. One form of an ultrasonic microscope is shown in Fig. 1.



Fig. 8. Glass rod (left) and tube (right) in a nonhomogeneous ultrasonic field.





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Performance criteria of electronic digital computers based on results of an extended 27-month life test.

AINTAINING system reliability in a large digital computer is a far different problem from that encountered in the operation of radar, television, and other communication systems. A stray pulse or an intermittent failure of any one of thousands of electrical components, for example, may cause a circuit to function improperly and thereby invalidate all subsequent calculations. The engineer who enters the field of electronic computation must therefore adopt an entirely new concept of system reliability, based on the elimination of single errors. Unfortunately, he cannot find the criteria for implementing this concept in any textbook; he must learn them gradually from the experience of others and through his own cut-and-try methods.

The purpose of this article is to place on record the results of a 20,000-hour reliability run of a prototype digital computer, in which the goal was error-free operation for extended periods. Although this life test does not offer a specific answer to every question

it raises, the findings may give the reader a point of departure for developing his own philosophy on the subject.

Five-Digit Multiplier

Before the construction of the MIT Whirlwind I electronic computer* could be completed, it was essential that pertinent data be obtained on the reliability of basic circuits and the life expectancy of vacuum tubes and other components. Since no information on the extended operation of a system such as the Whirlwind could be found in the literature, a five-digit multiplier (Fig. 1) was built as the proving ground for the new pulsed circuits and components.

A short description of the multiplier will aid the reader in understanding the discussion of the life test which follows. The logical design of this prototype computer is shown in Fig. 2. The arithmetic element uses 275 yacu-

*A high speed digital computer sponsored by the Office of Naval Research.

um tubes, 350 crystal rectifiers, 800 resistors, 675 capacitors, 100 pulse transformers, and 80 r.f. chokes. Design was limited to one arithmetic process because the circuits and techniques are similar for each process; multiplication was chosen because of the strict circuit requirements it imposes. Storage and input-output elements were not stressed and appear in the simplest forms: toggle switches, push buttons, and indicator lights. The control was built from special pulse-control test equipment developed at MIT* and contains approximately 100 vacuum tubes and 950 other components.

When two numbers are to be multiplied, they are inserted manually into the registers of toggle-switch (T-S) storage. The numbers are read into the arithmetic registers and multiplication is executed by 0.1-microsecond pulses. A control switch provides for either automatic (2-mc.) or step-bystep (push-button) operation. Results are displayed in binary notation by flip-flop indicator lights.

A preventive-maintenance scheme, called "marginal checking," was built into the system in order to detect deteriorating components before they could cause errors in computations. (The rack at the extreme right in Fig. 1 holds these circuits.) The function of marginal checking is to vary certain

*Described in the Aug., 1951. through February, 1952. issues of RADIO-ELECTRONIC ENGINEERING.

voltages, generally screen voltages, in selected circuits of the multiplier so that the components operate under great stress. Any component with a low operating margin will effectively lose this margin during the check and the circuit will not operate. When a test problem is run, the operator can then isolate the weak component and replace it.

Power for the multiplier is supplied from three motor-generator sets whose d.c. outputs are -100, +150, and +250 volts. Power for marginal checking is obtained from a G-E amplidyne whose d.c. output can be manually varied from -100 to +100 volts. During marginal checking this generator is switched in series with the d.c. supply to the circuits which are to be checked.

Extended Reliability Run

On April 1, 1949, the multiplier started a reliability run which extended for 27 months. During this time, the machine continuously multiplied two five-binary-digit numbers and checked for a correct result at the end of each multiplication. The multiplications required about 8 microseconds each and were repeated at the rate of 15,000 times a second. When errors occurred, they were recorded by electromechanical counters and an Esterline-Angus inking recorder. Three counters were used as a "two-out-of-three" check; twice a day they were tested carefully to be sure they would respond to a single-error pulse.

Performance requirements were rigorous. All errors of undetermined origin and those from failures of defective, deteriorating, or accidentally damaged components were counted. Those resulting from failures of power supplies were also charged against the system. The only exceptions were errors caused directly by two failures in city power, two power line failures, and a transient introduced into the power line by a local thunderstorm.

For the first 18 months, about half an hour of each working day was spent in preventive maintenance. During the last nine months, as performance improved, this checking was reduced to twice a week. In addition, trouble-shooting for intermittent failures, not isolated by marginal checking, was necessary—especially for the first six months.

A log was kept during the entire run, with entries stating when errors occurred and what remedial action was taken. An operation chart was drawn daily from the information in the log to provide an over-all picture of the multiplier's reliability. The longest error-free run extended for 143 days, or nearly five months. It was interrupted when, for some unknown rea-

son, a power supply fuse burned out.

The test was terminated June 30, 1951, because operating experience on the Whirlwind I computer had reached a point where little benefit could be obtained from further studies of the five-digit multiplier.

Error Periods

Figure 4 summarizes the number of error periods that occurred during each of the 27 months. An "error period" is defined as the discrete period during which any number of errors occur without interruption. This number may range from one to several thousand, but since single errors, as well as multiple errors, can invalidate results and require the attention of an operator, each error period is considered as having the same weight regardless of the number of errors recorded. The total number of error periods over the 27 months was 142, or an average of one every 136 hours.

Work During Shutdown

Over half of the error periods (78) occurred during the first 96 days (April 1 through July 5, 1949). Considerable dependence had been placed on the marginal-checking facilities as a means of obtaining and keeping a high level of system performance, but this large number of error periods indicated that the new maintenance technique alone was not sufficient.

Because daily checking ensured that all circuits basically had wide operating margins, it was concluded that the frequent errors were caused by transient disturbances rather than by slow drifts in circuit tolerances. Intermittent connections were suspected first, and for lack of more refined methods, the search for such connections was made by

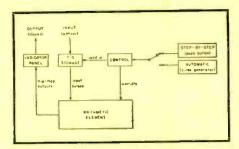
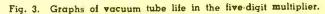
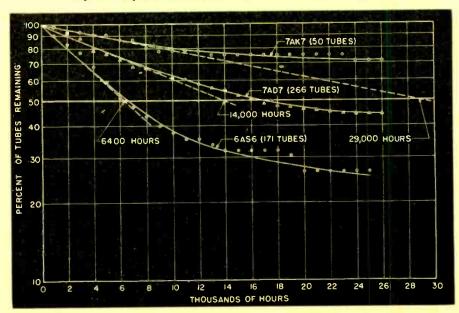


Fig. 2. Block diagram showing logical design of the five-digit multiplier.

painstakingly tapping panels and components. Within a short time sufficient weaknesses were found to indicate that a shutdown for overhaul was necessary. Nearly all of the faults discovered were ones which caused momentary rather than permanent failure. Furthermore, they would have been overlooked if evaluated by the usual criteria of performance; they were shown up in this case by the extreme sensitivity of the multiplier acting as a detecting instrument. The defects found were (1) insufficient spring pressure in cartridge-type fuse holders, (2) inadequate contact pressure in power distribution relays, (3) momentary shorts or leakage between elements within vacuum tubes, (4) poor connections in adapters which had been provided to permit use of lock-in-base tubes in circuits built for octal-base tubes, (5) loose screws on powerwiring terminal strips, and (6) unsoldered or cold-soldered component connections. The shutdown was utilized to correct all of the faults that had been discovered and to guarantee reliability further by eliminating all unnecessary contacts (such as relays and manual switches) and by replacing all fuse holders and tube adapters with





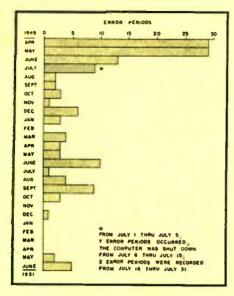


Fig. 4. Performance of the five-digit multiplier during the reliability run.

more rugged units. It is not known that all of these weaknesses would have caused operational failures if they had remained, but as a conservative measure they were regarded as potential faults and were therefore corrected.

During the 96 days following shutdown, the number of error periods decreased to seven. The error rate for the remainder of the 27-month run was an average of one every 286 hours.

Vacuum Tube Life

Significant information on vacuum tube life has been obtained from records on tubes used in the five-digit multiplier. The multiplier contains about 375 tubes (sockets) of which approximately half are types extensively used in the Whirlwind computer (40% of type 7AD7 and 10% of type 7AK7). About 18 per cent of the tube complement is type 6AS6, while small numbers of other types comprise the remainder.

Figure 3 shows the life characteristics of (1) the 7AK7, a dual-controlgrid pentode which was manufactured under pilot plant conditions, (2) the 7AD7, a video amplifier pentode purchased from commercial production, and (3) the 6AS6, a miniature dualcontrol-grid tube also from commercial production. The plot is percentage survival vs. length of service for original and replacement tubes. The criterion for the end-of-life of a tube is the tube's failure to perform satisfactorily in the circuit to which it is assigned. Life of the 6AS6 tubes is apparently much shorter than that of the other two types, because the 6AS6's are used in circuits that have smaller operating margins and the effective life of tubes in a given piece of equipment is closely related to circuit design. If it had been possible to build circuits in which

changes in tube characteristics had no effect on circuit performance, then the percentage of survival would have been much higher than these curves show.

A question sometimes raised in discussions of tube life is whether tubes tend to have a definite period of usefulness and therefore should be replaced as a group after a certain length of time or whether the failures occur at a fixed rate so that nothing would be gained by wholesale tube replacement. Experience with the multiplier seems to point to the latter type of behavior and certainly indicates that wholesale replacement is not warranted within the period of time shown on these curves. In Fig. 3, the data are shown on a semi-log plot with smooth curves (the solid lines) drawn through the points so that the slope of a curve is a measure of the rate of tube failure. For all three types the rate of failure decreases for increasing length of service, as indicated by the flattening out of the curves. However, the samples are probably too small for this fact to be considered significant. To get a conservative measure of tube life in this equipment, points have been determined where 50 per cent of the tubes would have remained if failures had continued at their initial rates, as shown by the broken lines. These figures are 6400 hours for the 6AS6, 14,000 hours for the 7AD7, and 29,000 hours for the 7AK7.

Other Components

No capacitors or r.f. chokes failed during the test and only two pulse transformers had to be replaced. On the other hand, it was necessary to replace 29 of the 120 carbon resistors selected to less than 1% tolerance for use in flip-flop circuits. Crystal clamps were also troublesome in flip-flop circuits, where a back resistance of at least 0.5 megohm is essential. One hundred clamps of a special high-backresistance type similar to the 1N38 were used in these circuits, and a total of 78 replacements was necessary because of the small tolerances. By comparison, 386 crystals (type 1N34 or equivalent) used in other less critical circuits required only 32 replacements.

Because a guarantee of maximum reliability was the intended goal, this sensitive clamp circuit should have been redesigned. However, rather than interrupt the test, a simple marginal-checking routine was applied periodically to the clamp circuits and the deteriorating crystals were quickly located. In this case, then, the desired reliability was ensured at the expense of additional preventive maintenance.

The importance of extensive operating experience in discovering unpre-

dictable factors that influence reliability was emphasized on several occasions. Two examples are of interest. As originally designed, the multiplier had pilot lights to indicate the presence of the +150-volt and +250-volt power inputs to each panel. These lights were 110-volt lamps fed from the respective supply points through appropriate dropping resistors. During the reliability run, it was discovered that occasionally an error count was caused by the burning out of one of these lamps. A search revealed that the dropping resistors were mounted near the filter circuits at the bottom of the panel and that the leads at the top of the panel were cabled for some distance with several wires which distributed power to the circuits on the panel. Under these conditions, interruption of current to a lamp caused a sudden jump in voltage on the wire to that lamp. This voltage jump, capacitively coupled into the power distribution circuits, was responsible for the errors observed. Relocating the dropping resistors at the lamps rather than at the filters eliminated the trouble.

The second example of unpredictable factors which can affect reliability was discovered accidentally. A metal coat tree in the multiplier room was habitually used by a few employees who worked in that portion of the building. One employee observed that a static discharge from hanging his new plastic raincoat on the coat tree caused multiplier errors. The exact way in which these were introduced was not determined. Previously, qualitative tests had been made to discover whether the system was sensitive to radiated signals and negative results were obtained. A commercial r.f. bomber was used for these tests and no attempt was made to cover the complete r.f. spectrum.

Noise Measurements

One of the aims of the multiplier reliability test was to examine the adequacy of maintenance techniques and, if possible, to discover new techniques which might be applicable to the Whirlwind I computer. Toward this end, some experiments were carried out to determine the sensitivity of the system to noise signals.

In the majority of electronic circuit applications outside the computer field, an occasional transient disturbance whose amplitude is comparable to that of the wanted signal is of little or no consequence. Interpretation of signals within these systems, whether by human beings or electrical equipment, involves an averaging or filtering process which effectively discriminates against noise. In a digital computer, however, interpretation of signals is done by memory

(Continued on page 31)

FUNDAMENTAL CHARACTERISTICS

THOSE who are familiar with various complex present-day computers will have no difficulty in classifying a specific one as being either "analog" or "digital." This classification into analog or digital computation is apt to be considered both exclusive and exhaustive. It is not difficult to put such two-valued faith to task. This faith may have been strained (though not broken) for the first time, perhaps, when the digital differential analyzer appeared on the scene. Some described it as a digital computer programmed in an analog fashion. Future computers may require, not a single, but a repeated employment of both of these words.

However, no revolutionary developments in the computer field are necessary to cause hopeless entanglement with this limited vocabulary. Suppose a novice were to ask humbly for an explanation of the difference between digital and analog. It would be natural to try to clear up this difference once and for all with a few simple examples. Take the speedometer of a car. The speed indication is by means of a shaft whose angular position is the analog of the speed of the car. This is a fine example of an analog unit, although an innocent reference of the novice to the numerical calibration of the dial might leave an uneasy doubt in the mind. The mileage indicator, on the other hand, is an excellent example of a digital unit: the leftmost wheel counts one for each 10,000 miles, the next wheel for each 1000 miles, and so on down the line. Unfortunately, the purity of this example is rudely shattered by the rightmost wheel; this black wheel of the family turns in a continuous fashion as any decent analog shaft would and seems to carry those large numerals only for the sheer purpose of confusion.

By this time there would probably be a distressed expression on the beginner's face, and, in search of a better example, the electric clock on the wall might be considered. Both hands of such a clock are mounted on continuously rotating shafts whose positions are the analog of time. When about to call the clock an analog unit, however, the beginner might suddenly announce that the two hands of the clock seem to be related to each other in a manner very similar to the wheels of the mileage indicator. In fact, are not the hands of the clock like digits, one showing finer details of the measured quantity than the other?

At this juncture, it might seem like a good idea to execute a strategic retreat and call the clock a unit consisting of OF DIGITAL

ANALOG

UNITS

By JOHN M. SALZER

Hughes Research & Development Labs.

The terms "digital" and "analog" by themselves are not adequate to describe a computer fully.

analog elements combined digitally. Indeed, it could even be said that this description would fit all clocks and watches. But then the pupil might point out that his watch says "tick-tock" and really measures time by counting the ticks and the tocks, that somebody had told him counting was an action characterizing a digital unit, and that this would make at least the second hand of his watch digital rather than analog! If this is not obvious, it is certainly clear that a stop watch moves in discrete jerks. To add to this burden of proof, it is only necessary to recall the big clock in any high school corridor, which jumps at one minute intervals.

After such an unhappy encounter with a novice, it would certainly be appropriate to re-examine the situation and it would not take very long to find that "digital" and "analog" are about as fortunate classifications for physical units as straw hats and round hats would be for men's headgear. Just as almost every hat is round in some respects, so is any measuring device or computer the analog of something in some respects. The analog of temperature, for example, could be a voltage in an analog unit or a number in a digital unit-in both cases within a certain accuracy. If an analog computer is the analog of a differential equation, a digital computer is the analog of a difference equation.

Whereas the analog class seems to be basically unrestricted, the digital class has more definite boundaries, as will be pointed out below. The real difficulty

- 1. Positional notation
- 2. Quantization
- 3. Sampling
- A purebred digital computer would incorporate all of these features, a thoroughly analog one none. But now examine each quality separately.

Positional Notation

Positional notation is a feature that is fundamentally digital. In the number 888, there are three identical digits; however, they carry different weights according to their relative positions. The high precision attainable in a digital unit is closely tied in with this positional notation. It is only necessary to use more digits of the same kind to increase the accuracy.

There are two ways in which the relative positions of the digits of a number can be recognized: in space or in time. A parallel machine handles all digits simultaneously and requires identical equipment (arranged in space) for each digit. On the other hand, a serial machine recognizes the weight of a digit by the relative time of its appearance at a particular point.

If it is agreed that "digital" means that which consists of digits—and how could it not be so?—, then it is clear that positional notation is a cardinal property of a digital unit. A binary relay register, for instance, is surely a digital

with the use of these words is caused by an endeavor to make them describe too much at once. Properties which are more fundamental should be reverted to and the equipment classified in terms of these properties. The writer has proposed' the following three features as a basis:

^{*}This article is based on a paper presented at the National Electronics Conference which was held in Chicago, Sept. 29, 30 and Oct. 1, 1952.

ω₀t in Degrees			
From:	Tot	$y(t) = \sin \omega_0 t$	
2. 10	4	*	
*		*	
- 30		*	
44.72	44.81	0.704	
44.82	44.86	0.705	
44.87	44.95	0.706	
44.96	45.03	0.707	
45.04	45.11	0.708	
45.12	45.19	0.709	
45.20	45.27	0.710	
3.4	- 1	*:	
200		100	

Table 1. Indication of how an unsampled quantity can be represented digitally.

unit; each relay is twice as significant as one of its neighbors, although it is physically identical. Or take the time clock at the entrance of a factory; the hour wheel has a much greater effect on the weekly pay check than the physically identical minute wheel.

Now consider a gas meter. One type of gas meter in existence shows about five small dials, like small clocks. Each dial is calibrated from 0 to 9 and boasts one hand only. The gasman reads the total consumption as a five-digit number. Although the five indicators are identical, they have different influence on the gas bill. So far, everything that has been said about the meter would class it a digital unit. Only when the individual digits are examined will any doubt arise, for each hand moves in a continuous fashion. As the gas flows, so moves each hand; therefore, each hand (with its own scale factor) is the analog of the gas consumed. Were the movements of the hands rigged with some escape mechanisms so that they would go through a revolution in ten distinct and equal jumps, the gas meter would be called digital without a doubt.

Quantization

This difference in the mechanism of an individual digit belongs in the discussion of the second basic feature, quantization. Assume an n-digit binary relay register; then for any finite n

greater than one, it will certainly be a digital unit. Even when n goes to one, the single-relay register is still likely to be considered digital because it can occupy only two possible states, i.e., it gives a quantized measure of whatever it represents. Had a decimal register been assumed, the individual digit would again be considered a digital unit because it is capable of assuming only ten different states.

As the number of possible states increases, the quantized nature of a unit becomes obscure and it is finally called analog. Indeed, some people say an analog unit is that which is quantized into an infinite number of states. Actually no shaft, however well machined. can stop at any of an infinite number of possible angles. The voltage on a condenser is generally considered a good example of an analog; yet it cannot change in smaller steps than the voltage due to a charge of a single electron.

To have faith in quantum theory, the fact that everything is quantized must be accepted in the final analysis. If so, how many possible states must a singledigit unit be capable of occupying-a hundred, a thousand, or a million-before it should be called analog? A direct answer to this question could only be arbitrary. The important factor is that quantization introduces an uncertainty into a physical quantity.

When a three-digit decimal counter reads 115, it may indicate that the value of the represented physical quantity is between 114.5 and 115.5. Therefore, the quantized representation is accurate within a tolerance. However, so is a nonquantized representation. If the indicator of a voltmeter stops at the 115-volt mark, it may only be known that the voltage is, for example, 115 ± 0.3.

Thus, an error is associated with both quantized and continuous indications. In what respect do these errors differ? They differ in their statistical distributions. Figure 1 shows possible distributions of errors in the examples used above. A quantized representation of 115 volts may mean anything between 114.5 and 115.5 with equal probability. If so, the error is uniformly distributed. as illustrated in Fig. 1(A). On the

other hand, the nonquantized representation generally has a less definite error distribution, which is often assumed to be normal. The tolerance limits may then correspond to the probable error. and such a distribution corresponding to the above example is shown in Fig. 1(B).

Just as statistical methods have recently been applied to noise analysis in communication engineering, they have long been applied to quantization errors or roundoff errors'. The use of the same methods in both cases is not accidental: rather it underscores the fundamental connection between uncertainties due to varied causes.

Sampling

The third aspect that is bound to enter a discussion of this kind is the process of sampling. Sampling can be defined as the act of taking specimens of a dependent quantity at particular values of the independent quantity. If time is the independent quantity, sampling implies that data are measured, defined, or examined only at particular instants of time.

Thus, sampling is basically related to the time and manner of observing data, rather than the type of unit involved. It is true that most kinds of digital units, such as digital data transmission equipment and conventional digital computers, require the sampling of data; nevertheless, digital units can be built that operate in a continuous fashion. It is further true that information approaching or leaving an analog unit is usually continuous; however, for technical convenience, sampled data are sometimes employed in analog systems. The only generality that can be stated is that when equipment is time-shared or when the observation of data takes a discrete length of time, the data involved must be sampled.

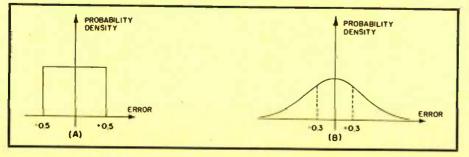
The process of sampling is illustrated in Fig. 2. Part (A) shows a continuous function of time, which may be displayed on an oscilloscope. The height of the luminous line above the base line is the analog of y(t). If the grid of the cathode-ray tube is pulsed on periodically, the sampled display of part (B) results. In part (C), the same sampled function is expressed digitally.

This simple illustration may raise two questions. First, although analog sampling is possible, why would it be used? Second, how can sampling be

avoided in the digital case?

Consider pulse communication. It is well known that if it is desired to transmit a band of B cps, it will be necessary to use a pulse repetition rate of at least 2B. The pulsed transmission of data has the advantage that the same channel may be used for several sets of information by time-multiplex-

Fig. 1. Possible distributions of errors in the examples given. (A) Uniformly distributed error. (B) Nonquantized representation of error distribution.



ing. The amplitude, the width, or the time of the pulse may be the analog of the function transmitted. On the other hand, in pulse code modulation the samples of the transmitted function are represented digitally.

Besides the time-sharing of equipment, another reason for sampling data is that an observation or a measurement may take a specific length of time to make. In radar, the time needed to receive an echo at maximum range defines the highest permissible pulse rate. The measured range is represented by an analog distance on the face of the oscilloscope. A motion picture is another example of sampled analog representation. Each frame is a sample of the object's illumination in terms of a chemical analog. The limitation of bandwidth due to sampling is vividly illustrated in movies when the wheel of the stage coach seems to rotate backward.

In order to indicate how an unsampled quantity can be represented digitally, Table I has been prepared. A portion of the sine wave is described in a continuous fashion within an accuracy of three decimal digits. This is done by indicating the degrees (or times) at which the function changes by a quantizing unit. No sampling is involved because the function is defined at all values of the independent variable.

One can build digital units or even digital computers to operate in a continuous manner, but time-sharing of equipment is precluded. This means that a separate element is needed for each digit (parallel unit) and for each operation. A dozen additions would call for a dozen parallel static adders. Such designs are possible and may be practical. A complex diode matrix may be designed to give the binary sum of two binary inputs, which energize the matrix. An experimental tube, the computron', has been partly developed to perform static arithmetic operations. At a recent computer symposium in Pittsburgh, a paper was presented on a special-purpose continuously operating digital computer'.

Elaboration on the difference and the relation between quantizing and sampling may be in order. Both processes introduce discontinuities, but while quantization produces a discontinuity in the value of a quantity, sampling produces a discontinuity in the times at which a quantity is specified. Figure 3 shows a portion of a sine curve quantized but not sampled in part (A) and sampled but not quantized in part (B). The step-discontinuities of quantization depend on the magnitude of the dependent variable, while the impulse-discontinuities of sampling depend on the independent variable.

Although quantization and sampling are fundamentally different effects,

they are interrelated. For example, it would be foolish to tabulate (sample) a sine wave at every millionth of a degree if it is defined only to three decimal places. Similarly, if sampling is done at every ten degrees, there is little advantage in a quantizing accuracy of ten decimal places. In numerical analysis, quantizing errors are called roundoff errors, while the errors arising from sampling are called truncation errors. In an efficient numerical procedure, these two types of errors are balanced.

The analogous situation has been commonplace in conventional analog equipment design. The counterparts of quantizing noise and sampling delay are respectively noise and response lag. Resulting errors (called respectively static and dynamic) should be of the same order in a well-designed analog unit.

Conclusion

It has been indicated that the division of units into digital and analog classes is often obscure and sometimes confusing. Three features have been proposed—positional notation, quantization, and sampling—as more fundamental in characterizing the nature of particular equipment.

Understanding these basic characteristics is not just of academic interest; it can also help in orienting engineers in new avenues of endeavor. By combining these basic properties in various degrees, new ideas and equipment may be more easily created than by thinking in terms of what is conventionally meant by digital and analog. Consider the future problems and solutions which may be ahead of us.

An interesting problem is the balancing of errors due to sampling and errors due to random noise. In serial digital computers, adjustable word lengths may be thought of as a means of changing the quantizing error and the real-time sampling rate simultaneously. Halving the word length could almost double the machine speed and would increase the quantizing error while de-

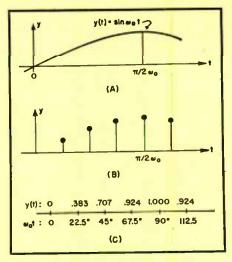


Fig. 2. The process of sampling.

(A) A continuous function of time.

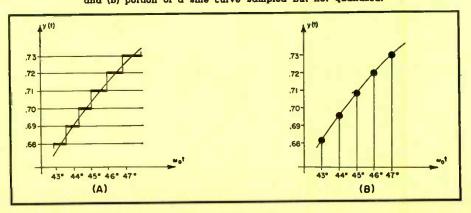
(B) Result of periodic pulsing. (C) Sampled function displayed digitally.

creasing the sampling error. The corresponding design change in an analog case makes the unit less accurate but also less sluggish at the same time.

A fascinating possibility is the use of units consisting of analog (nonquantized) elements combined in a digital manner, just as in the examples of the electric clock and the gas meter. For the transmission of data, such representation is not new. The coarse and fine dials with corresponding selsyns have been used in numerous cases. Could some kind of a computation be done on data so represented?

As techniques in designing compact digital equipment improve, the use of digital schemes for special purposes will become more and more popular. For fixed programs, the magnetic drum may prove a much more efficient and rapid storage element than for general purposes. Digital computations with nonsampled data may also be expected. In addition to the examples already cited, new developments, such as the perfection of ferroelectric techniques, might make such static computers generally practical. These computers will have (Continued on page 30)

Fig. 3. (A) Portion of a sine curve quantized but not sampled. and (B) portion of a sine curve sampled but not quantized.



NEW PRODUCTS

ULTRA-LOW FREQUENCY OSCILLATOR

An ultra-low frequency oscillator with standard rack panel construction has been announced by the Krohn-Hite Instrument Company. Model 400-C simultaneously provides both sine- and square-wave voltages at any frequency



between 0.009 and 1100 cps. The sinewave output may be used either balanced or single-ended. Maximum output is 30 volts peak-to-peak across a 1000-ohm load.

Special circuitry to eliminate tuning and bandswitching transients has been incorporated in this RC bridge oscillator. Descriptive pamphlet is available on request from the Krohn-Hite Instrument Co., 580 Massachusetts Avenue, Cambridge 39, Mass.

TV MASTER SWITCHBOARD

Increased operating control and flexibility are made possible by the television master switchboard recently developed by Federal Telecommunication Laboratories, Inc., Nutley, N. J. Completely self-contained, the unit permits the channeling of six separate inputs to six destinations by means of indirect relay



switching. These relays may be located in the console or at a remote rack.

Automatic clearing, termination and holding features have been incorporated in the switchboard, as well as adjustment of the gap or lap switching interval. The built-in fader employs a twochannel video amplifier through which any two incoming signals may be routed; the output signal may then be reinserted as an additional signal source. Tally lights and internally illuminated push buttons aid in operating effectiveness.

NOISE ANALYZER

Hermon Hosmer Scott, Inc., has announced a versatile sound analyzer which separates noise, sound and vibration signals into their component frequency bands. The high- and low-pass filters can be independently adjusted in steps of ½ octave, and a simple interlock permits the passband width to be fixed in any multiple of ½ octave. The



position of this passband can then be adjusted throughout the audible range by a single control.

Housed in a saddle-leather case with a shoulder strap for portable use, Type 420-A includes a calibrated attenuator, an indicating meter meeting ASA standards, and an output jack for general purpose filter applications.

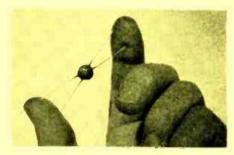
Inquiries should be sent to V. H. Pomper, Hermon Hosmer Scott, Inc., 385 Putnam Avenue, Cambridge 39, Mass. Bulletin is available on request.

MINIATURE PULSE TRANSFORMER

The smallest pulse transformer now commercially available was recently developed by *P C A Electronics*, *Inc.* Weighing less than .03 ounces, the MPT 101-0.1 is slightly smaller than a pea, making it specially suited to miniature assemblies; it will, however, operate equally well in conventional circuits. New design techniques and a special

iron core make possible 0.1-microsecond pulse widths and rise times of less than .005 millimicroseconds when used in recommended P C A circuits.

MPT 101-0.1 meets MIL-T27 test specifications. It can operate indefinitely



at temperatures ranging from -70°C to +125°C., and will operate normally for a short time at +150°C. Although it is designed for pulse forming, it can also be used for pulse coupling. For further information, write to P C A Electronics, Inc., 6368 De Longpre Avenue, Hollywood 28, Calif.

WAVE ANALYZER

Analysis of the frequencies and amplitudes of signal components in a complex waveform is accomplished in a simple and direct way with the new Sierra Model 121 wave analyzer. Signal components are read directly on a 4" indicating instrument calibrated in decibels. Voltage is calibrated with an internal 100-kc. injection oscillator, and a listening jack is provided for monitoring the signal being measured.

Just introduced by the Sierra Electronic Corporation, 813 Brittan Avenue, San Carlos, Calif., this 15 to 500 kc. wave analyzer incorporates a novel two-attenuator design which permits a wide range of measuring amplitudes without the introduction of instrument



distortion. It has an input level range of from +42 dbm to -70 dbm at a 600-ohm impedance level; input impedance is 10,000 ohms in the passband.

SCINTILLATION DETECTOR

A new scintillation detector, Model DS-1, has been announced by Nuclear Instrument & Chemical Corporation, 229 West Erie Street, Chicago 10, Ill. Designed for efficient gamma-ray counting in clinical and laboratory applications, the detector is provided with a

(Continued on page 30)

12 Reasons why Electronics Engineers should specify

SYLVANIA PICTURE TUBES



To definitely establish the superiority of Sylvania Picture Tubes, in comparison with other brands, Sylvania called an outside research organization . . . the United States Testing Company.

Eight picture tubes of nine different manufacturers were selected and submitted to identical electrical and mechanical tests.

Shown above is Sylvania's outstanding record. The test results showed that Sylvania Picture Tubes outlasted and outperformed all others tested. For the detailed report of these significant tests, write to: Sylvania Electric Products Inc., Dept. 3R-3502, 1740 Broadway, New York 19, N. Y.



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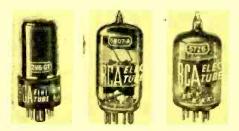
RADIO TUBES; TELEVISION PICTURE TUBES: ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT: FLUDRESCENT Tubes, fixtures, sign tubing, wiring devices; light bulbs; photolamps; television sets

NEW TUBES

RCA TUBES

The Tube Department of Radio Corporation of America, Harrison, N. J. has released three new tubes: a beam power amplifier, a medium-mu twin triode, and a "premium" twin diode.

Intended primarily for use in the output amplifier of automobile radio receivers operating from a 12-volt storage battery, the 12V6-GT is a beam power tube of the heater-cathode type. A single 12V6-GT operated with a plate and



screen voltage of 250 volts can deliver a maximum-signal output of 4.5 watts.

The 6BQ7-A is a medium-mu twin triode of the miniature type designed for use as the first r.f. amplifier tube in

a v.h.f. television-receiver tuner or as a low-noise i.f. preamplifier tube in a u.h.f. television receiver employing a crystal mixer. It supersedes the 6BQ7.

Especially useful as a detector in circuits utilizing wide-band amplifiers, the 5726 is a high-perveance, miniature twin diode. Constructed to give dependable performance under shock and vibration, this is a "premium" version of the 6AL5W.

HYTRON TUBES

Hytron Type 27EP4 is a 27" rectangular, 90°, all-glass, magnetically focused picture tube which provides an effective area of over 400 square inches. Features include an aluminized screen, single ion-trap gun design, and a neutral-density, spherical face plate.

Type 1N64 is a germanium diode designed to meet the requirements for a video detector in television applications. It is application-tested at both the low and high intermediate frequencies.

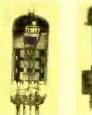
Both of these tubes are manufactured by the *Hytron Radio & Electronics Co.*, Salem, Mass.

TV PENTODE AND TWO DIODES

A new television pentode, the 12BY7, and two diodes for use in television

horizontal frequency damper circuits have been announced by the Radio Tube Division of Sylvania Electric Products Inc., at Emporium, Pa.

The 12BY7 is a high-transconduc-, tance sharp-cutoff video pentode de-







signed for service in television receivers. It features miniature T-6½ construction, and will furnish large output voltages across low values of load resistance and supply voltage.

Types 6AX4-GT and 12AX4-GT are half-wave, indirectly heated diodes contained in T-9 envelopes. They are designed to withstand the extremely high voltage pulses of line frequency between cathode and both heater and plate elements normally encountered in direct drive circuits. The 6AX4-GT and the 12AX4-GT are identical except for heater characteristics: the 6AX4-GT requires 6.3 volts at 1.2 amperes, while the heater of the 12AX4-GT requires 12.6 volts at 600 ma.

SKL WIDE-BAND DISTRIBUTION SYSTEM FOR TELEVISION





Two views of SKL Model 212TV Amplifier mounted in Model 420 Amplifier Cabinet, mounted on a felephone pole crossarm (top), pole (bottom). Courtesy Vermont Tele-

The -SKL- Distribution System provides simultaneous distribution of up to thirteen television channels, FM signals, and, if required, broadcast signals. Although the -SKL- system is inexpensive in initial cost, no effort has been spared to provide high quality, long lasting, low obsolescence designs and equipment. An unusual feature of the -SKL- system is the Model 212TV Chain Amplifier. These broadband amplifiers continue to operate even though a tube fails, which insures the high reliability so necessary in such a system. The -SKL- system is designed to have the lowest maintenance cost of any system on the market today, not only because of the reliability of the amplifiers which require no tuning or adjustment, but also because vacuum tubes have been eliminated in all other parts of the system. Only the -SKL- system can offer the long life, low obsolescence and low maintenance costs that are required for the long, profitable operation of distribution systems.

Write today for further information.

Right: Photo of erection of one of the two Horn Antennas at Barre, Vermont, for Vermont Television, Inc. These antennas, having 20 db gain, provide good signals from WBZ-TV Boston, 140 air miles, and WRGB Schenectady, 130 air miles.

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The Finest in Precision Equipment an oyster never advertises

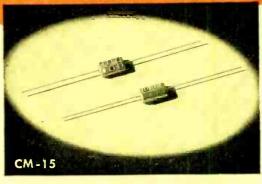
He seems to think you ought to like him for his shell, in spite of the fact that it looks no different from a million other oyster shells. If he's got a pearl inside, why doesn't he say so.

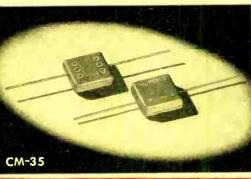
CAPACITORS LOOK PRETTY MUCH ALIKE FROM THE OUTSIDE, BUT EL-MENCO'S HAVE SOMETHING IN THEM and we want the world to know it.

Into every El-Menco Capacitor goes superb design, precise workmanship and the finest of materials. The finished unit is then factory-tested at *double* its working voltage to *insure* satisfactory performance on whatever job it is given.

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Write on business letterhead for eatalog and samples.

MOLDED MICA CAPACITORS

Radio and Television Manufacturers, Domestic and Foreign, Communicate Direct With Factory-

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WILLIMANTIC, CONNECTICUT

Personals



DR. ROBERT ADLER, who joined Zenith Radio Corporation, Chicago, Ill., in 1941 as a member of its research division, has just been appointed associate director of research. During the intervening years, Dr. Adler has made numerous contributions to the advancement of the electronics industry and to the improvement of communications equipment used by the armed services. He was awarded a Fellowship by the Institute of Radio Engineers in 1951.



F. CLARK CAHILL is now chief engineer of the Engineering and Production Division of Airborne Instruments Laboratory, Inc., Mineola, L. I., N. Y.; he formerly served in the Laboratory's Research and Engineering Division as supervisor of the Radar Section. During World War II, Mr. Cahill was associated with the Radio Research Laboratory at Harvard University as head of a war research work division. He has been with Airborne since 1945.



EDWARD L. COCHRANE, Vice Admiral, U.S.N., (Ret.), and Dean of the School of Engineering at Massachusetts Institute of Technology, has again been elected a director of Raytheon Manufacturing Company, Waltham, Mass. Admiral Cochrane first served in this capacity for Raytheon from 1948 until 1950, at which time he took a leave of absence from M.I.T. to direct the maritime administration in Washington as chairman of the Federal Maritime Board.



L. F. HICKERNELL, chief engineer of Anaconda Wire & Cable Co., Hastings-On-Hudson, N. Y., was recently elected a member of the board of directors of the American Institute of Electrical Engineers. Mr. Hickernell served as the chairman of the Detroit-Ann Arbor Section from 1929 to 1930; since then he has worked on many AIEE committees, both general and technical. His term as director will extend from January, 1953, through July, 1954.



DR. URNER LIDDEL has joined Bendix Aviation Corporation to direct product development in applied physics and atomic energy. Prior to his most recent position as chief of the physics branch of the U. S. Atomic Energy Commission, Dr. Liddel served as a civilian in the Office of Naval Research where he was director of the Division of Physical Sciences. He is a Fellow of the American Physical Society and the New York Academy of Sciences.



WILLIAM C. LUPFER has been appointed director of contract relations for Avion Instrument Company, Paramus, N. J., where he will be responsible for technical representation of all products. In 1943, Mr. Lupfer became associated with Sylvania Electric Products Inc., as contract and facilities supervisor for the Central Engineering Division, and more recently he was with Allen B. Du Mont Laboratories, Inc., as government contracts administrator.

A.F. Wattmeter

(Continued from page 7)

pling is employed between the two output transformers. The difference of the outputs is taken by reversing the connections of one thermocouple.

Protection against thermocouple overload and burn out is provided by the double-diode 6AL5 clippers interposed between the two amplifiers. These are adjusted to clip or cut off the output at a voltage value just below the point at which the thermocouple heater currents reach 125% of rated value. Since the couples are rated to stand 150% current, a small safety factor is included here.

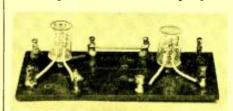
A calibration curve of meter reading vs. input power to resistive or reactive loads is shown in Fig. 3. For a given power input, change of load power factor over a wide range of capacitive or inductive angles makes no change in the reading. For all values of load voltage between zero and 150% of rated value, and with the load current circuit open, the meter stays at zero power.

The particular couples chosen for speed of response have heater ratings of 100 ma., 2 ohms, and couple ratings of 25 millivolts, 7 ohms. The indicating instrument used has a range of 50 microamperes and a coil resistance of 160 ohms. Full scale readings with a load power of 1.5 watts can be obtained.

Speed of response is not as slow as might be expected, full scale being reached from zero in slightly less than one second. For small change from a median reading, the response is even more rapid. Because of the protection given by the diode clippers, there is no fear of burn out or damage due to overload, and the instrument becomes as foolproof as a vacuum tube voltmeter.

Frequency range depends on the selection of the input step-up transformer and coupling capacitors, and to a very limited extent on the choice of the output transformer. The range of 50 to 15,000 cycles can be easily covered with conventional design, and this can be extended through the selection and loading of the input transformer. For extreme frequency ranges, the input transformer can be eliminated and input taken directly from the shunt. Additional voltage gain of about 50 can then be provided with another amplifier stage of conventional design.

Assembly of vacuum thermocouple pair.



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Military types CR15, CR16, CR18, CR19, CR23, CR24, CR27, CR32, CR36, CR47 are representative of current production by Bliley. Complete range of types and cross reference index is given in Bulletin 43.

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FREQUENCY STANDARDS

Types MC7, SR5 and SR8 are suggested for shipboard dependability. Price and details given in Bulletin 44.

Types BC46T, MO3B, TC92 are first choice for automatic temperature control in AM, FM and TV transmitters. Consult Bulletin 43 for basic details.

Types SR10 and MC9 provide wide range frequency choice for TV service, diathermy and citizens band. Request Bulletin 44 for price and description.

Type BH6A is the predominant choice for land mobile and airborne applications. Consult Bulletin 43 for basic information.

Types KV3, MC9, SMC100 and MS433 cover reference frequencies from 100 kc through 10.7 mc. Price and "stock tolerances" given in Bulletin 44.

Types AX2 and AX3 together with Bliley packaged oscillator Model CCO-2A were designed to bring precision and price together in the Ham Bands. Price and details are given in Bulletin 44.

Custom built fused quartz delay lines provide high stability and precision time intervals for manipulation of pulsed or pulse modulated signals. Consult Bulletin 45 for technical information.

Model BCS-1A is a high stability instrument for precision reference at 100 kc. Ideal choice for research and development laboratories. Descriptive information given in Bulletin 43.





BLILEY ELECTRIC COMPANY
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COAXIAL CABLE SYSTEM

A revolutionary coaxial cable system, with triple the telephone circuit capacity of those now in use, has been de-



veloped by Bell Telephone Laboratories and is undergoing exhaustive field trials prior to its installation in the Bell

System. It is expected to go into actual service on circuits between New York and Philadelphia early in 1953.

Known as "L-3" carrier, the new system will enable one pair of coaxial pipes (pencil-size tubes of copper within the cable itself) to handle simultaneously more than 1800 telephone conversations or 600 telephone conversations plus one television program in each direction. It will be the first carrier system on which both television signals and regular telephone conversations can be sent over the same pair of coaxial pipes at the same time. (Photograph shows a *Bell* engineer testing transmission characteristics.)

IEC STANDARDS

Nineteen countries were represented by 418 delegates at a series of meetings

of the International Electrotechnical Commission at Scheveningen, Holland, last September, to discuss international agreement on electrical standards. The United States participated in almost all of the technical meetings.

Among the important actions taken was the authorization of a new technical committee to develop standards for electronic tubes. A number of standands were completed for submission to the national committees, including safety rules for amplifiers and loudspeakers, several standards for radio components, and a revision of standards for power capacitors.

Arrangements were made for extending cooperative action on standards of joint interest to IEC and the International Commission on Rules for the Approval of Electrical Equipment (CEE).

TWIN-ENGINE FLIGHT TRAINER

U. S. Navy airmen will now "fly the beam"—including the new omni-range—in twin-engine ground trainers as the



new ERCO Flightronic trainer takes its place in the fleet's All Weather Flying School at Corpus Christi. Designed by the Engineering and Research Corporation, Riverdale, Md., under contract to the Special Devices Center, Office of Naval Research, this instrument trainer features generalized twin-engine type cockpit and performance, the new Navy color- and shape-coded control knobs, and the Special Devices Center's new standard radio aids simulator and flight plotting board.

GIANT TV ANTENNA

Resembling "Big Bertha" herself, this 86-foot television transmitting antenna is undergoing preshipment tests at *General Electric Company's* Syracuse, N. Y., plant. Only half of the antenna is pictured, the other half being behind the test building.

This 8500-pound giant soon will boost by 12 times the transmitter power of



Station WCPO-TV in Cincinnati, Ohio. The preshipment tests are made to insure that the antenna will efficiently accept and radiate TV signals from the station's Channel 9 transmitter.

OPHAR

WAXES COMPOUNDS

Zophar waxes, resins and compounds to impregnate, dip, seal, embed, or pot, electronic and electrical equipment or components of all types; radio, television, etc.

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If your talent and skill are not being used in a way for which your education and experience has equipped you, come to RCA. Here you will find unusual opportunities to work in close association with distinguished scientists and engineers in research . . . development . . .

design... and application of specialized electronic equipment for military projects as well as for an ever-increasing line of diversified commercial products.

Positions open are lifelong career opportunities. They are not "temporary" jobs. Unlike "feast or famine" industries, RCA has forged ahead regardless of war or depression. You can continue advanced study at recognized universities under RCA's modern tuition refund plan. You and your family enjoy outstanding Company benefits. Yes, your future is better at RCA.

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Specialized Employment Division,
Dept. 204B
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30 Rockefeller Plaza, New York 20, N. Y.

RADIO CORPORATION of AMERICA

NEW LITERATURE

TRANSISTOR PROGRESS

The November, 1952, issue of the Proceedings of the Institute of Radio Engineers was completely devoted to the multitude of advances which have been made in transistor research and development. The 528-page journal, containing 51 individual articles, covered all phases of transistor progress. Many of the articles described new applications of transistors in amplifiers, oscillators, rectifiers, electronic computers, and switching circuits.

Copies of this transistor issue are available from the Institute of Radio Engineers, 1 East 79th Street, New York 21, N. Y., at \$3.00 each.

TV EQUIPMENT COMPLEMENTS

All equipment used in a television station is arranged into a few functional groups in the bulletin entitled "Television Equipment Complements for Station Planning" which has been published by the Television Transmitter Division of Allen B. du Mont Laboratories, Inc. 1500 Main Avenue, Clifton, N. J.

The detailed complement of each group is listed with prices and each complement is given a number for easy reference. A short description of the function of the complement is also in-

cluded in each case so that the station planner using this bulletin can select equipment for any size station, large or small, and arrive at the approximate total cost of his equipment.

TWO-WAY RADIO

Use of two-way radio for better coordination of men, materials and machines is discussed in an eight-page illustrated booklet published by the General Electric Company. Entitled "Instant Communication," the booklet is slanted to those who use materials handling and emergency service equipment, and others who have plant protection problems.

Also contained in this publication is a list of 27 G-E offices throughout the United States from which advisory service is now available on communication problems. Copies are free on request to the Advertising Inquiry Section, General Electric Company, Electronics Park, Syracuse, N. Y.

RADIOTELEPHONES

Eight radiotelephone models, two radio direction finder models, and various accessory units are described in a new eight-page catalog. Identified as Form 852, it is available from Applied

Electronics Company, Inc., 1236P Folsom Street, San Francisco, Calif.

Besides a description of the basic design features of these instruments, the catalog includes a full tabulation of models showing number and types of channels, frequency ranges, receiver sensitivities, transmitter power outputs ranging from 40 to 500 watts peak, tube complements, power requirements, dimensions, and weights.

ELECTRONIC INSTRUMENTATION

In a 32-page booklet, the Berkeley Scientific Division of Beckman Instruments, Inc., 2200 Wright Avenue, Richmond, Calif., briefly describes electronic instruments which provide direct reading digital presentation of information together with their principal industrial applications. "Electronic Instrumentation" covers high-speed counting; counting plus control; precise interval timing; and measurement of rpm, pressure, temperature, flow, viscosity, velocity, frequency, distance, etc.

EMBEDDED SELENIUM RECTIFIERS

The Rectifier Division of Sarkes Tarzian, Inc., located at 415 North College Avenue, Bloomington, Ind., announces publication of a new four-page folder dealing with embedded selenium rectifiers. Designated as Catalog B1, this folder gives detailed information on the various types of embedments made by Sarkes Tarzian, Inc. A copy will be mailed free upon request to the manufacturer.

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A four-page bulletin describing this device in detail is available from the International Research and Development Corp., Columbus, Ohio.

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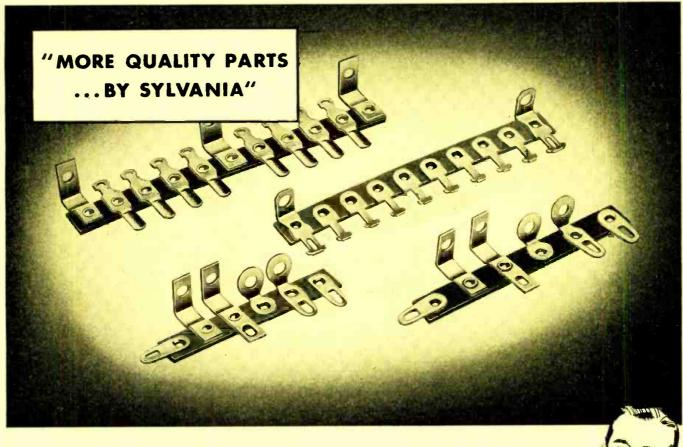
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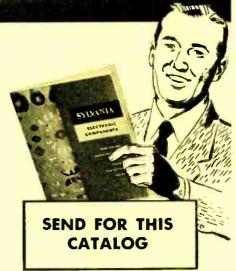
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RADIO TUBES; TELEVISION PICTURE TUBES; ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT; FLUORESCENT TUBES, FIXTURES, SIGN TUBING, WIRING DEVICES; LIGHT BULBS; PHOTOLAMPS; TELEVISION SETS



By WILFRID B. WHALLEY

Adjunct Prefessor of Electrical Engineering Brooklyn Polytechnic Institute

The development of the image orthicon.

AST month's article dealt with the development of the orthicon. This pickup tube provided quite stable operation, due to the use of low velocity electron beam scanning. It also had higher sensitivity than the iconoscope.

Still higher sensitivities were necessary, so that studios could operate with lower light levels, and so that outdoor scenes could be satisfactorily transmitted on cloudy days. Even with the improved characteristics of the orthicon, more lighting was required for good studio pickup than was comfortable for the performers. Further, the coming field of color television would require higher pickup tube sensitivity because of the fundamental loss of light through color filters or dichroic mirrors.

Another important requirement was that of smaller volume, particularly a reduction in the area of the light target so that lenses of sizes similar to those used in moving picture cameras might be employed. Then, too, for a lens of a given f number, greater depth of focus could be obtained with a smaller mosaic area; this, despite the fact that a smaller mosaic area reduces the photosensitivity. Also, to increase the depth

of picture focus, it was important that the mosaic or light sensitive surface be close to the end of the tube, and therefore adjacent to the lens.

Increasing Sensitivity

Starting with the orthicon, which had a sensitivity already higher than that of the iconoscope, consider what additional methods might be employed to increase the light-to-signal sensitivity further.

First, secondary-emission multiplication of the photoelectrons emitted by the light target might be used. This could follow techniques used in the image-iconoscope and infrared viewing tubes where the mosaic is placed some distance away from and parallel to the semitransparent photoelectron emitting surface (called a photocathode). By operating the photo surface at a negative d.c. potential with respect to the mosaic, and enclosing the device within an axial d.c. magnetic focusing field. the photoelectrons arrive at the mosaic with sufficient velocity to release several secondary electrons for each photoelectron, hence increasing the signal output current from the mosaic.

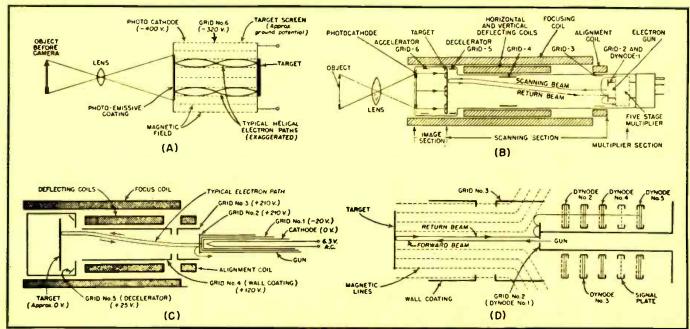
The iconoscope, image-iconoscope and orthicon used video preamplifiers with conventional pentode tubes. Such pentode tube amplifiers had been brought to a high level of efficiency by 1940. The product of voltage gain times mc. bandwidth reached a value of 180. Yet, for very small input signals and bandwidths of 4 mc. or more, these amplifiers gave relatively high noise factors, and were also critical with regard to microphonism and 60-cycle leakage currents. The basic limitation on sensitivity, common to all radio and radar systems, was the fluctuation noise component of plate current in the firststage tube, combined with the thermal noise current of the input circuit.

Multistage secondary-emission multiplier tubes had noise levels several orders below those of conventional receiving tubes. For example, the input dark "target" current of a good ninestage electron multiplier type phototube was less than 10° electrons per second (less than 10" ma.). This is approximately 10,000 times lower than the equivalent input noise current of a conventional video tube amplifier. However, to make use of secondary-emission multiplication, the primary signal electrons must be inserted into the evacuated envelope containing the secondary multiplication surfaces.

Secondary Electron Amplification

With iconoscopes and orthicons, the electron flow produced by the sequential discharging of the mosaic elements (with the scanning electron beam) went to a terminal in the glass wall. Hence, it was impossible with these pickup tubes to insert the primary electrons into a secondary-emission amplifier.

Fig. 1. Operation of image orthicon. (A) Image multiplier: (B) complete tube: (C) scanning section: (D) electron multiplier.



However, further examination of the orthicon operation suggested the possibility of using the electron scanning beam. As was discussed in last month's article, when the electron beam approached the surface of the mosaic, electrons were collected in proportion to the potential of each part of the surface (as determined by the degree of illumination). The uncollected electrons in the scanning beam were turned back. Therefore, this returning beam had a density varying, in time, with the degree of darkness of the surface being scanned. Also the noncollected electrons moved through the magnetic deflection region over a path almost identical to that of the forward scanning beam.

If the horizontal scanning were controlled by electromagnetic fields instead of electrostatic as in the orthicon, and this would be practicable if the tube were smaller, then the returning electrons could arrive at a point close to the aperture of the electron gun. Further, it might be possible to have a suitable secondary-emitting surface at the point of arrival so a secondary-emission multiplier could be used.

The image orthicon is such a device making full use of secondary-emission multiplication, both at the image and at the signal output.

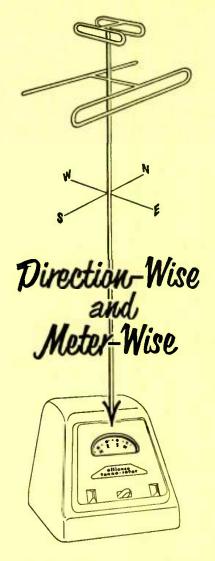
The Image Orthicon

As may be seen from Fig. 1 (from "Practical Television Engineering" by Scott Helt), the image orthicon contains image multiplication, scanning and secondary-electron multiplier sections. The tube is also physically smaller than the orthicon. The conducting shield, grid No. 6, in combination with the very fine mesh screen adjacent to the mosaic, maintains a uniform electric field in the image multiplier region. Hence, the photoelectrons from the photocathode are accelerated toward the mosaic or target, and kept in focus by the axial magnetic field. The two-sided target or mosaic is a unique development and consists of an extremely thin piece of special glass having a conductivity sufficient to allow electron charges to be neutralized in the time of one picture frame (one-thirtieth of a second). Glass thickness is between 5 and 10 wavelengths of visible light. The target is about two-thousandths of an inch distant from the very fine mesh screen. Because of the close spacing and thin structures, both the target and the screen must be mounted under tension.

In addition to stabilizing the field in the image region, the fine screen also collects any secondary electrons which are emitted from the target, and therefore avoids possible random distribution of electrons over the target surface. The decelerating ring, grid No. 5, together with the conducting wall coating, grid No. 4, between the target and the gun, reduces the arrival velocity of the electrons in the scanning beam to a suitably low value.

The five-stage electron multiplier is built around the electron gun. Each section consists of a disc of many vanes, each vane being inclined at 45° to the axis of the gun, and treated to give high secondary-electron emission. As the returning electrons strike the surface of grid No. 2, (which is effectively also dynode No. 1), secondary electrons are emitted and these are collected by the first ring, dynode No. 2. The secondary electrons produced on the surfaces of dynode No. 2 are accelerated to dynode No. 3, and similarly through the following stages to the collector (or signal plate) to which the video preamplifier is connected. In order to prevent retrace "smear" of the signal, negative blanking pulses are applied to the target.

The image orthicon is now the most used tube for television studio and outdoor cameras. When carefully adjusted, it has a sensitivity approximately 100 times as great as that of the orthicon. Due to its high complexity, however, great care is required in setting the various electrode voltages and the currents for the d.c. magnetic focusing and alignment



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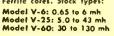


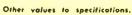
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Guided Missile Data

(Continued from page 5)

circuit flexibility for recording oscillographs or similar instruments and in no way limit their construction features to telemetry alone.

Communication facilities and remote control are provided for the supervisor of oscillograph recording as well as duplicate control points directly tied in at the telemetry stations. Panels providing for information to be patched into the oscillographs enable recordings to be made of the following data:

- 1. FM/FM telemetry discriminator out-
- 2. FM/FM telemetry decommutator outputs
- 3. PW/FM telemetry decommutator outputs
- 4. Land line telemetry (from the missile launcher, such as first motion, squid firing, etc.)
- 5. Timing signals

The oscillograph rack and all its component units were furnished under a development and fabrication contract (AF-33(038)24908) between the Air Force Missile Test Center at Patrick Air Force Base and Spar Engineering and Development, Inc., Jenkintown, Pennsylvania. Specifications, drawings, and technical exhibits of the contract established the design and layout of the panels and units.

Each panel or unit is separate, removable and essentially complete in itself. The panels provide for patching by means of recessed Western Electric type female jacks. An aluminum channel frame is formed to extend in a deep "U" from the front panel to a depth of about 14 inches. Across the outside of the aluminum extrusion in the rear, a Jones strip is mounted which terminates all the jacks mounted on the front panel. Thus, a panel may be easily removed by loosening all the screws on the Jones strip so that the barrier strip securing all the rack cable harness falls free when the front panel screws are removed. This type of construction places all the rear terminals and cable harnesses at a convenient depth in the rack and, since none of the terminal strips are mounted on the front panel, it can be of minimum size. All panels are of standard height or multiples of 1%", and 19" wide.

Amplifiers are also available to drive galvanometers properly from equipment having low signal outputs, or to provide sufficient levels for high frequency elements, and to provide isolation and sensitivity controls for incoming land line functions. The "amplifier panel" specifications are as follows:

Input impedance—100,000 ohms p.p. Input level for rated output—5, 10, 50, and 100 volts Input connector—Western Electric jack type 246A

Frequency response—0-10,000 cps
Output impedance—330 ohms balanced

Ouput current—maximum ±10 ma. Output connector—Western Electric jack type

Front panel indicators—meter to show relative output, amplifier balance and jeweled power lamp

Front panel controls—input attenuator, amplifier balance, meter selector switch, power switch and fuse

Power input-110-120 v., 60 cps

The "galvanometer panel," as the name suggests, provides a means of applying signals to the galvanometer elements. It is mounted directly above the oscillograph for operational case. Since this "galvanometer panel" has been designed to work in conjunction with an 18-element oscillograph, it provides circuitry for the full 18 galvanometers. Information to be fed to a galvanometer is patched in its respectively numbered jack. But, current flowing to any galvanometer must pass through its polarity reversing switch, attenuator, and continuity switch. This arrangement permits the recording technician to present several conditions to the oscillograph and, with the continuity switch open, to keep any or all of the galvanometer circuits open. To check operation, he can flip the switch to "momentary" position. For recording the flight, the desired continuity switches would be set in "continuous" position. The attenuators permit the setting of desired sensitivities directly at the recorder while viewing its limits of deflection. It is true that most of the telemetry equipment provides for level adjustment at the telemetry station itself, but it is not practical to adjust the levels remotely without excessive adjustment time and additional personnel. Polarity reversing switches are required to provide proper direction of deflection in order to permit closer correlation with similar events and easier data reading by deflecting the traces in parallel movement and reducing the times when traces cross, or adjusting channels so that the crossing angle will be great. These switches are recessed and are under a cover plate to maintain a neat appearance and to prevent accidental switching. The "galvanometer panel" specifications are as follows:

Input impedance—330 ohms constant Input connector—Western Electric jack type 246A

Output impedance—330 ohms constant

Front panel controls—polarity reversing switches, attenuators and continuity switches

The feature of this rack assembly

which permits oscillographs to be operated in a minimum of space is the slide rack chassis unit. This type of support for the oscillograph makes it possible for the instrument to be contained within the rack. For operational ease, it can be extended six inches and locked securely for adjustment, calibration or servicing. Continuous operation is achieved in any position. The galvanometer and power leads are twisted pair shielded cables.

An oscillograph phone unit was designed so that voice communications via hand phone or line amplifier would be available between the telemetering stations and missile checkout or launching areas. It also provides remote control facilities for operating the oscillographs, and an operations "hold fire" switch and indicator. The remote control circuits of the oscillograph permit a technician to supervise the operation of a bay of oscillograph racks, or permit it to be remotely operated and monitored at the telemetry receiving station. Control indicators show the standby condition of each oscillograph and any malfunction which may occur during an operation. Since the oscillograph racks are under the surveillance of one supervisor, only one oscillograph rack in a bay requires a phone unit.

The "hold fire" circuit is peculiar only to the missile test ranges. The usual techniques of firing a missile or projectile in any test program involve considerable instrumentation, coordination and safety precautions, and the only way every group involved or affected may be ready is to count down in seconds for the last interval before firing. In a development and test program, it is essential that all instrumentation be operating correctly at the time of launch. Yet, if the inevitable malfunction occurs a short time before firing, it must be reported immediately so that steps may be taken to prevent useless firing and loss of the missile as well as operation of equipment that requires considerable time to adjust or reload. For this purpose a switch, with safety cover, is located on the phone panel to indicate remotely and locally that a malfunction which the supervisor considers of a serious nature has occurred. A buzzer is also energized locally on the panel so that in the event the visual indication from a jeweled lamp is overlooked, the aural indication will alert everyone. Each indication of the "hold fire" system is on a separate electrical circuit.

The hand phones used with the units are Signal Corps Type EE-8. Again, this is equipment common to the majority of missile test ranges in the country today; it is a very fine handset for land line communications. Audio bridging amplifiers are provided so that

the messages may be monitored without holding a handset all the time or requiring another man as a "talker." The amplifier has an input for balanced or single-ended lines with an impedance of 50,000 ohms from either side to ground. Output power is 4 watts across a 500-ohm line with 0-db input.

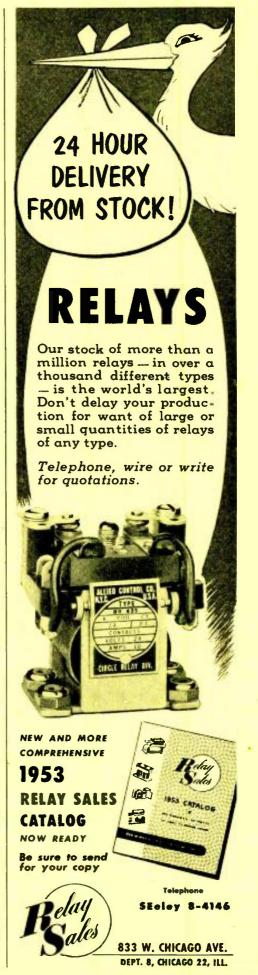
In conclusion, it should be stated that the equipment and design provide professional reliable operation of oscillograph recording equipment. It has been pointed out that each unit, or group of functions which are separate from the others, is fabricated complete in itself. This permits standardization of techniques and layout.

In some applications, several oscillographs are required to operate simultaneously from the same information. This occurs when instruments must be operated in tandem, as in cases where the instruments must be alternately reloaded with magazines for long or fast records. This follows the present planning since an oscillograph rack as described can be supplemented by racks on either side containing two or three oscillographs, each mounted on the oscillograph slide rack chassis assembly. Galvanometer panels may be associated with each oscillograph, or when the same data are on similar galvanometers, they may be controlled from the same panel if the elements are driven in series or parallel.

Proper damping is maintained on all elements at all times with the use of the galvanometer panel. The "T" pad attenuators feed the galvanometers with a constant 330-ohm resistive input, and all galvanometer shunts are made up to provide 64% damping when operating across the 330-ohm load.

Proper isolation and drive for galvanometers, when required for recording data from circuitry or equipment not suitable for direct connection to the elements, are provided by stable d.c. amplifiers. In addition to furnishing a means of setting up proper deflections, the limiting characteristics of the vacuum tube circuits prevent damage to many galvanometers by accidental hookup errors.

While this is not the first time an oscillograph has been assembled for rack mounting, it is one of the first installations to provide packaged components throughout. Although the described assemblies center about a particular application, many of the panels may merely require different labeling or the units may be rearranged to provide a wide variety of applications. All of the equipment described has been developed and fabricated, and is now commercially available. Installations of the described system have been made at the Air Force Missile Test Center, Patrick Air Force Base, Fla.



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BOOKS

"ELECTRON TUBES IN INDUSTRY" edited by Keith Henney, Editorial Director, and James D. Fahnestock, Associate Editor, of Electronics. Published by McGraw-Hill Book Company, Inc., 330 West 42nd Street, New York 36, N. Y. 353 pages. \$6.00.

The purpose of this book is to provide industrial personnel - engineers and technicians-with enough fundamentals to permit them to talk intelligently about electronics, to know what can be expected of electronic devices and what their limitations are, and to help them visualize new applications. In presenting these fundamentals, practical tried and tested circuits are used as examples. Many of these circuits have already found successful application in industry.

In this third edition, the book has been almost completely rewritten, bringing it up to date, eliminating unnecessary material, and emphasizing all practical aspects. Complicated theoretical aspects of electron tube technology have been held to a minimum. ---

Digital and Analog Units

(Continued from page 15)

features reminiscent of analog computers: they will have as many separate elements as there are operations to perform, and they will have, not a fixed delay of computation, but an exponential lag characteristic. It might be possible to interleave such digital units with analog ones quite efficiently, because of the continuity of data.

In general, the mixed use of digital and nondigital units in a computer has possibilities which call for constant reexamination as the art progresses. Even the controversy between proponents of digital and analog computers may one day be past history.

Some of the material presented here arose in connection with a doctorate dissertation1. The guidance and stimulation given to the author by Professor William K. Linvill has been instrumental in formulating many of these ideas.

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REFERENCES:

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New Products

(Continued from page 16)

thallium-activated sodium iodide crystal and has a plateau length of approximately 200 volts. With the external directional shield in place, efficiencies of 33% or greater are obtainable using cobalt 60, 40% or greater using iodine 131.

Model DS-1 is equipped with a removable directional shield, and has a builtin preamplifier which provides an output pulse in excess of one-quarter volt, making possible its use at the G-M input of any scaler or count-rate meter. It is available as a separate, complete unit, or with a special lead shield for sample counting.

RADIO CUE SYSTEM

Primarily for directing technical personnel and cue actors in a TV studio, the Model AB radio cue system can also be used in factories where the noise level is too high to permit direct communication. It was developed by the Polarad Electronics Corporation, 100 Metropolitan Avenue, Brooklyn 11, N. Y.

The transmitter operates on a low r.f. frequency into a loop antenna, which restricts the transmitted information to a closely confined area. Several r.f. channels are available if simultaneous transmission for separate activities is desired. Pocket receivers are small and lightweight.

JANUARY 26-30—IAS-IRE-RTCA-ION Symposium on Electronics in Aviation, New York, N. Y.

JANUARY 26-27 — Seventh Regional IRE Conference, University of New Mexico, Albuquerque, N. M.

FEBRUARY 4-6 - Western Computer Conference, Hotel Statler, Los Angeles, Calif.

FEBRUARY 5-7-IRE Southwestern Conference and Electronics Show, Plaza Hotel, San Antonio, Texas

MARCH 23-26-IRE National Convention, Waldorf-Astoria Hotel and Grand Central Palace, New York, N. Y.

APRIL 11-New England Radio Engineering Meeting, University of Connecticut, Storrs, Conn.

APRIL 18-Spring Technical Conference of the Cincinnati Section, IRE, Engineering Societies Bldg., Cincinnatt. Ohio

APRIL 29-MAY 1-Electronic Components Symposium, sponsored by the AIEE, IRE, RTMA and WCEMA, Shakespeare Club, Pasadena, Calif.

MAY 11-13—National Conference on Airborne Electronics, Hotel Biltmore, Dayton, Ohio

Computer Reliability

(Continued from page 12)

circuits which cannot distinguish between wanted signals and noise. For correct operation of these circuits, there can be no noise which equals the minimum amplitude of the wanted signal; and in practice, the peak noise should be considerably less than the minimum signal to ensure a margin of safe operation.

Two types of noise measurements were made, one in which asynchronous pulses of variable amplitude were inserted into various signal channels to simulate unwanted information pulses, and the other in which small voltage steps were introduced on different plate and screen lines to simulate power supply transients. The first of the tests uncovered a missing ground connection in one circuit and the second suggested a change in power supply filtering. Although it is felt that tests of this nature should supplement other maintenance procedures, no way has been found in which they can be readily mechanized for application to a large scale computer because of the variation in circuit impedance and in signal characteristics that would be encountered.

Experience gained during the conduct of the multiplier reliability test indicates that three significant conclusions may be drawn regarding the problem of obtaining error-free operation of an electronic computer:

First, errors resulting from gradual deterioration of tubes, crystal rectifiers, and other components can be practically eliminated if marginal-checking methods are used to locate weak circuits before they have caused operation failures. Until marginal checking was built into the multiplier, it was almost impossible to go through a day without computational errors and consequent shutdowns. During the life test, no errors could be attributed to deteriorating components-at least within existing ability to determine causes for failures. A total of 154 vacuum tubes and 83 crystal rectifiers were replaced because of low margins.

Second, lack of attention to the details of construction which ensure permanently good electrical connections throughout the system can result in potential sources of error which may

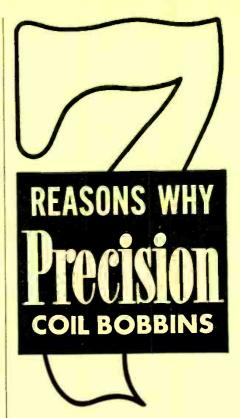
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go undetected for a long time. If such conditions exist, long trial runs with satisfactory operation do not establish the fact that the system is a reliable one. An example, taken from the log, will serve to illustrate this point. About halfway through the run, the multiplier started to make errors intermittently. The cause, determined only after tapping each component, was an unsoldered connection which had gone undetected for almost three years.

Third, failures that interfered with the useful operation of the multiplier fell into two general classifications: (1) sudden total failures of components and (2) intermittent circuit failures. At the outset, it was accepted that sudden failures, such as open or short-circuited components or connections, could be expected without warning and would cause errors in operation. Results of the test, however, showed that intermittent failures were far more serious because they were difficult to locate and correct. Of the 142 total error periods, 124 resulted from intermittent failures. Although the sources of some of these were undoubtedly detected and remedied, it was impossible to make direct correlations between errors recorded and defects corrected.

The principal value of the extended reliability test was the proof that circuits of the type used in the Whirlwind I computer could be constructed of presently available components and made to operate in a large system with relatively little time lost in unscheduled trouble-shooting and repair. Test data from the multiplier run could not be used to forecast the reliability of the whole Whirlwind computer since this system contained substantial numbers of components and circuits not present in the multiplier. The performance of the Whirlwind arithmetic element, however, indicates that a linear extrapolation of the multiplier experience to a larger system based on the number of tube cathodes is probably valid if similar circuits are involved. With this criterion, a system of five thousand tubes should average not more than one error period in each 20 hours of operation. For most mathematical, industrial, and scientific applications, this performance would be quite adequate. On the other hand, present-day thinking implies that much larger electronic systems are desirable for controlling actual physical situations where even a low error frequency is objectionable, and one must conclude that continued improvement in components, circuits, and system construction will be needed to obtain satisfactory reliability.

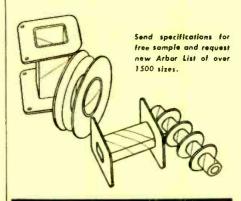


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IRE CONVENTION PROGRAM

Tentative list of papers to be presented at the IRE Convention in New York, March 23-26.

AIRBORNE ELECTRONICS

AIRBORNE ELECTRONICS

Some Systems Considerations in Flight Control
Servomechanism Desiga. R. J. Bibbero and R.
Grandgent. Republic Aviation Corp.
Faired-In ADF Antennas. L. E. Raburn, Electronics Research Inc.

Magnetic Amplifiers for Airborne Applications.
J. K. McKendry, General Precision Labs.

Aircraft Electrical Power. J. C. Dieffenderfer
and G. W. Sherman, Wright Air Dev. Ctr.

The Effects of Electronic Equipment Standardization on Aircraft Performance. G. C. Sumner. Consolidated Vultee Co.

The Technique of Monopulse Radar. W. Hausz,
G-E.

G-E.

Reducing Sky Wave Errors in CW Tracking Systems. M. S. Friedland, Patrick AF Base, and N. Marchand, Electronics Lab.

An Application of Integrator Type Signal Enhancer to Direction Finding Equipment. C. A. Strom and J. A. Fantoni, Rome Air Dev. Ctr.

A Theory of Target Glint or Angular Scintillation in Radar Tracking. R. H. Delano, Hughes Alercraft Co.

Aircraft Co.

Automatic Dead Reckoning Navigation Computers for Aircraft. J. L. Dennis, Wright Air Dev. Ctr.

ANTENNAS

The Measurement of Highly Directive Antenna Patterns and Over-All Sensitivity of a Receiving System by Solar and Cosmic Noise. J. Aarons. Air Force Cambridge Research Ctr. Radiation Patterns for Aperture Antennas with Non-Linear Phase Distributions. C. Allen, G-E.

G-E.

Pactors Affecting Radiation Patterns of Corrugated Surface Antennas. M. Ehrlich and L.

Newkirk, Hughes Aircraft Co.

A Microwave Anechoic Chamber for Antenna
Pattern Measurements. J. Simmons, Naval Research Lab.

Pattern Measurements. J. Simmons, Naval Research Lab.

Wide-Frequency-Range Tuned Circuits and Antennas. A. G. Kandoian and W. Sichak, Fed. Telecommunication Labs.

Arrays of Flush Mounted Traveling Wave Antennas. J. N. Hines, V. H. Rumsey and T. E. Tice, Ohio State U.

Transient Build-Up of the Antenna Pattern in End-Fed Linear Arrays. H. Enenstein, Hughes Aircraft Co.

A New Microwave Reflector. K. S. Kelleher, Naval Research Lab.

Crosstalk in Radio Relay Systems Caused by Foreground Reflections. H. W. Evans, Bell Telephone Labs.

Low Side Lobes in Pencil-Beam Antennas. E.M.T. Jones, Stanford Research Inst.

Notes on Propagation. L. A. Byam, Jr., Western Union Telegraph Co.

Tropospheric Propagation in Horizontally Stratified Media Over Rough Terrain. H. M. Swarm, R. N. Ghose and G. H. Keitel. Washington U.

Radio Wave Scattering in Tropospheric Propagation. J. W. Herbstreit, K. A. Norton, P. L. Rice and G. E. Schafer, Nat. Bureau of Standards.

Extended-Range Radio Transmission by Ohlique

United Nations. L. Beranek, MIT; C. W. Goyder, UN.
Variable Time Delay. K. Goff, MIT.
Flux Sensitive Head for Magnetic Recording
Play Back. D. E. Wiegand, Armour Research
Foundation.

Foundation.
Unlaxial Microphone. H. F. Olson, J. Preston and J. C. Bleazey. RCA Labs.
Sound Pressure Measurement between 50 and 220 DB. J. K. Hilliard. Altec Lansing Corp.
Fundamental Theory. L. Beranek, MIT.
Microphones. H. F. Olson, RCA.
Loudspeakers. H. S. Knowles, Industrial Research
Products. Inc.

Microphones, H. F. Olson, R.A.
Loudspeakers, H. S. Knowles, Industrial Research
Products, Inc.
Phonograph Reproducers. B. B. Bauer, Shure
Bros., Inc.
Tape Recording, Marvin Camras, Armour Research Foundation.
Studio Acoustics, H. J. Sabine, Celotex Co.
CIRCUITS

A General RLC Synthesis Procedure. L. Weinberg, Hughes Aircraft Co.
A General Theory of Wide-Band Matching, H. J.
Carlin and R. LaRosa, Brooklyn Polytech.
Synthesis of Electric Filters with Arbitrary Phase
Characteristics, B. J. Bennett, Stanford U.
Wide-Band Filter Amplifiers at Ultra-High-Frequencies, J. M. Pettit, W. A. Christopherson
and D. O. Pederson, Stanford U.
Network Analysis with the Aid of Generating

Polynomials. H. Kurss, Brooklyn Polytech.
Two New Equations for the Design of Filters. M.
Dishal, Fed. Telecommunication Labs.
Conventional Amplifiers. W. Bradley, Philo Corp.
Feedback Amplifiers. H. N. Beveridge, Raytheon

Feedback Amplifiers. H. N. Beveridge, Raytheon Mfg. Co.
Transistor Amplifiers. R. L. Wallace, Bell Labs. Distributed Amplifiers. W. G. Tuller and E. H. Bradley, Melpar Electronics.
Traveling Wave Tube Amplifiers. L. Field, Stanford U.

ford U.
Continuously Variable Delay Line. C. Berkley,
Allen B. Du Mont Labs., Inc.
General Transmission Theory of Distributed Helical Delay Lines with Bridging Capacitance.
M. J. DiToro. Allen B. Du Mont Labs., Inc.
Distributed Constant Delay Lines with Characteristic Impedances Higher Than 5000 Ohms.
W. S. Carley, U. S. Naval Ordnance Lab.
Helical Winding Expotential-Line Pulse Transformers for Millimicrosecond Service, J. Kukel and E. M. Williams, Carnegie Inst. of Technology.

and E. M. Williams, Carnegie Inst. of Technology.

Time Domain Approximation by Use of Pade Approximants. R. D. Teasdale, RCA.
Frequency Transients in Idealized Linear Systems. B. Gold. Hughes Aircraft Co.
Transient Analysis of Junction Transistor Amplifiers. J. J. Suran and W. F. Chow, G-E.
The Grounded-Collector Transistor Amplifier at

Carrier Frequencies. F. R. Stansel, Bell Tele-

pillers, J. J. Suran and W. F. Chow, G-E. The Grounded-Collector Transistor Amplifier at Carrier Frequencies. F. R. Stansel, Bell Telephone Labs.

Symmetrical Properties of Transistors and Their Application. G. C. Sziklai, RCA Labs. Div. Study of Transistor Circuits for Television. G. C. Sziklai, R. D. Lohman and G. B. Herzog, RCA Labs. Div. Conductance Curve Design of Relaxation Circuits. K. A. Pullen, Aberdeen Proving Ground. Transistor Relaxation Oscillators. S. I. Kramer, Fairchild Guided Missiles Div. ELECTRONIC COMPUTERS

Multichannel Analog Input-Output Conversion System for Digital Computer. P. A. Adamson and M. L. MacKnight. Hughes Aircraft Co. An Analog to Digital Converter with an Improved Linear Sweep Generator. D. W. Slaughter, Cal. Tech.

Dynamic Binary Counter with Analog Read-Out. L. Packer, Columbia U.

Life and Reliability Experience with Transistors in a High Speed Digital Computer. J. J. Scanlon. Bell Telephone Labs.

Engineering Experience in the Design and Operation of a Large Scale Electrostatic Memory. J. Logue, A. Brennemann and A. Koelsch. Int'l. Business Machines Corp.

Analog Computing with Magnetic Amplifiers Using Multi-Phase A-C Voltages. J. E. Richardson, Hughes Aircraft Co.

Some Recent Developments in Logical "Or-Andor" Pyramids for Digital Computers. C. Leondes, Pennsylvania U.

Magnetic Core Switches as Logical Elements in Computers. E. A. Sands, Magnetics Res. Co. Magnetic Shift Register Using One Core Per Bit. R. D. Kodis, S. Ruhman and W. D. Woo, Raytheon Mfg. Co.

Simple Computer for Automatically Plotting Correlation Functions. A. H. Schooley, Naval Research Lab.

relation Functions. A. H. Schooley, Naval Research Lab.

Symposium: Diagnostic Programs and Marginal
Checking for Large Scale Digital Computers.

ELECTRON DEVICES

ELECTRON DEVICES

The Negative Resistance Diode. I. A. Lesk and V. P. Mathis. G.E.
Reliability of Transistors. W. R. Sittner and R. M. Ryder, Bell Telephone Labs.
Characteristics of the M-1768 Transistor. L. B. Valdes, Bell Telephone Labs.
Developmental High Frequency Alloy Transistors. C. W. Mueller and J. I. Pankove. RCA Labs.
Behavior of Germanium Junction Transistors at Elevated Temperatures and Power Transistor Design. L. D. Armstrong, RCA Labs. Div.
Gas Pressure Effects on Ionization Phenomena in High-Speed Hydrogen Thyratrons. W. C. Dean. Odessa, Texas; G. W. Penney and J. B. Woodford, Jr., Carnegic Tech.
Low Noise. Hot Cathode, Gas Tubes. E. O. Johnson, W. M. Webster and J. B. Zirker, RCA Labs. Div.

RCA Labs. Div.
w Dispenser Type Thermionic Cathode. R.

Levi.
Multi Output Beam Switching Tubes for Computers and General Purpose Use. S. Kuchinsky, Burroughs Adding Machine Co.
An Equivalence Principle in High Frequency Tubes. Robert Adler, Zenith Radio Corp.
High Power Traveling Wave Tube Amplifiers.
M. Ettenberg, Sperry Gyroscope Co.

Operation of the Traveling-Wave Tube in the Dispersive Region. L. A. Roberts and S. F. Kaisel, Electronics Research Lab. A Traveling Wave Electron Buncher. R. B. Neal, Stanford U.

Some Properties of Periodically Loaded Struc-tures Suitable for Pulsed Traveling Wave Tube Operation. M. Chodorow and E. J. Nalos. Stanford U.

Experiments on Millimeter Wave and Light Generation. H. Motz. W. Thon and R. N. Whitehurst, Stanford U.

ENGINEERING MANAGEMENT

ENGINEERING MANAGEMENT
Report of Year's Activities by the Chairman of
the Professional Group on Engineering Management. R. I. Cole. Rome Air Dev. Ctr.
General Problems of Engineering Management
Facing the Electronics Industry. H. Pratt,
Telecommunications Advisor to the President.
Research and Development Problems of Engineering Management in the Electronics Industry.
M. J. Kelly, Bell Telephone Labs.
Production Aspects of Engineering Management
in the Electronics Industry. W. A. McDonald.
Hazeltine Electronics Corp.
What the Military Services Expect from Engi-

what the Military Services Expect from Engineering Management of the Electronics Industry. Major General D. L. Putt, Air Research and Dev. Command.

INFORMATION THEORY

Recent Advances in Information Theory. L. De-Rosa, Fed. Telecommunication Labs.

Radar Problems & Information Theory. H. Davis,

Radar Problems & Information Theory. H. Davis, Watson Labs.
Analysis of Multiplexing and Signal Detection by Function Theory. N. Marchand, Marchand Electronic Labs.
Optimum Nonlinear Filters for the Extraction and Detection of Signals. L. A. Zadeh, Columbia U.

and Detection of Signals. L. A. Zadeh, Columbia U.

Detection of Information by Moments. J. J. Slade. Jr., S. Fich, D. A. Molony, Rutgers U. Error Probabilities of Binary Data Transmission Systems in the Presence of Random Noise. S. Reiger. Air Force Cambridge Research Ctr. Statistical Properties of the Output of Certain Frequency Sensitive Devices. G. R. Arthur, Sperry Gyroscope Co.

Cross-Correlation Applied to Automatic Frequency Control. M. J. Stateman, Sylvania Elec. Prods. Inc.

Approximate Probability Density Function of First Level Crossing for Linearly Increasing Signal Plus Noise. G. Preston and R. Gardner, Phileo Corp.

Design Criteria for the Optimum Demodulation of Generalized Modulated Signals. F. W. Lehan, Cal. Tech.

A Necessary and Sufficient Condition for Unique Decomposition of Coded Messages. A. A. Sardinas and G. W. Patterson, Burroughs Adding Machine Co.

dinas and G. W. Patterson, Burroughs Adding Machine Co.

A Systematic Survey of Coders and Decoders. B. Lippel, Signal Corps. Engrg. Labs. Method for Time or Frequency Compression-Expansion of Speech. G. Fairbanks, W. L. Everitt and R. P. Jaeger, Illinois U.

A New Coding System for Pulse Code Modulation. A. G. Fitzpatrick, Burroughs Adding Machine Co.

Coincidence Detectors for Binary Pulses. C. Gates, Cal. Tech.

INSTRUMENTATION

A New Method for Measuring Noise Figure and Gain of a Radar Receiver. R. J. Parent and V. C. Rideout. Wisconsin U. Automatic Instrumentation for Continuous Monitoring of Systems Performance. M. V. Ratynski, M. Kant and H. Webb, Rome Air Dev.

ski, M. Kant and H. Webb, Rome Air Dev. Ctr.

Automatic One-Shot Methods for Bandwidth Measurement. J. B. Woodford, Jr., and E. M. Williams, Carnegie Tech.

Microwave Power Meter with Automatic Zero Setting and Telemetering. L. A. Rosenthal and G. M. Badoyannis, Rutgers U.

Monitoring of Errors in Synchro Servo Systems. G. Quazza. Brooklyn Polytech.

Transistor Metrology. D. A. Alsberg, Bell Labs.

Measurement of Transistor Parameters by CRO and Other Methods. W. E. Morrow, Jr., MIT.

Transistor Static Characteristics Ohiained by Pulse Techniques. D. R. Fewer. Bell Labs.

Bridges for Measuring Junction Translator Admittance Parameters. L. J. Giacoletto, RCA.

A Transistor Alpha Sweeper. H. G. Follingstad, Bell Telephone Labs.

Rapid Tracing of Transistor Characteristics by Oscillographic Methods. V. Mathis, G.E.

The Response of a Panoramic Receiver to CW and Pulse Signals. H. W. Batten. R. A. Jorgensen, A. B. Macnee and W. W. Peterson. Michigan U.

A VHF Impedance Meter. J. H. Mennie, Boonton Badic Corn.

A VHF Impedance Meter. J. H. Mennie. Boonton

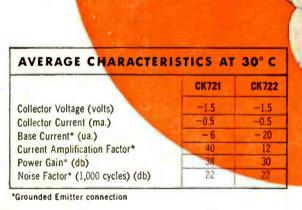
Radio Corp.
Simplified Measurement of Incremental Pulse
Time Jitter. W. T. Pope, Griffith Air Force

Base.
Wide-Band Wave Analyzer. O. Kummer, Bell
Telephone Labs.
Ultra-Low Frequency, Three-Phase Oscillator.
G. Smiley, General Radio Co.
(To be continued in March issue)



PNP GERMANIUM JUNCTION

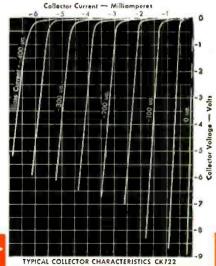
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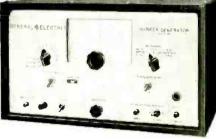
Marker Generator ST-5A. Marks all the critical frequencies on a pass band as well as having continuous coverage. Designed to give fast manipulation with crystal controlled accuracy for outstanding performance. Features separate crystal on each TV channel with simultaneous picture, audio and trap markers on both channel and intermediate frequencies.

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Model ST-2A



Model ST-SA



Model ST-4A



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This illustration clearly shows that the concentrated field of energy between the two conductors, which are 7 strands of #28 copper weld wire, is contained by the tubular construction. This important field of energy is unaffected by any exterior conditions.

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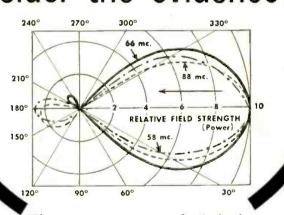




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The test patterns on both high and low bands reveal the Amphenol Inline Antenna's superior uni-directional reception lobe. This single forward lobe intercepts the TV signal at its maximum available strength. It also rejects unwanted reflected signals or side interference that cause "ghosts" and unsteady pictures.

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1. BY MAKING CBS-HYTRON TV ORIGINALS BEST.

Longest experience with production . . . with applications . . . with improvements . . . all count. CBS-Hytron-built 1AX2, 1X2A, 6BQ6GT, 12A4, 12B4, 12BH7, 12BY7, 12BZ7, 25BQ6GT, 16RP4, etc. are more trouble-free. Prove it to yourself.



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3. BY APPLYING "RELIABLE" TUBE TECHNIQUES.

CBS-Hytron 6AL5 is typical. Experience with the military 6AL5 family (JAN 6AL5, 6097/CT, 5726) is passed on to you. You profit by a commercial CBS-Hytron 6AL5 made truly reliable.



4. BY MATCHING EACH TUBE TO THE SET.

Daily, CBS-Hytron analyzes leading TV chassis. Dynamic socket-by-socket checks, plus continuous field experience, pay off. Give you

CBS-Hytron matched-to-the-set performance... with the accent on trustworthy replacements.

Take advantage of CBS-Hytron extras like these. Keep your customers happy. Guarantee yourself against profit-slicing call-backs. Demand dependable CBS-Hytron tubes.



Wish you could test a chassis topside? Without first pulling and wrestling with the heavy chassis? Without disturbing wiring and parts by digging underneath for buried sockets? How much

faster, easier, safer you could work! New CBS-Hytron Test Adapter does the trick. Just replace a 7-pin miniature tube with the Test Adapter. Plug tube into Test Adapter. Presto, all socket connections are topside . . within instant reach of your test prod or clip. Just one job pays for this new CBS-Hytron Test Adapter. Get yours today!

HERE'S HOW! With the CBS-Hytron Test Adapter, you quickly measure voltage, resistance, gain. You inject and trace signals . . . monitor intermittents. You check oscillating stages. Or the effect of adding a bypass condenser or shunt resistor.

With several CBS-Hytron Test Adapters you make stage-bystage circuit checks... fast. You do all this dynamic testing the e-a-s-y way..., topside. With no ill effects at a-f frequencies. And only slight capacitance and inductance effects at much higher frequencies.

You will like: The positive contact of the low-resistance, silverplated hase pins and test points. The plainly marked pin connections. The easy insertion and tight grip. CBS-Hytron Test Adapter is another designed-by-and-for-you "must" you must have. See your CBS-Hytron jobber today.

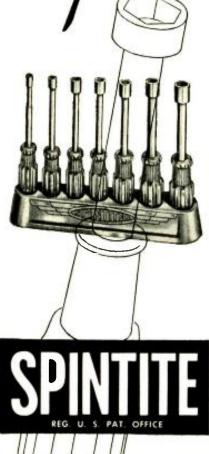






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- ASSEMBLY WORK
- REPAIR WORK
- RADIO
- TELEVISION
- INDUSTRIAL
- AIRCRAFT



Within the INDUSTRY

JACK A. BERMAN, in charge of sales for Shure Brothers, Inc. for the past



thirteen years, will head his own manufacturers' sales representative firm in Southern California.

Mr. Berman, who is resigning as *Shure Brothers*' vice-president in charge of sales and as treas-

urer of the Radio Parts & Electronic Equipment Shows to establish his own firm in Los Angeles, will represent *Shure Brothers* and other manufacturers' lines in the Southern California territory.

THE HAMMARLUND MANUFACTURING COMPANY has leased an additional 12,-000 square feet of factory space at 541 West 34th Street in New York for use in sub-assembly manufacturing, spare parts packing and shipping, and for stocking standard condensers . . . PYROFERRIC COMPANY has acquired new space at Bronx Boulevard and 216th Street in New York in order to increase production facilities for iron cores and other powdered metal components . . . COMMUNICATION MEAS-UREMENTS LABORATORY, INC. has moved into its own modern one-story plant at 350 Leland Avenue, Plainfield, New Jersey. The company had had its headquarters at 120 Greenwich Street in New York City for fourteen years . . HYTRON RADIO AND ELECTRONICS

co. has begun construction on a new 150,000 square feet of additional space for manufacturing and warehousing at Newburyport, Massachusetts . . . PRE-MIER T.V. RADIO SUPPLY has moved to new quarters at 3239 West North Avenue, Chicago 47, Illinois. The new location provides four times as much space as the company formerly occupied . . . SYLVANIA ELECTRIC PROD-UCTS INC. has dedicated its new radio receiving tube plant at Burlington, Iowa. The multi-million dollar, 150,000 square foot plant will be an important supplier of radio tubes to the armed forces . . . HYTRON RADIO AND ELEC-TRONICS COMPANY has moved its eastern sales office to 32 Green Street in Newark, New Jersey . . . TRIAD TRANSFORMER MANUFACTURING CO. has opened its new plant at 4055 Redwood Avenue in Venice, California. The company recently celebrated its 6th anniversary . . . WESTINGHOUSE **ELECTRONIC TUBE DIVISION** is now in production at two new tube plants in Elmira and Bath, New York. Virtually all types of tubes will be produced in the two new facilities . . . INTERNA-TIONAL RESISTANCE COMPANY of Philadelphia has purchased 66.4 acres

in Asheville, N. C. and will construct a \$200,000 plant for the purpose of expanding the company's manufacturing facilities . . . RADIO CITY PRODUCTS CO., INC. has moved all of its test equipment production to its Easton, Pa. plant. The engineering, sales, purchasing departments, and the general offices will remain in New York . . . STRONGHOLD SCREW PRODUCTS, INC. has purchased a one-story, 80,000 square foot factory building at 1801 W. Winnemac Avenue, Chicago. The company plans to take possession by April 1, 1953.

THE CINCINNATI SECTION of the Institute of Radio Engineers is sponsoring the Seventh Annual Spring Technical Conference which will be held in Cincinnati on April 18th.

R. W. Lehman, Baldwin Piano Company, 1801 Gilbert Avenue, Cincinnati, Ohio is in charge of exhibits and advertising in connection with the conference. Reuben Nathan, Crosley Division, Avco Manufacturing Corporation, 1329 Arlington Street, Cincinnati 25, Ohio is in charge of publicity.

A diversified program of papers is being planned by the committee in charge.

BERNARD L. CAHN, since 1949 general sales manager of the Insuline Cor-



porution of America, has been elected vice-president of the company. He assumed his new duties on December 1st of last year.

A graduate of New York University where he majored

in business administration and management, Mr. Cahn joined *Insuline* in 1946 after four years of Army service. Entering as a private and emerging as a major, he spent twenty-seven months in the European Theater of Operations.

As assistant to the president and then as sales manager, he has traveled widely throughout the U.S. and is well known in the electronic parts business. He is a member of the Show Corporation Board, the organization responsible for the annual Parts Show.

B & L RADIO AND TV SUPPLY has recently been opened in Lubbock, Texas to wholesale electronic parts. E. W. Bland and Ogle T. Lemon are partners in this new venture . . . Announcement of the formation of the HIGH VACUUM EQUIPMENT CORPORATION has been made by Joseph B. Merrill, president and general manager of the firm. The general offices and factory of the com-

24

RADIO & TELEVISION NEWS

AMAZING NEW TRAINING PLAN

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EXTRA FEATURES THAT MEAN MORE MONEY FOR YOU!

Thousands of new job opportunities will be available for you right in your own state, now that the govern-ment has lifted restrictions on new TV stations. My simple, successful methods can PREPARE YOU NOW to and Electronics industries...help you get the success and happiness that you always wanted out of life. You learn the practical, easy way by using actual parts and equipment in the 15 big Radio-TV kits I send you, including a COMPLETE TV RECEIVER... yours to build and keep.

My Advanced Training Prepares You For Better Jobs Then, atter you finish your training for a position as a full-fledged TV Technician—where you can write o tull-fledged IV Technician—where you can write your own ticket and choose from dozens of fascinating careers—I don't stop there! I continue to train you—AT NO EXTRA COST—to qualify for even better pay in the BETTER JOBS that demand FCC licenses.

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PREPARES YOU AT HOME FOR YOUR

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REQUIRE AN FCC LICENSE en to every student at NO EXTRA COST after Theory and Practice is completed. SET-UP YOUR OWN HOME LABORATORY WITH THE 15 BIG TELEVISION-RADIO KITS WE SEND YOU (At No Extra Cost)

YOU BUILD AND KEEP ALL THESE UNITS



Big TV Tube

Advanced FM-TV Training For Men Who Know Radio

COMPLETE theory and practical training course . . . complete with kits including large screen TV receiver.

FCC License Coaching Course Included FREE.

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MY SCHOOLS FULLY APPROVED TO TRAIN VETERANS UNDER NEW G.I. BILL! If discharged after June 27, 1950—CHECK COUPON BELOW! Also approved for RESIDENT TRAINING in New York City . . . qualifies you for full subsistence allowance up to \$160 per month.



Dept. T-2

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"As Merchant Ship Radio Omcer. I receive \$867. For 40-day trip. Your training helned me get this fine position."

Stanley Mawrocki

"Your excellent instruc-tion helped me get my present joh as an air-nort Airlines."

Eugene E. Basko

I now hold a fine air-lines position at La-Guardia Field, New York City, thanks to your ex-training."

— Joseph Rosenberg

"Thanks to your training. I qualified for a good job as a Receiver Tester at Federal Tele-and Radio."

Paul Frank Seier

Many others working at NBC, RCA, CBS, Dumont, Philos.
Emerson, Admiral and other leading firms.

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Address			

Zone State City

I am interested in: Radio-TV Advanced PM-TV VETERANS. If qualified under new G.I. bill, check here Resident Study -------------



Customers judge your service by the results they get. If a radio or TV repair job fails to stand up, they blame you, not the parts you used.

Don't jeopardize your business reputation with "just-as-good" replacement parts. OHMITE resistors provide an extra margin of safety. You can depend on these quality resistors—wire-wound or composition—to give years of trouble-free service.

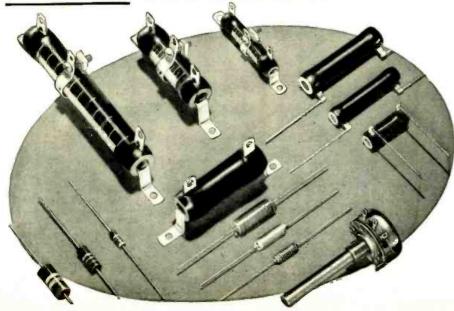


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DEPENDABLE RESISTANCE UNITS



pany are located at 349 Lincoln Street, Hingham, Mass. The company will specialize in the development, design, and manufacture of high vacuum equipment used in the fields of electronics, metallurgy, plastics, and metals . . . ELECTRO-VOICE, INC. of Buchanan, Michigan has purchased RADIO MFG. ENGINEERS, INC. (RME), nineteen-yearold amateur communications equipment firm. The subsidiary company will remain under the present management of E. G. Shalkhauser and Russ Planck and all RME business will be conducted from the company's Peoria. plant . . . LEWIS AND KAUFMAN, INC. has changed its name to LEWIS AND KAUFMAN, LTD. The change is concurrent with the absorption of personnel and facilities of the 20.000 square foot Satiocy, California plant of PACIFIC ELECTRONICS . . . LOUIS BROS., West Coast television antenna manufacturer, has formed a new division called CON-CERT HALL. This division will manufacture bass reflex cabinets, speaker baffles, and television cabinets. The company is located at 3543 E. Sixteenth Street, Los Angeles 23, California . . . CROSLEY DIVISION has contracted to purchase the manufacturing facilities of the tube divisions of SAR-KES TARZIAN, INC. at Batavia, Illinois. The plants produce television picture tubes and miniature receiving tubes ... ACME ELECTRONICS, INC. is the new name of PEERLESS ELECTRONICS DISTRIBUTORS, INC. The firm will continue to do business at 74 Willoughby Street in Brooklyn where it has been located for the past 5 years.

FRED J. LEMKE has been appointed operating manager at the Akron, Ohio

headquarters of Olson Radio Warehouse.

Mr. Lemke was formerly Merchandise Division Superintendent for mail order at Montgomery Ward and Company, an association

which lasted for more than eighteen years.

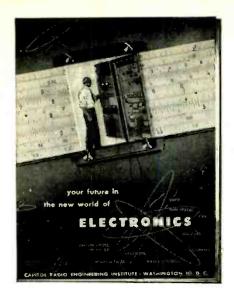
In his new post he will be responsible for expediting the handling of all mail orders received by the Ohio parts firm.

JULIUS HABER has been appointed director of public relations for the RCA Victor Division of Radio Corporation of America, succeeding JAMES M. TONEY who has been appointed director of consumer products distribution

... Sangamo Electric Company has made three new appointments in its Capacitor Division which are of interest to the industry. WILLIAM W. TAYLOR has heen named assistant sales manager, BRUCE E. VINKEMULDER is the new sales promotion manager, while A. E. McCLUSKEY is now serving as distributor sales manager. All of these men will make their headquarters at the company's Marion. Illinois plant

(Continued on page 90)

RADIO & TELEVISION NEWS



How far ahead can you be next year...

IN TV AND ELECTRONICS?

Send for this free CREI booklet today . . .
 and find out!

THIS BOOKLET can mean the difference between small, w-i-d-e-l-y s-p-a-c-e-d salary increases—and rapid advancement. Between routine work—and challenging opportunity. Between constantly defending your job against better-trained men—and dynamic confidence. Between short-circuited hopes—and high-powered ambition.

An exciting new world has opened up with such superspeed that even the most optimistic electronic experts fall short in their predictions of expansion.

Think of the 1,110 TV stations now on the air and the 2,500 stations made possible by the FCC unfreeze. Think of the over 18,000,000 TV sets now in use. That's 5,000,000 more than we were supposed to have by 1954. Think of the 100,000,000 radios in current operation. (95% of the nation's homes have one or more sets.) Think of the tremendous defense orders now being placed for electronic equipment and installations.

Think of the thousands of radio-equipped fire and police departments throughout the U.S. Of the many radio-equipped railroads, of the hundreds of cities with 2-way radio service for cars and cabs. Think of the wide-ranging field of aviation communications—radio-controlled aircraft, navigation-and-traffic control, airport stations.

Think of the maritime world with its navigational aids, fathometers, ship-to-shore and ship-to-ship communications and radar. Think of electronic heating, fax and ultra-fax, of electronic medicine, and all the other applications of electronic know-how.

Countless positions must be filled—in development, research, design, production, testing and inspection, manufacture, broadcasting, telecasting and servicing. Who will get those positions? You—if you prepare today—if you are alert and have the ambition to advance your knowledge. You—if you take 2 minutes to send for a free copy of "Your Future in the New World of Electronics."

This helpful book shows you how CREI Home Study leads the way to greater earnings through the inviting opportunities described above.

However, being an accredited technical school, CREI does not promise you a "bed-of-roses." You have to translate your willingness to learn into saleable technical knowledge —via study. Since its founding in 1927, CREI has provided thousands of professional radiomen with technical educations. During World War II, CREI trained thousands for the Armed Services. Leading firms choose CREI courses for group training in electronics at company expense, among them United Air Lines, Canadian Broadcasting Corporation, Trans Canada Airlines, Bendix Products Division, All-American Cables and Radio, Inc., RCA-Victor Division, and the Machlett Laboratories.

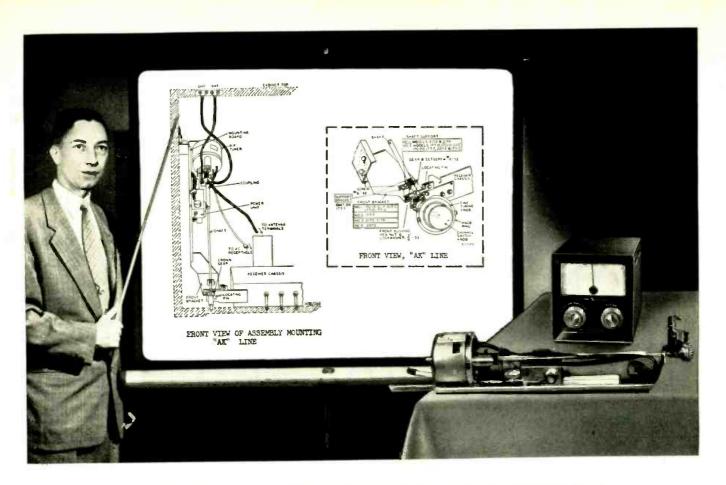
CREI courses are prepared by recognized experts, in a practical, easily-understood manner. You get the benefit of time-tested materials, under the personal supervision of a CREI Staff Instructor. This complete training is the reason why CREI graduates find their diplomas keys-to-success in Radio, TV and Electronics. CREI alumni hold top positions in America's leading firms.

At your service is the CREI Placement Bureau, which finds positions for students and graduates. Although CREI does not guarantee jobs, requests for personnel currently exceed supply by far.

Talk to men in the field and check up on CREPs high standing in electronics instruction. Determine for yourself right now that your earnings are going to rise with your knowledge—and that you get your rightful place in the Age of Electronics. All this CREI can promise you, provided you sincerely want to learn. Fill out the coupon and mail it today. We'll promptly send you your free copy of "Your Future in the New World of Electronics." The rest—the future—is up to you.

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February, 1953



GENERAL ELECTRIC ANSWERS YOUR QUESTIONS ON UHF SERVICE

G-E Field Engineers are holding UHF clinics throughout the country—open to all TV servicemen—without charge.

V servicemen in practically every area will soon face problems connected with UHF. General Electric technicians from Electronics Park are now holding UHF field clinics all over the country.

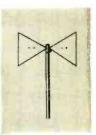
The G-E field men will explain continuous tuner converters, switch channel converters, turret head-end conversions-the various kinds of UHF antennas, where they should be used, their installation.

You will see how to install and adjust various kinds of UHF tuners -for new and older sets. With the knowledge you gain from these G-E UHF Field Clinics-you'll be prepared to handle all kinds of UHF service.

Get in touch with the TV service manager at your General Electric TV distributor's right away. Tell him to sign you up for the first clinic that hits your area.

General Electric Company, Receiver Department, Syracuse, New York You can put your confidence in_ GENERAL (28) ELECTRIC







UHF Broad Band Stacked "V"Antenna



UHF Six Element Yagi Antenna

RADIO & TELEVISION NEWS



Here's the hardest-selling, custom-made Home Calendar ever offered to Radio-TV Service Dealers! It's tailor-made just for you! Features an appealing illustration painted exclusively for Sylvania by a famous cover artist. Reproduced in full color and imprinted with your name and address.

Your prospects simply can't overlook this calendar. It's filled with timely hints and valuable household suggestions they'll want to keep handy. And, every time they turn the page they'll be reminded of your dependable service, skill, and experience.

Order now...supply limited! At only 11/2¢ per customer per month (in lots of one hundred or more), this calendar

is truly the smartest advertising buy ever offered. But don't delay, the supply is limited! Order a couple of hundred from your regular Sylvania distributor... TODAY! If he is out of stock, write to: Sylvania Electric Products Inc., Dept. 3R-2102 1740 Broadway, N. Y. 19, N. Y.

SYLVANIA



RADIO TUBES; TELEVISION PICTURE TUBES; ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT; FLUORESCENT TUBES, FIXTURES, SIGN TUBING, WIRING DEVICES; LIGHT BULBS; PHOTOLAMPS; TELEVISION SETS

February, 1953

29

FAR BETTER RECEPTION WEVERY LOCATION with Sensational New

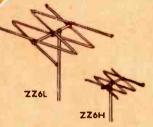
Patent Pend

TV ANTENNAS

SUBURBAN MODELS

ZZ6A

Models ZZ4A and ZZ6A give you all-channel (2 thru 13) reception in ONE SINGLE BAY ANTENNA. The Model ZZ4A has excellent gain and is designed for suburban areas. Model ZZ6A has even greater gain and provides excellent all-channel reception in near fringe greas.



NEAR FRINGE MODELS

For near fringe area reception, the Models ZZ6L and ZZ6H are recommended. Model ZZ6L covers Channels 2 thru 6, Model ZZ6H is for Channels 7 thru 13. Both antennas offer high gain with patterns and front-to-back ratios similar to cut-to-channel yagis.

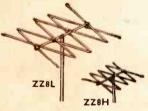
The TRIO Rotator is America's most dependable — has two powerful 24

volt motors — one for each direction of rotation. Absolutely weather-proof, permanently lubricated. All motors, shafts and gears mounted on

From ultra-ultra fringe to metropolitan areas, the sensational new TRIO ZIG-ZAG TV Antennas are providing clear, enjoyable TV pictures.

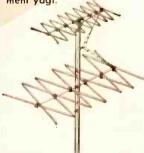
Enthusiastic reports are pouring in from across the nation, testifying to the high efficiency of the new, exclusive TRIO ZIG-ZAG TV Antenna design.

Yes, results — not mere claims —
have made the TRIO ZIG-ZAG America's
most wanted TV antenna!

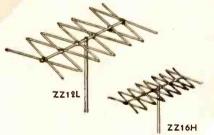


FRINGE MODELS

Models ZZ8L and ZZ8H were designed for normal fringe area reception and provide clear, snow-free pictures. Forward lobe patterns and front-to-back ratios are similar to a good single channel, multi-element yagi.



ZZ12L and ZZ16H are stacked for all VHF Channel Reception



ULTRA FRINGE MODELS

The extremely high gains of the ZZ12L and the ZZ16H models provide unequalled reception in ultra-fringe areas. Model ZZ12L covers Channels 2 thru 6 and Model ZZ16H, Channels 7 thru 13. These two models when stacked, are fed with only one 300 ohm line and provide ALL VHF CHANNEL RECEPTION. Line match is excellent and front-to-back ratios are unusually high.

* To provide even greater strength, TRIO Antennas now have stamped steel element clamps.



TRIO MANUFACTURING COMPANY

GRIGGSVILLE, ILLINOIS

RADIO & TELEVISION NEWS

BUY DIRECT AND SAVE

Sweeping the Country!

TUNERS 'PRE-FAB' RECEIVERS AUDIO PRODUCTS CO.

Collins Audio Products Co. is in no way affiliated with Collins Radio Co.

Two ALL NEW Complete Kits for Every High-Fidelity Need



The FM-11 tuner is available in kit form with the IF Amplifier mounted in the chassis, wired and tested by us. You mount the completed RF Tuning Unit and power supply, then after some simple wiring, it's all set to operate. 11 tubes: 6J6 RF amp, 6AG5 converter, 6C4 oscillator, 6BA6 1st IF, (2) 6AU6 2nd and 3rd IF, (2) 6AU6 limiters, 6AL5 discriminator, 6AL7-GT double tuning eye, 5Y3-GT-rectifier. Sensitivity 6 to 10 microvolts, less than 1/2 of 1% distortion, 20 to 20,000 cycle response with 2DB variation. Chassis dimensions: 1212" wide, 8" deep, 7" high. Illustrated manual Each Collins Tuner Kit is complete with punched chassis, tubes, power transformer, power supply components, hardware, dial assembly. tuning eye, knobs, wire, etc., as well as the completed sub-assemblies: FM tuning units, AM tuning units, IF amplifiers, etc., where applicable. Since all these sub-assemblies are wired, tested and aligned at the factory, Collins Pre-Fab Kits are easily 'assembled even without technical knowledge. The end result is a fine, high quality, high fidelity instrument at often less than half the cost — because you helped make it and bought it direct from the factory. Bring your present reproducing system up to date with a new Collins Tuner.



FM/AM Tuner Kit

\$7750

The original 15 tube deluxe FM/AM pre-fab kit redesigned on a smaller chossis. The tuner now measures 14" wide by 12" deep by 71/2" high. This attractive new front and dial assembly opens up new applications where space is at a premium. Kit includes everything necessary to put it into operation—punched chassis, tubes, wired and aligned components, power supply, hardware, etc. Kit comprises FMF-3 tuning unit, IF-6 amplifier, AM-4 AM tuning unit, magic eye assembly and complete instructions. All tubes included. Shipping weight 19 lbs.

Selected Basic Components For Special Applications



FMF-3 Tuning Unit

supplied. Shipping weight 14 lbs.

\$1525

IF-6 Amplifler

\$1975



AM-4 Tuning Unit

The best for FM. The most sensitive and most selective type of "front end" on the market. The best for FM. The most sensitive and most selective type of "front end" on the market. 6 to 10 micravolts sensitivity. Image ratio 500 ta 1. 6J6 tuned RF stage, 6AG5 converter, 6C4 oscillator. Permeability tuned, stable and drift-free. Chassis plate measures 6½"x4½". In combination with the IF-6 amplifier, the highest order of sensitivity on FM can be attended. Tubes included as well as schematic and instructions. Draws 30 ma. Shipping weight FMF-3: 2½ lbs. Dial available @ \$3.85 A remarkable value! 6 tubes are used in the IF amplifier: 6BA6 1st IF, (2) 6AU6 2nd and 3rd IF's, (2) 6AU6 limiters and 6AL5 discriminator. High gain, wide-band response (200 KC) for highest fidelity. 20 to 20,000 cycles. Distortion less than 1/2 of 1%. Draws 40 ma @ 220 volts. Chassis plate dimensions: 11-5/16"x2½" Shipping weight: 3 lbs.

Tops in AM superhet performance! A 3-gang Tops in AM superhet performance! A 3-gang tuning condenser gives 3 tuned stages with high sensitivity and selectivity. Assembly is completely wired, tested and aligned ready for immediate use. Frequency coverage 540 KC to 1650 KC at a sensitivity of 5 microvolts. Tubes 68A6 RF amplifier; 68E6 converter; 68A6 IF amplifier ond 6AT6 detector. Draws 30 ma @ 220 volts. Mounts on a chassis plate measuring 4"x736". Shipping weight 2½ lbs. Dial availping weight 21/2 lbs. Dial available at \$3.85. MAIL



RD-1C Tuner & Dial

The COLLINS RD-IC FM tuner chassis is unique in the field. A whole, compact FM tuner and dial that fits in the palm of your hand. Canvert AM sels to FM/AM receivers for only of your hand. Canvert AM sels to FM/AM receivers for only a few dollars! Unlimited applications where space is at a premium. Use in conjunction with your phonograph amplifier. Full frequency response to 20,000 cycles. Sensitivity 20 microvolts, permeability tuned. Tuning unit and IF amplifier on the same chassis plate. Drows 40 ma 100 volts. Tubes: 6AG5 converter, 6C4 oscillator, (2) 6AU6 IF amplifiers, 6AL5 in new ratio detector circuit. Shipping weight tuner and dial 5 lbs.

To: Collins Audio Products Co. Inc. P.O. Box 368, Westfield, N. J. Tel. WEstfield 2-4390	
☐ FM Tuner Kit ☐ FM/AM Tuner Kit ☐ Slide Rule Dial Assembly ☐ FMF-3 Tuning Unit ☐ IF-6 Amplifier ☐ RD-IC Tuner and Dia ☐ AM-4 Tuning Unit	
NAME	
ADDRESS	
CITY	
Amount for Kit \$ See weights, odd shipping cost \$	
Total amount enclosed \$ Check Money Order	

YOU THINK OF TUNERS, THINK OF COLLINS AUDIO PRODUCTS WHEN

February, 1953



New "500" telephone. It has already been introduced on a limited scale and will be put in use as opportunity permits, in places where it can serve best. Note new dial and 25 per cent lighter handset.

It adds miles to your voice

For years the telephone you know and use has done its job well—and still does. But as America grows, more people are settling in suburban areas. Telephone lines must be longer; more voice energy is needed to span the extra miles.

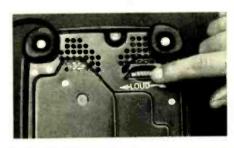
Engineers at Bell Telephone Laboratories have developed a new telephone which ean deliver a voice ten times more powerfully than before. Outlying points may now be served without the installation of extra-heavy wires or special batteries on subscribers' premises. For shorter distances, the job can be done with thinner wires than before. Thus thousands of tons of copper and other strategic materials are being conserved.

The new telephone shows once again how Bell Telephone Laboratories keeps making telephony better while the cost stays low.

BELL TELEPHONE LABORATORIES

Improving telephone service for America provides careers for creative men in scientific and technical fields.





Adjustable volume control on bottom of new telephone permits subscriber to set it to ring as foudly or softly as he pleases. Ring Is pleasant and harmonious, yet stands out clearer.

QUICK FACTS ON NEW TELEPHONE

Transmitter is much more powerful, due largely to increased sound pressure at the diaphragm and more efficient use of the carbon granules that turn sound waves into electrical impulses.

Light ring armature diaphragm receiver produces three times as much acoustic energy for the same input power. It transmits more of the high frequencies.

Improved dial mechanism can send pulses over greater distances to operate switches in dial exchange.

Built-in varistors equalize current, so voices don't get too loud close to telephone offices.

Despite increased sensitivity of receiver, "clicks" are subdued by copper oxide varistor which chops off peaks of current surges.

RADIO & TELEVISION NEWS



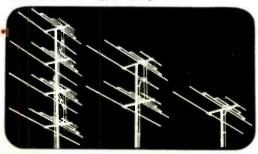
The Finest All-Channel Antenna



Secret of the Q-Tee all-channel operation is the patented printed circuit electronic channel separator in this colorful red plastic housing. Lic. A.A. K. Pats. 2,422,458; 2,282,292; 2,611,086, others pending.

Easy stacking makes the Q-Tee a pleasure to install especially when in combination with new UHF antennas. Three series. Q-Tee single hay for primary areas, Q-Tee double (two-bay) for near-fringe areas; Q-Tee quad (four-bay) for fringe areas.

There is only one Q-Tee! It's powerful — it's revolutionary — it's patented — it's made only by Vee-D-X. Embodying an entirely new engineering approach to all-channel reception, the Q-Tee has met with sensational success. Its brilliant performance, ease of installation, ease of stacking and clean-cut appearance have won for it the reputation of "Antenna of the Year". Ideal for all multi-channel areas (primary, near-fringe and fringe), the Q-Tee provides the high front-to-back ratio found in no other broadband antenna. In areas of co-channel interference this often means the difference between a good picture and none at all. The Q-Tee is an excellent basic VHF antenna for use in combination with UHF antennas.

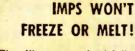


THE	LaPOINTE-PLASC	OMOLD CORP	ORATION
	ROCKVILLE,	CONNECTICUT	N-2

☐ Send full information on Q-Tee		
NAME		
STREET		
CITY ZONE STATE		

February, 1953





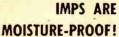
They'll operate faithfully in temperatures ranging from -40°C. to +100°C. (212°F.)—and that's the boiling point of water!





IMPS ARE REALLY RUGGED!

The tough thermo-setting
plastic will take an
astounding amount of abuse
—yet IMPS will still look
and perform like new!



No moisture can get through the varnished plastic case, or even through the lead onchor points.





IMP LEADS CAN BEND AND BEND!

Tinned leads that are really securely anchored—you'll be amazed at how much punishment they'll take without breaking!

All over the country service-engineers are praising the newest and finest molded tubular paper capacitor—the Pyramid IMP!

IMPS are available in all popular ratings in 200, 400 and 600 volt ranges. See your local distributor.

For free, attractive catalog on IMPS, write Dept. RI

PYRAMID ELECTRIC COMPANY

1445 HUDSON BOULEVARD . NORTH BERGEN, NEW JERSEY

BUILD THIS TRANSISTOR RECEIVER

ROBERT K. DIXON

Receiving Tube Division
Raytheon Manufacturing Company

A BOUT four years ago, the transistor was first announced. Since that time, a considerable amount of effort has gone into the design and production of transistors and much has been written about them.

Transistors are semiconductor devices capable of acting as amplifiers, oscillators, and performing other functions now performed by vacuum tubes and with greater efficiency. The basic material in most transistors today is germanium and the devices are made in two different types: the point contact, which was the original, and the junction.

A semiconductor is any material which is neither a good conductor nor a good insulator, thus its name. Germanium has a simple atomic structure with the inter-atomic spacings in the crystals forming relatively straight corridors or paths. The basic lattice of the crystal has eight atoms per cell, four of which form the corners of a small cube while the other four are wholly within the cube. There are relatively large spaces between the atoms. In this pure form germanium is basically a stable material and does not exhibit a surplus or deficiency of electrons.

By the introduction of certain selected elements, the germanium can be made to exhibit an excess of electrons and thus become a negative or "n" type material, or by the introduction of other impurities or chemical elements there may be a deficiency of electrons and the material will be considered a positive or "p" type material.

If electrical pressure is applied to a piece of "n" type germanium material, current flow will exist by virtue of the free electrons existing therein. Similarly, if electrical force is applied to the positive type material, conduction appears by virtue of the phenomenon

Transistors are now within the reach of all. Here is a simple receiver you can build—other types of equipment using transistors will be covered in subsequent issues.

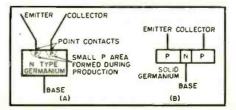
called hole conduction. The application of electrical potential causes electrons to move from the negative and toward the positive end, the presence of holes facilitating the electron flow.

The point-contact transistor consists

Editor's Note: Obviously no attempt has been made to "miniaturize" this unit. It is more important to familiarize oneself with the design and limitations of transistors. Miniaturization is then not too difficult a task. These transistors are new items; however, they are available at a suggested retail price of \$7.60.

of a block or crystal of material such as germanium with two properly spaced pointed electrodes making contact with the surface of the germanium. In many respects, it resembles the well-known crystal diode with the exception of the additional electrode. During manufacturing, the position of the two point contact electrodes (including the relative spacing of these elements) is adjusted for proper operation of the transistor as an amplifying device.

Fig. 1. Internal construction of the (A) point contact and (B) junction transistor.



The basic block of germanium is normally "n" type in the point-contact device. Small areas of the germanium adjacent to the pointed electrodes are converted to "p" type material during production. (See Fig. 1A.)

Over-all view of the experimental broadcast receiver. Although two transistors were used the

circuit can be built with a single unit.

Junction transistors consist of a block of material in which "n" and "p" type materials are arranged in alternate layers. The end sections can be either "n" or "p" material with the center zone being the opposite type. (See Fig. 1B.)

The point-contact transistor finds wide application in switching circuits and oscillator circuits at frequencies normally not possible with the junction type units. The point-contact transistor has inherently higher noise output than the junction units.

The junction transistor, on the other hand, is a more efficient amplifier while operating at low voltages. They are extremely rugged and have exceptionally long life. The normal noise voltage generated in a junction type is lower than that of the point-contact type transistor. Since the electrons travel somewhat slower through the germanium material in transistors than in a vacuum and due to the high internal capacities of junction transistors as we know them today, operation is normally limited to the lower frequencies.

This article deals with a "p-n-p" junction transistor recently announced by the Raytheon Manufacturing Com-

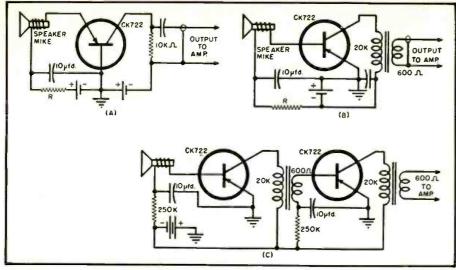


Fig. 2. Microphone preamplifiers using transistors. (A) grounded base. (B) grounded emitter. and (C) a two-stage, transformer-coupled amplifier. See text for details.

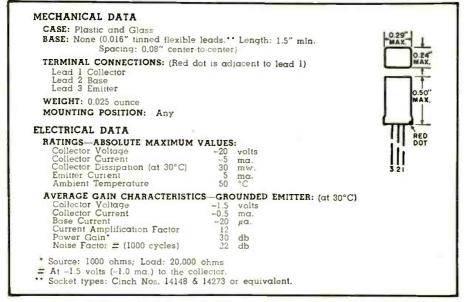


Table 1. Tentative data on the Raytheon CK722 germanium junction transistor.

pany, identified as the CK722. The characteristics and ratings of the CK722 are shown in Table 1. It is extremely rugged and when operated at normal ratings has exceptionally long life.

Basically, the "p-n-p" junction transistor may be compared to the vacuum tube with the emitter resembling the cathode, the base resembling the grid, and the collector resembling the plate. There are several basic differences, however, which are outstanding.

In the "p-n-p" junction transistor,

conduction is accomplished in a solid instead of in a vacuum. The collector is operated with a negative bias instead of the customary positive voltage applied to the plate. Another outstanding difference lies in the input impedance. The vacuum tube has almost infinite input impedance over a considerable range of frequencies. The transistor, on the other hand, is a current-operated device and has a rather low input impedance in the grounded base or grounded emitter connection which is analogous to the

grounded grid and grounded cathode type amplifiers.

The graphic symbol for the "p-n-p" junction transistor is shown in Fig. 3. Since the transistor is a three-terminal device, several combinations of connections may be used, namely, the grounded emitter, the grounded base, and the grounded collector.

Fig. 5 is a typical set of characteristic collector curves for the CK722. These curves may be compared to the plate characteristics of a pentode amplifier except that instead of grid voltage we use various values of base current. A load line of 1000 ohms has been drawn in and examination of the curve will show that operation is linear over almost the full range from zero to maximum collector current, The slow increase in collector current with increasing collector voltage at any fixed value of base current is typical of junction transistors and is indicative of the high collector resistance.

An additional characteristic which is little known but of considerable importance is the "Zener" effect. If the transistor is operated with positive base current so that normally there is no collector current, the collector voltage can be increased to a point where conduction will occur. This is the "Zener" point and may be an important consideration in operation of transistors. "Zener" current flowing during the peak a.c. voltage cycle could cause excessive limiting and consequent high distortion in an amplifier.

Many applications for the CK722 junction transistor will become apparent to the experimenter. Since junction transistors had up to now been available on only a limited basis, very little application and circuit work has been done.

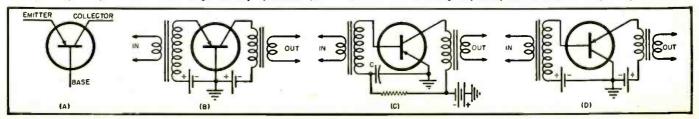
Three basic type circuits immediately suggest themselves. These are: switching circuits, oscillator circuits, and amplifier circuits.

We shall discuss in some detail, the CK722 as a small-signal, low-voltage amplifier.

The small size and relatively high efficiency at low operating voltage coupled with the absence of any heater voltage make the transistor ideally suited for preamplifier use. A further advantage is the fact that transistors are not microphonic, thus no special precautions in mounting need be taken.

Fig. 2 includes several suggested circuits for transistors used as microphone preamplifiers. The microphone

Fig. 3. Equivalent graphic circuits. (A) Graphic symbol of CK722 "p-n-p" junction transistor. (B) Common base amplifier, with low input impedance and high output impedance. Requires two batteries. (C) Common emitter circuit having medium input impedance and high output impedance. Permits single battery operation. (D) Common collector with high input impedance and low output impedance.



may be a small 2 or 3 inch dynamic speaker. Notice that it is directly connected to the transistor without use of an impedance matching transformer. With a voice coil impedance of 6 ohms and with R adjusted for a collector current of 100 microamperes. the sensitivity will be approximately equal to a good carbon mike with much better fidelity and less noise. The circuit of Fig. 2B may be used to eliminate the need of a tapped battery, however, the gain will be slightly less. If a long shielded cable is required, a transformer should be used instead of a resistor load in the collector of the transistor as in Fig. 2B. This can be a small plate-to-line transformer of 20,000/600 ohms impedance.

Because the operating current is low, battery life is good. The supply for the transistor can be obtained from the standard high voltage plate supply of the amplifier and, in fact, this circuit has the advantage of supplying a more constant current to the transistor. The important factors in these circuits are the low input impedance of the emitter, on the order of 100 ohms with the grounded base connection, and the high output impedance of the collector, on the order of 500,000 ohms. With grounded emitter connection, the input impedance of the base is a function of other operating parameters so no value can be given for it.

Several stages of transistor amplifiers can be cascaded and the use of coupling transformers will assure maximum gain. Plate-to-line transformers may be used as shown in Fig. 2C. Resistance coupling can be used but with some loss in gain (approximately 6 db). Large coupling condensers must be used to obtain good low frequency response because of the low impedance levels.

Push-pull operation of transistors is entirely feasible, permitting greater power dissipation with consequent greater power output. Class A operating efficiencies on the order of 50 percent are obtainable while class B operating efficiencies to nearly 80 percent are possible. Matched units should be used in this application and degeneration can be applied to improve performance.

The audio amplifier type operation lends itself admirably to a simple broadcast receiver. To investigate this application more thoroughly, such a receiver has been built. For those interested in duplicating it, a description follows:

Transistor Receiver

One or two transistors may be used in this receiver (Fig. 4.). The first unit is utilized as a detector/amplifier. The second transistor is connected as a grounded emitter amplifier.

The first unit is capable of delivering adequate earphone volume so that the second stage can be eliminated if it is desired to reduce the cost of the receiver. Although the experimental receiver shown has been built on

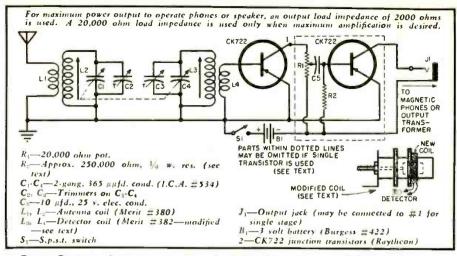


Fig. 4. Diagram of transistor receiver. A single unit may be used if desired. See text.

metal, obviously it could be built using a wooden case without affecting its performance.

In the Boston area where this receiver has been operated, the two tuned circuits have given more than adequate selectivity to separate the local stations. An antenna of 50 feet and a good ground made possible reception of stations over approximately a 15 mile radius. The importance of a good antenna and ground, particularly in an area somewhat remote from high power broadcast stations, cannot be overemphasized.

The two circuits are coupled through mutual coupling existing by physically placing the coils close together, one inch separation center-to-center is recommended. The detector coil must be modified to connect to the transistor detector/amplifier. The antenna coil portion of the *Merit* type 382 should be carefully removed. It can be slid off the end of the form without damage to the coils after unsoldering the leads. The wire from this antenna coil may be used to scramble wind 50

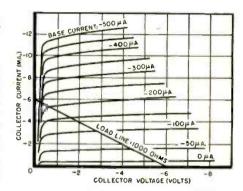


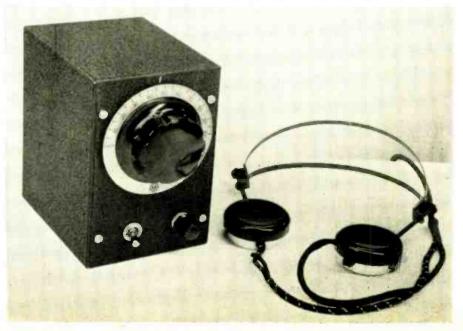
Fig. 5. I /E /Ib curves for the CK722.

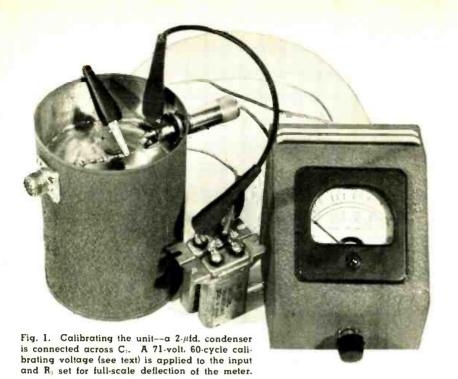
turns on the 382 form, tight against the first pi of the tuning coil. (See Fig. 4). This detector coil can be cemented in place with a good coil dope, such as *Amphenol* 912.

The amplifier is connected in the grounded emitter type circuit. The advantages of this circuit are that only one battery is required and that it has a higher input impedance than the

(Continued on page 132)

Over-all view of the experimental transistor receiver showing accessory headphones.





Your rig's r.f. output, not the rated d.c. input, is the important factor. Old Timer and Novice can make good use of this simple direct-reading output meter.

N ALMOST any ham shack, Novice or otherwise, there comes a time when the operator wishes for a simple means of checking the output of his rig to determine whether it is op-

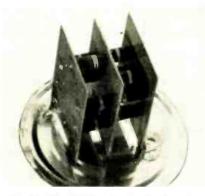


Fig. 2. The 50-ohm load, showing the twelve 150-ohm resistors connected in series-parallel. The plate on the left is soldered to a feedthrough on the can lid. The right-hand plate is grounded

erating as efficiently as it should. The wattmeter described here is the result of such a desire at W9OCL. It will be particularly useful to the Novice in helping him to get acquainted with the factors involved in amplifier efficiency.

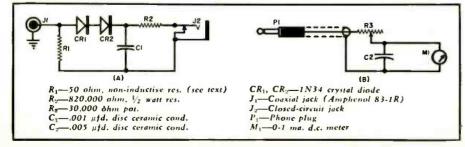
Aside from simplicity of calibration, two other requirements were considered to be desirable. These were a 100-watt dissipation rating and a comparatively flat load up to 30 mc.

Although the metering circuit is good up to approximately 40 mc., the voltage standing wave ratio of the load has been measured up to 400 mc. and found to be less than 1.5. If a wattmeter is needed for higher frequencies it would be simple to substitute another metering circuit for the one shown in the circuit diagram. The metering circuit here was chosen because of the fewer parts required and its ability to read power at 60 cycles as well as at 30 mc.

The 100-watt dissipation requirement was satisfied by using twelve

150-ohm, 2-watt Allen Bradley resistto the lid by an L-shaped piece of metal.

Fig. 3. (A) Wiring diagram of oil-cooled load assembly. (B) Meter-case assembly.



OIL-COOLED LOAD WATTMETER

ROBERT M. SEE. W9OCL/5

ors in series-parallel, cooled by being immersed in ordinary #10W motor oil.

Mechanical Construction

A general idea of the construction of the wattmeter can be seen by studying the photographs. The "chassis" is simply a one-quart motor oil can. Save the oil so it may be used later. When opening the can of oil use an opener which will cut smoothly so that the lid will fit comfortably inside the can. Later this lid will be soldered into place to form a completely sealed oil-cooled load, so clean the can well.

The twelve 150-ohm resistors are mounted between three thin brass plates in a sandwich-like manner, six in each "deck." Each deck will then have a resistance of 25 ohms, and the two decks in series a resistance of 50 ohms. The three 2% x 1% inch plates are used for mechanical support and electrical bond. To keep the lead inductance to a minimum, holes are drilled into the plates just large enough to slip in the resistor leads. In this way only a one-eighth inch lead is used. The resistors are fitted flush with the plates and soldered into place. Fig. 2 shows the resistor load in its finished form.

Now the total resistance between outside plates will be approximately 50 ohms. One of the outside plates may be electrically joined to the oilcan lid by soldering a strong L-shaped piece of metal to the plate and lid. This junction should be made so that the lid is suspended above the 50-ohm load about one-half inch. The other outside plate of the load may be connected to a feedthrough insulator which is mounted on the lid.

Fill the oil can about two thirds full of the #10W motor oil and slip the 50-ohm load down inside until it is about half an inch from the bottom of the can. Make certain that the oil completely covers the resistors of the load but leaves some air space helow the lid. The lid should now be soldered to the inside of the can to form a good electrical contact as well as a leakproof seal.

The foregoing will take a little care. To find that half-an-inch of elearance it is best not to try to use a half-inch piece of wood or other material, even as a temporary spacer, because once you have placed the 50-ohm load in the can it may be very difficult to get it out again. Of course, no spacer is used in the finished unit. Sliding the can lid in and out also produces wear and the lid may refuse to stay in place when you finally try to solder it.

Do your measuring and marking with a ruler and avoid any temptation to measure by "eye 'n' try" although

it may seem quicker.

When you pour the oil, pour it gently into the center, because if the sides are oily, they will not take solder. Use as large a soldering iron as pos-

sible for this job.

These points may seem elementary but many hams learn their construction techniques through unhappy experience and these suggestions are intended as tips for the novice who may not have had too much shop work.

None of this is to imply that the work is ticklish, but it should be carefully done and well organized.

The r.f. input is brought into the load by means of a coaxial connector. It should be placed so that the lead to the feedthrough insulator will be as short as possible. A hole is cut on the other side of the can for a closed-circuit type of phone jack. Between the coax connector and the jack are connected the two 1N34 crystals and R_2 in series. These should be placed so that the leads will be as short as possible. C_1 should be a disc type ceramic condenser which is wired into the circuit with a minimum lead length.

The 0-1 millian meter with C_2 and R_3 are mounted separately in a meter ease. Connection from the meter to the load is made by shielded wire which plugs into the jack on the load.

Circuit Considerations

It has been found that by immersing Allen-Bradley 2-watt composition resistors in oil, the power dissipating capabilities can be increased approximately four times with negligible change in the resistance. This fact makes it possible to build the 50-ohm load with only twelve 2-watt resistors. To prove this point to yourself, take two 1500-ohm, 2-watt resistors and measure their resistance on a bridge or by some other accurate method. Now apply 117 volts, 60 cycles to both. Lay one of the resistors in a small dish filled with oil while leaving the other resistor in the open air. After about fifteen minutes disconnect the voltage and measure the resistances again. You will find that the resistor immersed in oil will have changed less than 3% while the other resistor has increased in value at least 20% and is showing visible signs of breaking down. The power being dissipated was eight watts, or four times the rated dissipation of the resistors!

To insure against your load changing value it would be wise not to run your transmitter into the wattmeter for periods exceeding ten or fifteen minutes at a time without allowing it to cool

The metering circuit is simply a diode voltmeter of the peak-reading type. C_1 determines the lowest frequency which the meter will read accurately. By using a .001 µfd. disc-type condenser for C_1 a signal with a frequency as low as 500 kc. may be read with accuracy. However, to calibrate the meter with a 60-cycle voltage a condenser of higher capacitance is needed. This will be discussed later.

Two crystals of the 1N34 class are required in the circuit in order to keep the voltage applied to the crystal within the manufacturer's rating; the peak voltage is equally divided between the two crystals. Another circuit was tried using resistor voltage dividers so that only one crystal would be needed. This was found impractical since the resistor's lead length introduced a resonant circuit which made the higher frequency readings low.

Calibration

Since the voltage across the load will vary directly with the power being dissipated, the meter can be calibrated to read directly in watts (See Fig. 4). However, since this meter is used in other test equipment it was easier to read the power from a curve than to make a new scale for the meter. The curve in Fig. 4 was calculated from the constants of the circuit. A full-scale deflection of 1 maon the meter would indicate on the curve that 100 watts was being delivered to the load.

To calibrate the meter, connect a $2-\mu fd$. condenser across C_1 and apply a 60-eycle, 71-volt source to the input connector of the load. Plug the meter into the jack and set R_a so that the meter reads full scale. The calibrating voltage may be obtained from your 117-volt line and dropped by means of

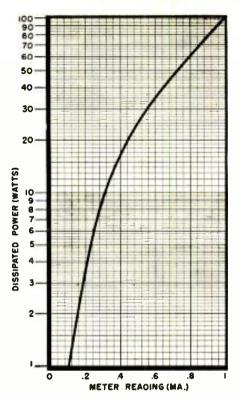
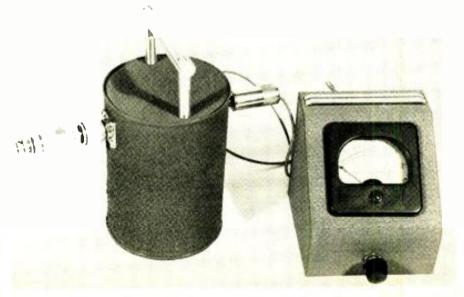


Fig. 4. Calibration curve for the 50-ohm load, calculated from circuit Constants. It can be used as a conversion chart or for calibrating the meter face directly.

a Variac or some other method. A v.t.v.m. should be used to determine that the voltage is exactly 71 volts. Now the 2-µfd, condenser may be disconnected and a cover put on the load can. Your wattmeter is now ready for

Extensive tests have shown that the wattmeter will give approximately 5% accuracy up to 30 mc. The accuracy will depend largely on the accuracy of the ealibrating voltage and the lead lengths of the components.

Fig. 5. The r.f. input jack is located on the left and the phone jack for the shielded cable to the meter is on the right. The knob on meter case is R.



CARE OF TRANSISTORS



Fig. 1. The CK721 and CK722 junction-type transistors. To the right is shown the CK716 in its specially designed molded socket housing.

Transistors are still expensive and may be easily damaged. Here are some practical pointers on caring for these units.

ODAY'S prices place transistors definitely into the category of expensive components. Every experienced radio technician knows that a natural law seems to be that the most costly parts are the most easily damaged. The danger signal is up. Persons setting out to do transistor circuit work are giving serious forethought to protective measures. This writer knows first-hand the horror of burning out an expensive transistor even before securing the required test data.

For future guidance, a careful study has been made of the ways in which these crystal devices can be damaged. and the findings are presented in this article in hope that they will be of service to other technicians. If you know how you can get into trouble with these units, avoiding the pitfalls will be easier.

Supply Potential Polarity

Correct polarity of applied voltages is very important in transistor circuits. Reversing the high-voltage supply in a tube circuit means nothing more than making the plate negative and stopping circuit operation. But reversing the comparable collector voltage in a transistor circuit means a quick burn-

It is worthwhile noting that use of the wrong polarity is an easy matter for the newcomer to transistor circuitry, although he may have had years of experience in tube applications. In fact, the more experience he has had with tubes, the more apt he will be to make the mistake with point-contact transistors because it has become his habit to make the grid negative and plate positive. The reverse is correct in point-contact transistor circuitry (See Fig. 2A). The emitter, which is comparable to the tube grid, is biased positive, while the collector, which is

comparable to the tube plate, is made negative. Both emitter and collector voltages are viewed with respect to the base (germanium wafer) which is comparable to the tube cathode.

In the point-contact transistor, maximum current flow (crystal forward current) occurs when either the emitter or collector whisker is made posi-

Editor's Note: An announcement has just come through from Raytheon that they are in production on the CK722 junction-type transistor. The CK721 junction type is available only in limited quantities at the present time. Their suggested price on the CK722 has been dropped to 87.80 each. For additional information on the design and application of transistors, see the article "fulld This Transistor Receiver" on page 35 of this issue.

tive with respect to the base, just as in crystal diodes. The emitter supply voltage, being normally "whisker-posiis low (on the order of 's volt) so that emitter current, while higher than collector current, is held to a safe value. Reversing the emitter voltage polarity will impair circuit operation but will not damage the transistor. When the collector voltage polarity is reversed, a large forward current flows, due to the much higher collector voltage, and burnout occurs quickly.

In the junction-type transistor, shown in a basic amplifier circuit in Fig. 2B, the supply potential polarities are the same as in a tube circuitemitter negative and collector positive. While this reduces the chance of a mistake when transferring the attention from tubes to junction transistors, a very good likelihood of error is present when working back and forth between point-contact and junction transistors. Reversing the polarity of the junction transistor collector supply voltage is just as disastrous as in the case of the point-contact unit.

While on the subject of polarity, at-

RUFUS P. TURNER, KGAL

tention should be called to the fact that a polarized circuit component such as an electrolytic condenser or d.c. meter normally is connected "backward" in some transistor circuits, especially those using pointcontact transistors. To tube circuit technicians, long accustomed as they are to grounding the negative terminal of an electrolytic condenser, the necessity for grounding the positive in point-contact transistor circuits may be overlooked.

Mounting and Soldering

When the Rautheon CK703 pointcontact transistor first appeared on the market in 1949, the ingenuity of technicians was taxed regarding a satisfactory way to make contact with the tiny base pins of that unit. Soldering to the pins was strongly discouraged. The size and construction of the CK703 was the same as the CK716 shown in Fig. 1. This writer devised a socket (See "A Crystal Receiver with Transistor Amplifier" by Rufus P. Turner. Radio & Television News, January 1950) which, though small in size, turned out to be bulky by comparison with the transistor.

At present, a tiny molded phenolic socket (Cinch Exp. 8749) is available for the CK716. The Cinch 8672 subminiature socket accommodates Western Electric Type A1698 and Bell Luboratories Types M1725 and M1729. The 3-pinned General Electric Types G11 and G11A may be plugged into a 5- or 7-pin subminiature tube socket. Each of the junction types examined thus far by the writer (typical example: Germanium Products Corp.-Federated Semi-Conductor, Inc. No. RD2517) have pigtail leads.

If the transistor is not provided with pigtail leads, no attempt should be made to solder or weld connections to its terminals unless the transistor manufacturer specifically sanctions this method of connection. It is fairly easy to damage germanium devices with heat such as that from a soldering iron or welding device. When soldering to the pigtail leads of transistors provided with such leads, hold the pigtail tightly with long nose pliers as close as possible to the body of the transistor and continue to grip the lead for a short time after the joint appears to have cooled. The pliers will conduct the heat away, preventing its entry into the interior of the transistor. Two good rules are to complete the soldering job as quickly as possible and to use as long a pigtail in the construction as possible.

Transistors may be mounted in any position. This is a convenience, since full exploitation of their small size often favors mounting transistors in whichever is the most convenient position.

Protection from Transients

Transistors must be protected from large voltage surges. A very sensible precaution before inserting the transistor is to examine a circuit thoroughly for possibility of surges. Damaging transients may be set up by steep signal waveforms, circuit switching, kickback from inductive components, sudden application of steady operating potentials, and similar causes.

Each circuit should be analyzed as an individual case and necessary remedial steps taken to reduce transients to, or lower than, the maximum potentials specified for the transistor to be used.

When theoretical investigation of transients must be supplemented with experimental data, the tests often can be made satisfactorily with an equivalent 3-terminal resistor network substituted in the circuit for the transistor.

Sudden switching of steady operating potentials on or off is to be avoided in new test circuits which have not been investigated fully. In a strange transistor circuit, it is advisable to increase the various operating potentials, in a stepless manner, slowly and simultaneously from zero to the design level. Only in this way can certain transistor damage be averted.

Current Limiting

Care must be taken to keep transistors in some circuits from becoming d.c. unstable and running to destruction. One such circuit is the oscillator (Fig. 3) in which a parallel resonant circuit is inserted between base and ground. Sufficient resistance must be present at R_1 and R_2 to limit emitter and collector currents to safe values.

A good precaution is to install a current limiting resistor, selected to conform to the type of transistor and circuit operating conditions, in series with the emitter of any transistor oscillator. If a collector load resistor is not employed normally in the circuit, another resistor should also be connected in series with the collector. Current limiting resistors are desirable also in many transistor amplifier and control circuits, especially in those circuits employing external base resistors or in which a coil or transformer is used instead of a load resistor in the output. In Fig. 2, points A and B are the proper locations for current limiting resistors.

External resistance connected between the transistor base and ground tends to make the transistor unstable. Hence, any attempt to "cathode bias" a transistor must be approached with caution. When it is imperative to employ such external resistance in a circuit, its value must be kept as low as

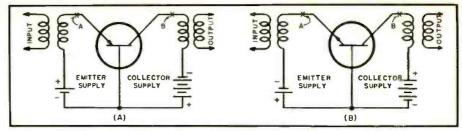


Fig. 2. Single-stage amplifiers (A) point-contact. and (B) junction types.

possible to prevent instability. "Cathode-biased" transistor amplifiers frequently oscillate or "sing" unless the base resistors are bypassed adequately.

In all transistor circuits, care must be taken to avoid excessive peak currents. Such current peaks can occur easily when high capacitances effectively are in series with either electrode of the transistor. The situation is very much the same as that in which a large filter condenser follows a metallic rectifier. Current limiting resistors must be provided for reduction of the peak currents.

Temperature Environment

While germanium transistors show negligible self-generation of heat, they are sensitive to ambient temperature, the junction type to a greater extent than the point-contact type. In fact, temperature dependence is one of the unsolved shortcomings of the transistor.

It is inadvisable, for that reason, to operate transistors at full ratings at high temperature. While +80 degrees centigrade has been stated as the top operating temperature for some transistors, it is best to consult the ratings of the individual type to be used. A warm chassis is not a good place to install transistors. The junction type particularly must be kept well away from hot tubes, resistors, and similar components.

It is correct to regard transistors as rugged, since they have given good account of themselves in vibration and shock tests, appearing better than vacuum tubes in some instances. But

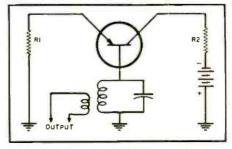


Fig. 3. Circuit of a "base" oscillator.

this is no reason to be unduly careless in handling them. Possible damage should not be risked by tapping or hammering on transistors or by dropping them from considerable heights. To prevent possible internal deformations, the transistor should not be pinched excessively by its mechanical mounting.

With transistors, we are in very much the same position as with vacuum tubes during the 20's. In those days, tubes were expensive and fragile and we just did not throw them around. Every circuit was checked and its "bad acting" possibilities thoroughly considered before tubes were plugged into their sockets.

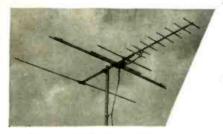
If for no other reason, the present cost of transistors should put us on guard. The best procedure is to become fully aware of the possibilities for damage to the units, and then to check and double check all circuitry. Finally, care must be exercised in the initial operation of an experimental transistor circuit.

-30-

This portable, battery-operated television receiver uses transistors and no tubes except the 5" picture tube (at the right). This unit was one of the series of transistor equipment demonstrated recently by RCA at its Princeton, N. J., Laboratories.



V.H.F.-U.H.F.



"Suburban Illtra Q.Tee"

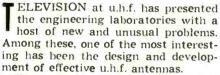
ANTENNA DESIGN

"Ultra Q-Tee"

L. F. B. CARINI

Assistant Chief Engineer The LaPointe-Plascomold Corp.

Engineering criteria in developing an all-channel antenna for both u.h.f. and v.h.f. video bands.



The majority of v.h.f. antennas of past design and in current use are unsuited inherently for the reception of u.h.f. Directivity patterns are poor and, more important, these antennas fail to produce the gain required to pick up elusive u.h.f. signals.

Designing an antenna capable of providing a uniform gain over the entire u.h.f. spectrum is, in itself, an inordinate technical challenge. With v.h.f. the dozen channels ranging from 54 mc. to 216 mc. presented no serious problem, and indeed, many of the socalled all-channel antennas gave satisfactory response for average service. The problem of designing an antenna that has a reasonably linear response for all the u.h.f. channels and for v.h.f. as well, becomes complicated by the inability to decide upon compatible values in compromising between theoretical and physical ideals. The new

band of ultra-high frequencies is so broad, comparatively speaking, that many antenna types which were entirely satisfactory at v.h.f. cannot be adapted for u.h.f.

The accompanying chart (Table 1) shows the relative gain of various types of u.h.f. antennas as compared to a simple dipole used as reference. Note that, as in v.h.f., the highest gains are furnished by the more directional arrays.

Theoretical considerations have dictated and practical tests have proven that the best policy is to combine a u.h.f.-designed element or antenna with a v.h.f. antenna for optimum allchannel reception. Such an antenna is shown on the cover. Resonant filters, or channel separators, in the form of printed circuitry may be employed to effectively separate the v.h.f. portion of the antenna from the u.h.f. elements. The use of printed circuits permits filters to be applied directly to the antenna where the division of elements actually defines the limits of channel segregation. Printed circuitry makes possible small, compact LC units of light weight, which when properly encapsulated, are electrically stable and weatherproof as substitutes for the usual large inductances and condensers.

For metropolitan service, it was found that the average 2 to 3 db gain supplied by a simple broadband "V" cut for u.h.f. when added to a v.h.f. antenna would provide adequate gain within city limits. In fringe areas where maximum signal gain must be obtained, the v.h.f. antenna is used in conjunction with a u.h.f. multi-element yagi. Gain as high as 14 db is obtained to satisfactorily pick up a signal in the most difficult locations. This type of antenna was extensively employed in the Portland area.

Other considerations of what constitutes good u.h.f. antenna design reflect the importance of physical construction. At u.h.f., any slight physical displacement of the antenna, or its constituent components, is sufficient to introduce noise, picture fluctuation, or ghosts. Therefore, one of the primary precautions to observe in engineering development is rigidity in design and permanence of construction. tion proofing and a freedom from any movement of the antenna elements become particularly important because they contribute to maintaining a steady signal input to the receiver. For this reason, large metal surfaces which offer considerable high wind resistance are objectionable and should he made of screen or perforated sheet metal. Use of a Fiberglas boom for the yagi antenna increases the strength and rigidity of the array. Noise generation at u.h.f. is serious enough as a result of tube noises and it should not be augmented by defective and loose mechanical connections as contributed by corrosion and rubbing of parts during high winds.

Table 1. Comparative gain for several types of antennas suitable for u.h.f. reception.

TYPE	FREQUENCY RANGE	GAIN (in db)
Dipole (1/4 wave center fed)	Broadband	0
V (single)	Broadband	2-3
V (2-bay)	Broadband	5-6
Double Dipole	Broadband	3-4
Bow Tie	Broadband	3
Folded Dipole*	Broadband	5
Helical	Broadband	8
Rhombic	Broadband	9
Corner Reflector	Broadband	10
Yagi (single 12-element)	Single Channel	14
Yagi (2-stack 12-element)	Single Channel	17
Colinear	Multiple Channels	9
Colinear (4-bay array)	Multiple Channels	14
Colinear (8-bay side-by-side)	Multiple Channels	17
* With reflector		



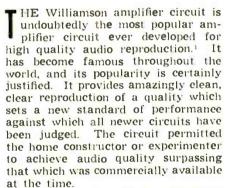
Evaluating antenna performance—a

"Q-Tee" model.

IMPROVING THE WILLIAMSON AMPLIFIER

DAVID HAFLER and HERBERT I. KEROES

Acro Products Company



The high quality of the amplifier is due to several design principles. All stages are designed for minimum distortion and maximum bandpass. Class A triodes are used throughout. A pushpull, resistance-coupled driver stage is used to provide adequate signal at low distortion to the push-pull output stage. This stage consists of triode connected tetrodes which furnish a very important advantage over conventional low mu triodes. They require grid signal voltages of approximately 40 volts for full output as contrasted with 60 or 70 volts for triodes of the 2A3 and 6B4 type and 80 to 90 volts for a tube like the 6AS7G. In many triode amplifiers, there is more distortion generated in the attempt to drive the output stage than there is in the output stage. In the Williamson circuit there is sufficient drive available, and the limiting factor is the distortion inherent in the output stage. This is kept to low levels through the use of a feedback loop encompassing the entire four-stage circuit, including the output transformer.

These distinctive features of the amplifier make for a truly high grade circuit. The basic principle of the design is that there is no skimping. For example, Mr. Williamson stipulated design specifications and operating



A variation on the Williamson circuit which provides "ultra-linear" operation and a minimum of distortion.

parameters for the output transformer to be used to insure that this critical component had frequency response far in excess of the audio band and could handle 20 watts of undistorted power even though the power rating of the complete circuit was less than 15 watts.

combination of attributes This makes an outstanding amplifier with frequency response from 10 cps to 100 kc. (a wide bandpass provides good transient response) and intermodulation distortion of less than 1% at 10 watts of output. It has the elusive quality of "presence" which cannot be reflected in measurements but only in listening tests.

Improving the Williamson circuit is obviously a difficult task. It seems that conventional designs using conventional components are unlikely to excel the Williamson either in listening quality or in laboratory tests.

However, a recent unconventional circuit development has made possible a simultaneous reduction in distortion and increase in efficiency in the output stage of the Williamson (and many other circuits). This new circuit arrangement, on which patents are pending, is termed "ultra-linear"2 operation-a name chosen because the circuit represents the most linear possible mode of operation of a pair of output tubes. It is neither triode nor tetrode tube operation but borrows the advantages of both without the disadvantages of either.

"Ultra-Linear" Operation

Arguments concerning triodes versus tetrodes have been carried on for many years without any definitive conclusions. Each tube type has its advantages and its disadvantages, and those who favor either will find many reasons to justify their choice while disparaging the other type. The present status of the battle seems to be that the tetrode advocate is in the minority. The triode with feedback, such as is used in the Williamson eircuit, has surpassed it in popularity among home constructors and custom builders of audio equipment although not among commercial manufacturers. The commercial interests are motivated by the fact that the efficiency of tetrodes is higher than triodes, and the distortion of a tetrode amplifier can be made lower over a greater operating range than can be done with

Since there are arguments on each side, the choice between the two must be based on the relative weights of the various factors by which they differ. One person prefers triode low impedance; another likes tetrode power sensitivity. Similarly, the triode proponent likes the sound of triodes; the tetrode man likes tetrode sound. Each rejects the elusive and minute distortions which characterize the other tube type.

The basic cause of the whole argument seems to be that neither tube type is close enough to perfection.

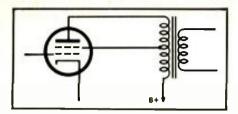


Fig. 1. "Ultra-linear" connection of a tetrode.

Each has its faults. Conventional tubes are essentially nonlinear circuit elements. As such, they generate audible distortion. Acceptance of one type is not necessarily because of its quality—often it stems from rejection of the other type. Choice resolves to the lesser of two evils. The remedy for this basic situation can only come from either a new tube type or from a new method of operating existing tube types.

The tetrode output tube can be operated as a triode by connecting screen to plate as is done in the Williamson circuit. If the screen is par-tially connected to the plate, we have what is effectively a new type of tube. This can be accomplished by connecting the screen grid to a point on the primary winding of the output transformer as is illustrated in Fig. 1. If the primary tap is at the top of the winding, we have a triode tube with plate characteristic curves concave upward. If the tap is at the low end, the "B plus" point, we have a tetrode with plate characteristic curves concave downward. At a critical intermediate point, we obtain a plate characteristic which is essentially a straight line. This is the point of "ultra-linear" operation and the point of minimum distortion.

Fortuitously, the "ultra-linear" point also has several additional operating advantages. It maintains the full efficiency and power sensitivity of the tetrode along with its high power capabilities. Simultaneously, it has low internal impedance like the triode. It combines the most advantageous features of each and has lower harmonic and intermodulation distortion than either of the two basic tube types.

Fig. 2, for example, shows a comparison of the intermodulation distortion of a push-pull stage without feedback for triode connection, "ultralinear" connection, and tetrode connection. These curves show that the triode cannot handle high powers while the tetrode has relatively high distortion at lower operating levels. The "ultra-linear" stage obviously is an improvement over either of the others over most of the useful power range. Evidently, with other things held equal, an "ultra-linear" output stage must make a better amplifier than can be realized with any triode or tetrode circuit.

One of the more subtle advantages of "ultra-linear" operation lies in the inherent regulation of this type of output stage. There is practically no change in tube current drain from

quiescent operation up to full output. This permits the use of a minimum power supply. With other operating arrangements there is a loss of low frequency power handling capacity if the power supply regulation is inadequate.

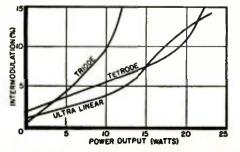
"Ultra-linear" tube operation cannot be utilized with standard output transformers. It is necessary to have a tapped primary winding, and the conventional units of multiple impedance have taps at positions which do not give optimum results. The primary tap for tube types such as are commonly used in the Williamson circuit must be at a point so that the load impedance in the screen circuit is 18.5% of the load impedance in the plate circuit. In order to carry through the optimum conditions, a special transformer, the Acrosound TO-300. has been developed to be used for "ultra-linear" operation of beam power tuhes of the 6L6, 807, 5881, and KT-66 type. It is a unit which has a tapped primary of 6600 ohms total impedance with the screen-to-screen load impedance 1220 ohms-the ratio of plate-to-screen load which provides most linear tube characteristics. The transformer also has a frequency characteristic of plus or minus 1 db from 10 cps to 100 kc. and the ability to handle 40 watts of audio power over a very wide frequency range.

The specifications of this transformer exceed those stipulated by Mr. Williamson. The operating conditions of the output stage exceed those of his triode-connected tubes. Therefore, since the Williamson circuit using the "ultra-linear" output stage will have a more linear characteristic in that portion of the amplifier which is its weakest link and the prime source of distortion, the combination of "ultralinear" stage and the Williamson circuit can be expected to be an improvement over the original. Actually, the power output of the "ultra-linear" Williamson is about doubled for the same distortion as compared to the triode Williamson and auditory quality is also improved.

Combining the Two Circuits

Fig. 3 shows the complete circuit of the Williamson amplifier with the "ultra-linear" output stage. Several minor changes have been made from the original circuit for optimum integration of the two circuits. All of the changes from the original circuit are

Fig. 2. Comparison of distortion characteristics of triode, "ultra-linear," and tetrode stages. See text for full details.



shown within dotted lines on the schematic. The change in the output transformer is the major change. The other deviations from the original involve only a few condensers and resistors. These changes readjust the feedback to maintain it at the desired 20 decihels, and they also improve on the stability margin of the original circuit. 3, 4

The circuit requires a power supply furnishing between 425 and 450 volts at 130 to 140 ma. This is obtained most simply hy using a standard 400 volt, 200 ma. power transformer with 5V4G rectifier and condenser input. Operation of the power transformer at the lower drain provides higherthan-rated output voltage along with cool operation. The input filter condenser should have at least a 500 working volt rating while the later condensers can be 450 or 475 volt types. The use of a cathode-type rectifier limits the initial voltage surge so that higher rated condensers are not required.

In order to get equal output signals from each half of the phase inverter, the plate and cathode resistors should be matched to within 1%. If equipment for measuring this closely is not available, the use of 1% deposited carbon resistors (made by Continental Carbon, IRC, or Wilcor) is suggested. This also applies to the plate load resistors of the push-pull driver stage which should be matched so that the drive to the output stage is equal on both sides.

The output tubes can be 807's, 5881's, WE350A's, or the British KT-66's. All of these can take the recommended voltage without exceeding tube dissipation. Though the difference in performance is not substantial, the authors have found that the KT-66 provides the lowest distortion at low power levels (around one or two watts), and its power capabilities are somewhat better than the others.

It is highly recommended that, as shown, the output cathode resistors be bypassed with a condenser in excess of $100~\mu fd$. This avoids third harmonic distortion and consequent intermodulation distortion particularly under conditions of high level dynamic operation.¹

Negative feedback is carried around the output transformer and all four stages. This negative feedback reduces distortion, hum, noise, and output impedance by a factor of 10. In connecting the feedback loop, the color coding of the plate and screen leads of the output transformer should be observed. As indicated on the schematic, the plate and screen leads marked with a white tracer should be paired and connected to the lower output tube; this tube is on the side of the circuit which is energized from the cathode of the phase inverter. The other plate and screen leads go to the side of the circuit which comes off the plate side of the phase inverter. In this way, feedback phasing is correct, and there will be no oscillation of the amplifier at either high or low frequencies if the remainder of the circuit has been wired correctly.

The feedback connection is made from the 16-ohm tap irrespective of the tap used to connect the speaker. This arrangement saves having to reconnect the output winding and change the feedback resistor should a speaker of different impedance be connected to the amplifier.

A bias balancing network is shown in the cathode circuit of the output stage. This cannot compensate for badly mismatched tubes, but it does permit adjusting for normal variations from tube to tube. A milliammeter should be inserted in each cathode circuit at the points marked "X", and the cathode currents should be balanced by adjusting the potentiometer. Each tube should draw in the neighborhood of 60 ma. if the plate supply voltage is 450 volts. If the plate voltage is 400 volts, the current drain will be approximately 50 ma.

Amplifier Performance

Maximum undistorted output of the "ultra-linear" Williamson amplifier is about 30 watts. This output is achieved with an input signal of one volt. In the triode Williamson, close to two volts of drive are required, and maximum output is not over 15 watts.

The comparative intermodulation data for the triode and "ultra-linear" Williamsons is shown in Fig. 4. It can be seen that the "ultra-linear" circuit provides about double the power before the distortion becomes serious. At levels of one or two watts, the intermodulation is in the vicinity of .06%. At 13 watts of output, it is only .3%, and it reaches the 1% point at about 20 watts.

The high power handling capacity of the amplifier is well demonstrated by the power curve of Fig. 5. It represents the maximum undistorted power available at various frequencies. The amplifier puts out 25 watts at 20 cps and nearly 30 watts past 20 kc. This power curve is not a response curve. It would be possible for response to be flat and for power to be down considerably at the ends of the frequency spectrum. The undistorted

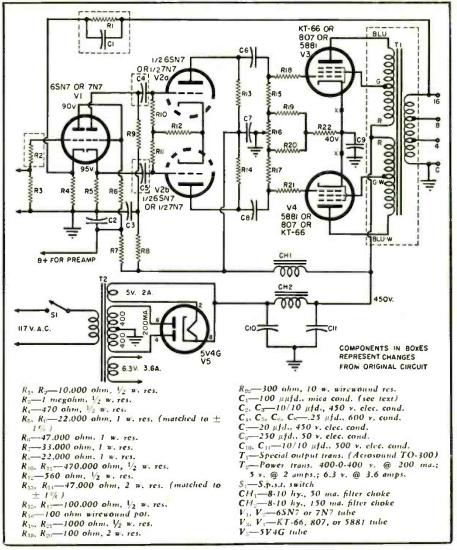


Fig. 3. "Ultra-linear" Williamson circuit. Dotted sections are changes from original.

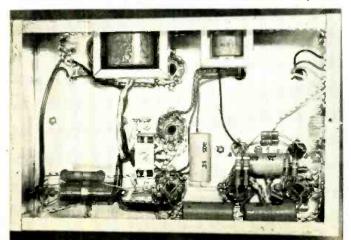
power measurement is a much more rigid test of amplifier performance than a response curve run at a 25 watt level where the distortion is ignored. Little publicized data makes the distinction between a true power curve of undistorted power and a high level response curve.

Fig. 6 shows the response curve which is broad beyond normal re-

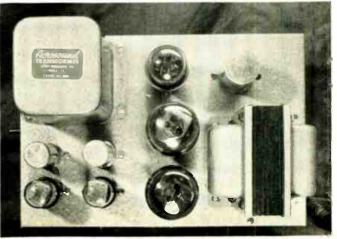
quirements. The response of plus or minus 1 db from 2 cps to 200 kc. is required to minimize phase shift in the audio band since very small variations in gain are correlated with comparatively large variations in phase even at points far removed from where the response is first observed to vary. In this circuit, the response is flat from

(Continued on page 98)

Underchassis view of the "ultra-linear" Williamson amplifier.



Top chassis view showing specially-designed output transformer.



February, 1953

4

TV SIGNAL DISTRIBUTION METHODS



Fig. 1. Blonder-Tongue MA4-1-M mixer-amplifier. Unit has four channel amplifiers and supplies two sets or one set and a distribution line.

By EDWARD M. NOLL

ULTI-RECEIVER systems can be simple or very elaborate depending on the number of outlets. signal levels, and distribution requirements. Outlet arrangement can vary from a simple outlet box for supplying two receivers to an apartment house installation serving hundreds of receivers. The objective of an outlet system is to supply as good or better signals to each receiver than could be obtained from a separate antenna for each receiver. This objective is obtained with ease for some installations but only with difficulty for others. Outlet system criteria are as follows:

1. Signal Level. Sufficient signal level should be delivered to each receiver input for each desired station. Levels should correspond to what could be obtained from a conventional antenna system for each receiver at the same location. Some tolerance can be extended in a strong signal area in regards to signal level because of the receiver a.g.c. facility. Amplitude must not be allowed to decline to a level where noise and interference become more apparent on the picture. In weak signal areas it is

Several ways of handling multi-receiver TV installations including strong-fringe, all-strong, or all-fringe signals.

advisable that the multi-outlet system give a boost to the signals so stronger signals are available at each receiver.

2. Signal-to-Noise Ratio. A distribution system should have a high signal-to noise ratio. Although amplification is advisable, amplifiers need to establish a signal-to-noise ratio comparable to or better than a high quality tuner. Terminations are exacting in feeding receiver groups since mismatches open such lines to high noise levels and interference.

3. Interaction. A difficult multi-outlet problem is the elimination of such interference between receivers as local oscillator radiation, other spurious beats, and loading. Thus a distribution system must have definite one-way characteristics—transfer of signals to receivers but maximum rejection of signals attempting to leave the receivers. Again, terminations must be exacting as any standing waves on lines can be shifted by receiver channel switching, changing ratios and loading at other receivers on the line.

4. Signal Level Range. Still another difficult multi-outlet problem is the ability to handle wide signal level ranges (both fringe and local) on the same distribution system. Both weak and strong signals on the line can be trying, presenting such problems as overload, picture superimposition, oscillations, and beat interference. It is difficult to hold down the strong signals (without sacrificing their quality) and, at same time, permit maximum amplification of weak signals.

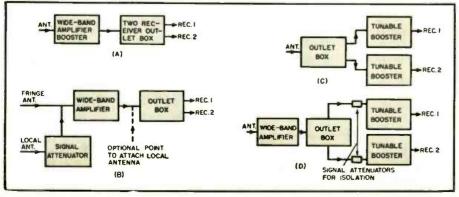
Basic Methods

A simple multi-outlet box is satisfactory when sufficient signal is available. There is a substantial signal loss in almost all outlet boxes and if any one of the desired channels is low in level, picture quality declines. Often on the high-band channels a particular channel can be peaked by experimenting with the lengths of line between the outlet device and each receiver. A sliding, two-foot length of tinfoil on each lead is helpful in peaking line length for optimum performance on a given weak channel.

If signal levels are weak a wideband booster should be used ahead of the outlet device (Fig. 2A). Here, on occasion, we must cope with the difficult problem of handling both weak and strong signals. Some possible solutions to this simple outlet method are:

a. Use the attenuator included with wide-band amplifier or employ an external attenuator. Adjust control

Fig. 2. (A) Wide-band booster and outlet box arrangement. (B) Method for combining local and fringe area signal distribution. (C and D) Reducing receiver interaction.



until strong signal does not overload amplifier—no oscillation or superimposition of strong signal on some other weak channel.

b. If there is a great level differential between strong and weak stations (local and fringe reception from a distance greater than 35-40 miles) the control setting method is not adequate because fringe level is sacrificed. Careful antenna orientation can often reduce the problem. Set the antenna for peak or near-peak fringe reception in combination with minimum pick-up of local channels. This is often a tedious adjustment as improper orientation on local channels can also cause loss of picture resolution or reflections. This task must be performed carefully and critically.

c. A more elaborate and sometimes the only solution to the difficulty is to use separate antennas. Choose a highgain and sharp-pattern antenna for fringe reception and a simple antenna for local reception. Apply separate transmission lines to the antennas. Connect line from local antenna, Fig. 2B, to output of wide-band booster or through attenuator to input of wideband amplifier. The length of the line from the local antenna must be adjusted critically so as not to act as a suppression stub for one of the fringe channels. This can be done by cutting off three-inch lengths and observing its influence on fringe station level. Pieces of tinfoil on each line can help in obtaining optimum adjustment.

The outlet box has as a second major function, the minimization of interaction between receivers. This can be in the form of loading (change of signal levels at one receiver when a second receiver is switched from channel to channel) or local oscillator feedthrough (interference pattern formed on one receiver as a result of the admission of local oscillator signal from the second receiver). Consequently, the outlet device should act as a oneway device as much as possible-least attenuation of the signal passing through to the receiver but maximum rejection of signals attempting to leave the receiver.

This can be a severe problem in trying to connect a multi-outlet receiver with strong local oscillator feedthrough to the antenna terminals. A few possible solutions are:

a. Insert tunable boosters between outlet device and individual receivers (Figs. 2C & 2D). A booster of adequate design is an excellent one-way device, providing amplification of the signal in one direction and good rejection of any signal attempting to move in the other direction.

b. The first solution can result in a somewhat poorer signal-to-noise ratio as signals are divided before amplification. A better plan is to include a wide-band booster ahead of the outlet device and separate tunable boosters for individual receivers. This is a practical means of multi-outlet installations for fringe areas.

c. If strong signals are available,

signal attenuators can be inserted in the receiver lines and adjusted for maximum attenuation of the local oscillator signal without a degrading loss of the station signal level.

Distribution Amplifiers

The plan of amplification-before-division is employed in most of the commercial types of multi-receiver systems. This expedient retains a better signal-to-noise ratio than is possible if the signal is first divided (reduced in level) and then amplified. Commercial systems can supply from two to hundreds of outlets depending on the design and number of units used. A small four-position arrangement consisting of a wide-band amplifier and two multi-outlet boxes (or a single four-receiver box) is effective in serving four receivers for duplex and semi-detached housing (either four apartments or two families with receivers on each floor).

With a good high-gain antenna and proper installation, good fringe area reception is possible with this arrangement. Critical performance checks must be made and all problems reduced as much as possible, using techniques mentioned previously. The use of a separate tunable booster at each receiver can improve fringe results.

Commercial systems generally consist of four basic units which can be arranged in numerous combinations to supply from 2 to 2000 TV sets. These units are:

a. Small distribution outlet amplifier to supply two individual receivers. The function of this unit is the same as the ordinary outlet box. However, this type of vacuum tube outlet box has a circuit that has little or no loss (some few with gain) and provides thorough isolation between receivers.

b. Larger distribution amplifiers with a number of individual receiver outlets (four to ten) with thorough isolation between outlets and very little signal loss. On most distribution amplifiers there are separate line outlets available to permit continuance of the coaxial line path to succeeding distribution amplifiers. Some slight loss

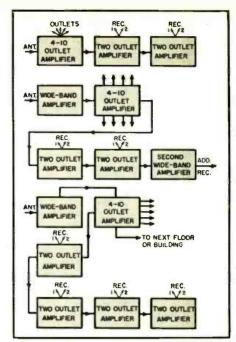
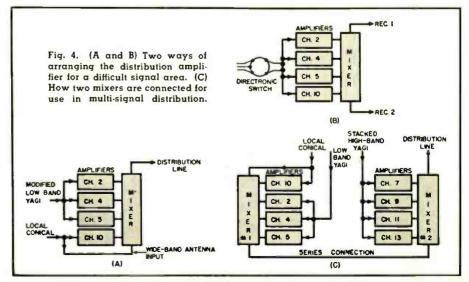


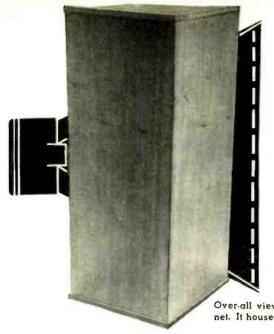
Fig. 3. Three ways in which the distribution amplifiers can be connected. See text for complete application information.

is encountered at these low impedance line outlets. Regular receiver outlets have a 300-ohm impedance.

c. Wide-band amplifier with a high gain is used to bring up signal level for a fringe-area or weak-signal distribution installation. For least difficulty in a distribution system, the signal level for each channel should reach a 10,000 microvolt level. When signal levels are lower, the line runs must be planned carefully to avoid noise pick up. Signal is attenuated rapidly as line lengths are increased and it is possible to have the signal fall off so seriously that poor signalto-noise ratios are established at the input of the next distribution unit. This poor ratio will continue through the succeeding units of the distribution system.

d. High-gain amplifiers in the form of individual channel amplifiers associated with a central distribution am(Continued on page 121)





AN IMPROVED CORNER HORN SPEAKER SYSTEM

By

GEORGE L. AUGSPURGER

Audio Research Laboratories

A new version of the integral space transducer originally described in the November 1949 issue.

Over-all view of IS-800 corner horn cabinet. It houses an ordinary 8" p.a. speaker.

Something for nothing is a slogan that usually leads to disappointment in audio work. However, recent developments such as the reluctance pickup and the Williamson amplifier circuit have served to give us something really worth listening to at a cost that does not preclude the purchase of food and clothing. It is only the speaker system, the most uncooperative and contrary link in the whole audio chain, that has so far refused to satisfy the most critical listener for anything less than several hundred dollars.

In the November 1949 issue of RADIO & TELEVISION NEWS Ray Doby and the writer described a corner horn speaker system which attempted to coax full-range response from smaller, less expensive speakers. The "integral space transducer," as it was called, was a step in the right direction, but it suffered from several unfortunate deficiencies. It presented a rather startling appearance (most people thought it was a portable bar), and was devilishly tricky to build. It also developed that the "I.S.T." was almost entirely at the mercy of its bass driver. Speaker selection was so critical that the total system "... when she was good, was very, very good; but when she was had, she was horrid!"

The unit to be described here retains the basic features of the previous design while gaining the advantages of greatly-increased bass efficiency, simplified construction, noncritical driver selection, and lower cost. This new design, using an ordinary p.a. speaker (Stromberg-Carlson RC-24) as a driver, can easily outperform a good twelve-inch bass-reflex With higher quality eightinch speakers such as the Altec 400B, the IS-800 will satisfy the most critical musical ear. The secret of its remarkable quality lies in the fact that, whereas its predecessor had merely helped the speaker achieve its best performance, the IS-800 gives its driver no choice. In other words, the horn loading, coupling chamber, backwave enclosure, and reflex ports are all worked out to give such a degree of control over the speaker cone that, regardless of its own attitude, improved transient characteristics, extended bass response, and more linear transfer qualities cannot help but result.

The IS-800 is basically a vertical corner horn of square cross-section. The driver is mounted at the base of the cabinet and is coupled to the horn by a small compression chamber and a concrete reflector block of the type used so successfully by P. G. A. H. Voigt. The horn expands along two adjacent sides of the square from a 36 square-inch throat to a mouth area of 288 square inches.

The completed cabinet looks somewhat like a glorified office wastebasket. All four sides are alike and all taper toward the base of the unit. The slanting sides not only offer a pleasing appearance, but clearance space is provided for haseboards and moldings. Moreover, the driver backwave is vented through the space between the room walls and the sloping sides of the cabinet.

The finished system is capped with a mahogany frame, and the horn mouth is protected by a perforated metal grille. The eye appeal of this simple design is quite favorable when compared with the usual visible louvers, ports, and ornate grille treatments. Of course, there is no reason why the front panels of the IS-800 cannot be decorated in any manner that the builder happens to like. We personally prefer the cabinet shown because it is harmonious and unobtrusive in any furnishing scheme.

The actual construction of the horn and cabinet may seem tricky and unfamiliar. Actually, there is nothing really difficult to worry about, but a good job will take time . . . a good deal more time than a bass-reflex cabinet for example. The proper sequence of assembly is as follows:

The two back panels (B_1, B_2) should first he cut out and fastened together. The panels are glued and screwed to the quarter-round joining strip and the triangular plywood base (F). The two curved horn sides (C_1, C_2) are then cut and fastened to their struts (D_1, D_2) . The struts, in turn, are fastened to the rear panels and the flared pieces joined with a section of quarter-round as was originally done for B_1 and B_2 . The front length of quarter-round, however, should be planed in such a way that the straight edges make an angle greater than ninety degrees toward the upper end.

This bit of doctoring is necessary since the joint is not vertical. If the joining strip is used without modification, the front walls of the horn will be pulled out of square and trouble will result.

The speaker mounting board (G) can now be installed and the coupling chamber completed by the addition of (H), which must be cut and fitted carefully to make a tight seal between the compression chamber and the horn throat,

The horn proper needs the addition of a concrete reflector block for its completion. This task is perhaps the most satisfying and creative part of the whole proceeding. The builder suddenly supplied with a fascinating batch of wet concrete, will probably spend a happy afternoon finding other uses for the messy stuff. The L.S.T., however, need only be tilted back at an angle of 45 degrees, and a small quantity of the mixture poured into its gullet. Pre-mixed dry concrete, available from almost any lumber company, is inexpensive and easy to use for this operation.

The front panels (A_1, A_2) are mitred and fitted together, tacked and glued to another joining strip. Two $\frac{1}{2} \times 1$ inch strips are glued one-quarter inch from the outside edges of the front panels, and a thin mahogany strip is

glued to the lower front edges of the sheets. *Kimsul* bats are tacked to the inside surfaces, and the exposed sides are finished in any manner desired. Usually an application of wood filler, then one of stain, and two coats of satin-finish varnish will do a satisfactory finishing job.

Before assembling the two halves of the cabinet, the concave surfaces of the horn should be covered with some sort of acoustic material. Acoustic tile cement is a good gooey compound to use when applying these deadening bats to the *Masonite* surfaces.

Six one-inch holes are bored in each rear side of the backwave chamber, and the two sections are assembled into the complete IS-800 cabinet. If a separate tweeter is to be used, the tweeter mounting strut and the necessary wiring should be installed before this final combination is effected.

The metal grille, the mahogany cap, and the driver can be fitted into place, and the "I.S.T." is ready for use. The cabinet should be placed in a corner of the listening room whose wall surfaces extend at least three feet beyond the speaker system. Since the vertical axis of the horn eliminates directional blasting, the usual precautions of speaker positioning do not apply to the "integral space transducer."

Experience with the previous article has shown that a brief warning is necessary at this point. The dimensions given on these pages are worked out on the basis of an eight-inch driver. Larger speaker sizes will not improve reproduction. Instead, the acoustic relationships of the cabinet will be upset, and ragged response will result. The IS-800 is specifically designed to be used with fairly compliant eight-inch cone speakers such as the Altec 400B, Jim Lansing No. 208, Stromberg-Carlson RC-24, or Jensen P 8-RX.

When listening to the reproduction offered by the IS-800, the builder will find that new settings of the equalizer controls are necessary to achieve correct tonal balance. The genuine bass response of the horn will extend the low frequency limit of the system considerably below that of conventional bass-reflex cabinets. The treble response, on the other hand, is non-directional and will have to be boosted unless a separate tweeter and high-pass network are incorporated into the speaker system.

Although the IS-800 is designed primarily for home sound installations, its compact size, non-directional propagation, and live quality sound reproduction make it an excellent unit for

Mechanical details for constructing the improved "integral space transducer." (A) Interior view (left) and completed unit. (B) Top view. (C) Section through x-x' (refer to B). (D) Front panels A_1 and A_2 (left) and top view of front panel assembly. (E) Back panels (left) and curved horn sides. (F) Struts (left), plywood mounting base (top right), speaker mounting board (bottom right), and fitting piece (center right). See text.

various other situations. Broadcast stations, school music departments, wired-music installations, and even small auditoriums offer opportunities in which the advantages of the "I.S.T." may prompt its use.

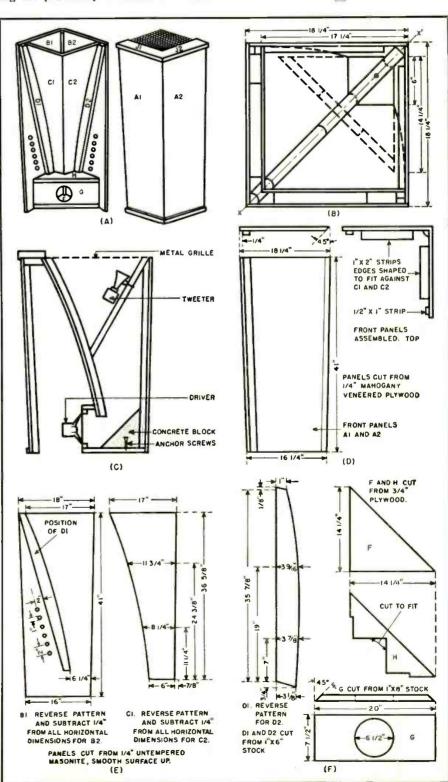
Many of the excellent speaker enclosures available are of such large physical size that their use in the average living room means the rearrangement or elimination of some of the furniture.

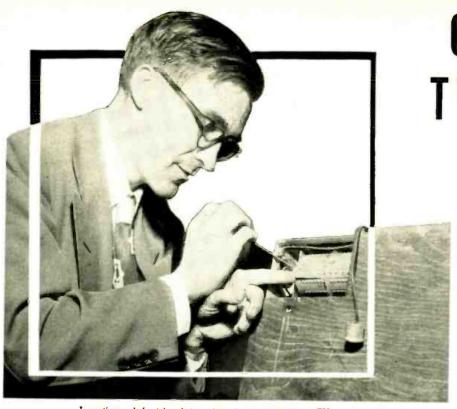
The music lover already has enough difficulties to overcome, without adding the possibility of domestic friction

to his or her rapidly growing list of problems.

While the new "integral space transducer" is considerably more elaborate than box type baffles, the use of a less expensive speaker plus the more realistic listening quality achieved more than offset complications in construction. Whether the reader has the unit built, builds it himself, or purchases it ready-made, he will appreciate the IS-800's improvements over conventional moderate-priced speaker systems.







Inserting u.h.f. strips into a turret type tuner in a TV receiver.

Data on four TV service problems: spot blanking, foldover, vertical retrace lines, and installation of u.h.f. strips.

ANY of our readers have presented common service problems and since quite a few are similar, we are going to cover four of these topics here. One of the most frequently asked questions is about a bright spot on the screen after the set has been turned off. This phenomenon contributes to shorter tube life and therefore concerns both the service technician and the set owner. The appearance of retrace lines, on weak stations especially, is also a cause of frequent inquiries. Foldover at either side of the picture is another recurring problem. As a sign of TV's rapid progress we have also been asked about the installation of u.h.f. strips into some v.h.f. turret tuners and the difficulties encountered there. In this article all four topics will be discussed individually and circuits shown which can be applied to almost all sets to remedy the various defects.

Spot Blanking

In some receivers, especially recent models using higher anode voltage and electrostatic focus, a circular spot appears on the screen after the set is turned off. This spot fades away gradually, becoming larger as it gets dimmer. When analyzed carefully the reason for it is found in the fact that the HV condenser or the external and internal conducting surfaces on the picture tube retain the HV charge even after the deflection circuit is shut

down. With HV still on the second anode and no deflection power applied, a circular spot appears. Electrons flow from the cathode to the second anode, lighting up the screen and at the same time discharging the condenser. When finally the charge drops below the voltage required to light up the screen, the spot disappears. Because each time the set is turned off only the center of the screen is hit by the electron beam, the screen wears out faster at that point and eventually a yellow or brownish spot may appear.

An ideal solution to this problem is to connect a resistance across the condenser at the moment the set is turned off. This would mean HV present at a switch contact and a chance of arcing as the switch is closed. The difficulty of such a scheme prevents its use in commercially available receivers.

Next to switching in a discharge resistance we could attempt to connect a very high resistance across the HV condenser permanently. In order not to load down the HV supply only about 10 microamperes could be drawn by this bleeder. This would mean a 1000 megohm resistor, able to stand a voltage of at least 10 kv. The only type of resistor applicable is the spiral, carbon-coated HV type used as a bleeder for HV meter multiplier probes. The size and expense of such ness.

CURRENT TV TOPICS

WALTER H. BUCHSBAUM

Television Consultant
RADIO & TELEVISION NEWS

There are, however, two different usable methods for removing this undesirable spot. One is to utilize the picture tube as a discharge resistor. the other is to move the electron beam to the side so that it hits the anode directly without reaching the screen. The first system is fairly simple to install and operates reliably and smoothly. When the picture tube is adjusted to give maximum brightness, maximum current flows through it. In the case of a shut-off spot simply adjusting the brightness control to maximum will remove the spot, because the large current passing through the picture tube discharges the HV condenser quickly. Many customers are willing to make this adjustment manually every time the set is turned off. For those who do not want to be bothered with this additional adjustment, an automatic circuit can be added. Fig. 1 shows four such circuits—all based on the principle of maximum brightness on the CRT when the set is turned off.

The brightness is mainly a function of the d.c. voltage between cathode and grid of the picture tube. In some receivers the cathode gets the picture signal and then the grid is at a d.c. potential, adjustable by the brightness control. Other models use grid drive with the cathode as the d.c. brightness-controlling element. Maximum brightness occurs when the grid is either at the same potential as the cathode or slightly more positive than the cathode. The purpose of each of the four switches S is to effect this condition at "Off" without interfering with the video signal. In order to function correctly, switch S must be part of the "Off-On" a.c. switch. Some receivers use a double-pole, single-throw switch mounted at the end of some other control, but the majority use only a single-pole switch. Fortunately most of the potentiometer manufacturers also market doublepole, single-throw switches which will fit in the same spot as the singlepole switch. It is necessary to ascertain the exact make and type of potentiometer and then buy a suitable switch.

Fig. 1A illustrates a case where the cathode is directly connected to the video amplifier and the grid receives its d.c. voltage through the divider network R_1 , R_2 . As the set is turned

off, switch S connects the grid to "B plus", making the grid momentarily more positive than the cathode. In the next instant the "B plus" voltage is shut off, the HV source is also removed, and the charge on the HV condenser has passed through the picture tube during the brief moment when the grid was more positive than the cathode. The same principle is used in case Fig. 1B where the grid is essentially at "B plus" and the cathode is connected to ground through switch S. Figs. 1C and 1D show arrangements where the grid is at ground potential or the cathode at about one-half the "B plus" voltage. In either case the spot blanking is accomplished by switching the d.c. element to give maximum brightness. Although actual circuits will vary, most TV receivers will use some scheme similar to one of these four circuits for driving the picture tube. If one remembers to make connection only to the d.c. element, the one having condenser C_1 going to ground, no difficulties should be encountered.

The second method for removing the spot is to cause the electron beam to move either sideways or up or down right after the set is turned off. In the electromagnetic-focus type sets the d.c. flowing through the focus coil as the "B plus" was shut off often accomplished this deflection. In addition, the loss of focus current prevented a focused spot from appearing, resulting in such a dispersed electron beam that it was hardly noticeable. New, automatic-focus picture tubes retain focus much longer, therefore the spot is more visible. One of the simplest methods of deflecting the spot consists of mounting a small permanent magnet either on the flared portion of the tube or at some convenient point on the cabinet or tube mounting. Locate the magnet at either top or side so that it deflects the picture slightly. When the set is turned off, the deflection-yoke power is gone, less HV is applied, and only the magnet affects the electron beam. In this condition the effect of the magnet is usually enough to move the spot completely off the screen. When operating normally the deflection yoke has much more control than the magnet and keeps the picture properly centered. Where a PM centering magnet is used this should not be disturbed or used to recenter the picture because it will counteract the additional small magnet. Twisting the deflection yoke slightly will be sufficient to overcome the small decentering due to the new magnet. Taping the magnet in place after its best location is determined, cures the spot appearances once and for all.

Vertical Retrace Lines

The photograph, Fig. 2, shows the appearance of vertical retrace lines when either insufficient blanking, a weak picture, or a slightly weak picture tube prevent perfect reception. In the last instance a picture tube rejuvenator may help for a while, but

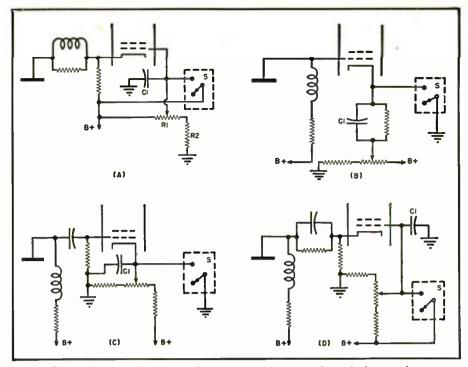


Fig. 1. Four switching methods to remove the spot on the cathode-ray tube. All switches are to be ganged with the "Off-On" switch. (A) Circuit where cathode is directly connected to video amplifier. (B) Circuit where grid is at "B plus" and cathode is grounded through S. (C and D) Circuit where grid is at ground potential or the cathode is at about one-half the "B plus" voltage.

the best permanent solution is, of course, a new picture tube. There are, however, various other reasons for the appearance of these retrace lines. Usually it is due to either insufficient video signal or excessive brightness, Normally the blanking pulses extend into the "blacker than black" region of the video signal and cut the picture tube off during the retrace period. If the video signal is so weak that it does not go sufficiently negative to cut the tube off at the retrace period, the lines will appear. Even with a fairly strong picture the brightness control may be set so far that the blanking pulses cannot reach the cut-off voltage of the picture tube. It may even be necessary for the brightness control to be advanced that far in order to overcome the ambient light. In those instances where the picture is satisfactory with the exception of vertical retrace lines, a simple auxiliary blanking circuit can be added. Several major manufacturers include these circuits in their de-

The principle used here requires that in addition to the blanking pulse contained in the video signal, a strong

pulse be applied to the picture tube during the vertical retrace time. This additional pulse is obtained from the vertical output section and, in order to cut the picture tube off, must be positive when applied to the cathode and negative when applied to the grid. For simplest circuitry the additional pulse should always be applied to the element not driven by the video signal. Three basic circuits are shown in Fig. 4. In Fig. 4A the grid of the picture (Continued on page 148)

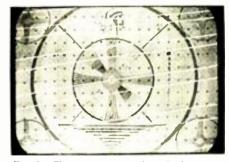
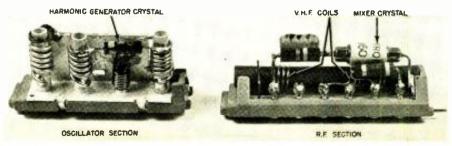


Fig. 2. The appearance of vertical retrace lines when there is insufficient blanking, a weak picture, or a weak picture tube.

Fig. 3. Close-up view of the u.h.f. strips used in the Standard Coil tuner.





V.F.O. MULTIPLIER

A COMPACT

Front chassis view of the home-built v.f.o.-multiplier. Three type 6AG7 tubes are used in this compact unit.

By EARL SNADER, WØZFO

Construction details on a low-power driver for 80-75, 40, and 20 meters. Power output is about .2 of a watt.

F YOU are looking for a compact v.f.o.-controlled bandswitching multiplier for that new pint-sized medium power rig you are building, here is something that may fill the bill. This unit delivers two-tenths of a watt output on 80-75, 40. and 20 meters, enough to drive a 2E26. Frequency control is by means of a builtin v.f.o. operating in the 3.5 to 4.0 megacycle range. A Clapp oscillator circuit is used in the v.f.o. Interstage coupling is by means of broadband couplers, eliminating the need for any separate multiplier tuning controls. The tuning condenser for the v.f.o. is mounted with a National type SCN dial drive mechanism. One gang of a three-gang, five-position, twocircuit-per-gang bandswitch projects out the rear of the chassis, to be used for bandswitching in circuits independent of the multiplier. The entire v.f.o.-multiplier assembly is mounted on a chassis 734" wide by 4" deep by 3" high. Power requirements include 6.3 volts a.c. at 2 amperes for heaters, 75, 105, and 180 volts regulated for the v.f.o. screen, plate, and multiplier screens respectively, and 300 volts for the multiplier plates. Three type 6AG7 tubes are used.

Since no commercially-built chassis could be found with the right dimensions, one was constructed out of heavy gauge aluminum. It was made in three parts: the top plate measuring 7%" by 4"; the base measuring 7%" wide, 3" high, and 4" deep; and a small partition 3" high by 4" wide. In the finished assembly this partition divides the v.f.o. and multiplier com-

partments and provides a mounting surface for the v.f.o. tuning condenser and the broadband coupler trimmers. The chassis base and the partition were both made with 1/2" flanges on the bottom and the top. Since the partition is fastened to the top plate before the top plate and chassis base are assembled, notches must be cut in the top flanges of the chassis base to pass the partition for assembly. It will be necessary also to cut small pieces out of the front edge of the partition to clear parts of the National SCN dial drive mechanism. Otherwise the partition should fit fairly snug inside the chassis base.

All the coils and the tube sockets are mounted on the top plate, and the location of each can be seen from the photograph. Since the v.f.o. tuning condenser is mounted on the partition, the condenser shaft should be aligned with the dial drive mechanism in the front of the chassis before the partition is permanently fastened in place. A Hammarlund type MC-50 variable condenser was used because it is ruggedly built and well suited for v.f.o. applications. Any good 50 µµfd. variable condenser could be used, provided it is equipped with double bearings and brass plates. This condenser is mounted with enough clearance between it and the top plates to allow room for the wiring associated with the v.f.o. tube socket. The v.f.o. tube socket is mounted directly above the v.f.o. tuning condenser. The trimmers for the broadband couplers are mounted on the opposite side of the partition from the v.f.o. tuning condenser. They can be mounted on a small bracket first and then fastened to the partition as a unit. Care must be taken to provide a good path for r.f. from the one lug of each trimmer to the chassis because they are grounded in that way.

The bandswitch must be partially disassembled for mounting to the chassis base. The sleeves separating the second from the third gang on this switch must be shortened. A hole is drilled for the shaft to pass through the front of the chassis, and the shaft is mounted securely in this hole with a panel bearing. Three holes, carefully aligned with the shaft hole in the front, are drilled in the rear of the chassis. One of these is for the shaft. The other two are for the switch assembly screws. The rear gang of the switch is then mounted on the back of the chassis, separated from the chassis by " fiber washers. Since the front mounting of the bandswitch will be some distance inside the front of the chassis base, a small aluminum bracket is provided to anchor the front of the switch to the chassis base.

The v.f.o. trimmer is mounted on the rear of the chassis base, directly behind the v.f.o. tuning condenser. There is nothing particularly critical about the location of this trimmer. There should be just enough room to mount it without crowding.

The v.f.o. tank coil consists of 60 turns of No. 28 plain enameled wire, closewound on a slug-tuned ceramic coil form 1/2" in diameter. A Millen type 69045 form was used in the original model. This is mounted in one corner of the v.f.o. compartment, behind the v.f.o. tube socket and about %" from the edge of the chassis. The cathode choke in the v.f.o. circuit. a National 2.5 mhy., type No. R-100S, is mounted in the front corner. The v.f.o. plate choke, a pigtail r.f. choke with an inductance of 2.5 mhy., is mounted between the plate lug of the v.f.o. tube socket and a terminal tie strip which also serves to terminate the plate power lead to the v.f.o. and provide a ground connection to the chassis.

The broadly resonant coil in the plate of the first buffer-multiplier tube is closewound on an *Amphenol* type No. 24 polystyrene form ¾" in diameter and 2½" long. The winding consists of 85 turns of No. 30 plain enameled wire. Single hole mounting is used, and the coil is located about 5%" behind the first multiplier-buffer tube socket.

The two broadband couplers are also wound on Amphenol type No. 24 polystyrene forms 34" in diameter. The 40-meter coupler consists of two coils of 27 turns of No. 28 plain enameled wire. These coils are closewound, and spaced 7/16" from each other. The center leads go to the "cold" connections of the coil (the bypass to ground and the 300 volt plate supply lead). The 40-meter coupler can be seen in the photograph showing a bottom view of the v.f.o.-multiplier unit. It is located just behind the bandswitch shaft. The 20-meter broadband coupler is not visible in the photograph, being hidden from view by the bandswitch. It is wound exactly like the 40-meter coupler with the exception that the coils each consist of 16 turns of No. 24 plain enameled wire. Both couplers are mounted with their axes parallel to the top plate but at right angles to each other. The 40-meter coupler is located along the rear edge of the top plate, far enough in from the edge to clear the flange on the chassis base. The 20-meter coupler is mounted along the side of the top plate and near the front. Small brackets were made from heavy gauge aluminum to mount the coupler coils to the top plate in the proper position. When mounted, the couplers should be spaced at least 1/8" from the nearest metal, whether it be the bracket or the top plate. This is extremely important and should be carefully noted.

Most of the wiring can be completed before the top plate is put in place. The wiring to the v.f.o. tuning condenser and trimmer, the broadband coupler trimmers, and the bandswitch is done last, after the top plate and

S1=3,4:40 METERS
5:20 METERS
6:20 METERS

Complete circuit diagram of the bandswitching v.f.o.-multiplier. Two switch positions are provided for the 80.75 meter band and the 40-meter band to allow for switching external circuits to cover the different portions of each of the bands.

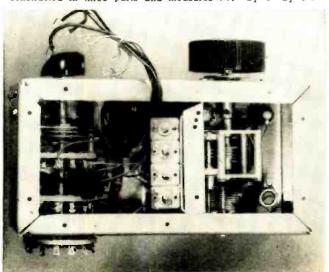
chassis base have been assembled together. Wire the filaments first, followed by the cathode and grid resistors and bypass condensers, and then finally the power leads. Condenser Co is mounted between a feedthrough insulator in the partition and the grid connection on the first multiplierbuffer tube socket (lug No. 4). Disc bypass condensers are used throughout, to save space and to reduce stray capacitances in the wiring. All bypass condensers and ground leads should come together at one place, to be grounded to the chassis at one place in the multiplier compartment and at one place in the v.f.o. compartment. A single bypass condenser serves to provide a path for r.f. to ground at the "cold" end of each of the three plate coils in the multiplier section. C performs this function, and coil leads to this condenser should be made

as short and direct as possible. Grid and plate leads in the v.f.o. should be No. 14 bus wire. It is particularly important that all connections in the oscillator circuit be sweated together, because even a slight resistance in any of them may render the oscillator inoperative. This is particularly true of the connections between the rotor of the v.f.o. tuning condenser and the v.f.o. tube itself.

In wiring the bandswitch and the broadband coupler trimmers, connect the lead from each coil to the bandswitch first. Then run the trimmer lead from the bandswitch connections rather than from the coils themselves. The screen lead to the second multiplier tube can be connected to the least accessible section of the bandswitch. This is the underside of that

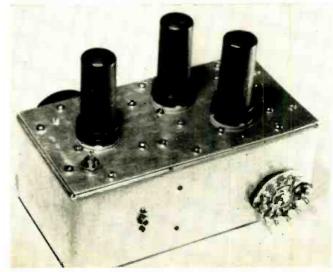
(Continued on page 152)

Under chassis view of unit. The compact aluminum chassis was constructed in three parts and measures 7%4'' by 4'' by 3''.



February, 1953

Rear view of v.f.o.-multiplier. The rear gang of the switch is mounted on the back and separated from the chassis by washers.





Design and construction data on a compact unit and its speaker enclosure. Quality parts are used throughout.

ODERN television receivers, with their large picture tuber proved circuitry, are capable of producing pictures of excellent size and quality. However, the sound sections of all too many of the television receivers currently in use have been sadly neglected. The audio stages in many of the receivers are no better than those found in the cheap "garden variety" a.c.-d.c. sets, and their speakers are often placed where they receive insufficient baffling. In an effort to overcome these shortcomings, the writer designed the amplifier and speaker combination described in this While this combination is capable of producing excellent results,

Over-all view of the author's unit showing amplifier and associated speaker cabinet.

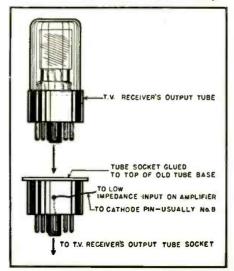


its price is not excessive and it can be easily constructed without resorting to trick circuits. The amplifier can be connected to an existing television receiver without "major surgery," and the speaker enclosure can be used as a convenient stand for a table model receiver or placed alongside a console.

Fig. 2 is the schematic diagram of the amplifier. The power supply section is conventional, consisting of a 5Y3 full-wave rectifier followed by a single-section LC filter. The bleeder resistor $(R_{\rm m})$ is used to absorb power from the rectifier while the other tube heaters are reaching operating temperature, thus preventing excessive voltage from appearing across the filter condensers. If a slow-heating rectifier, such as a 5V4, is used the resistor can be eliminated.

Much consideration was given as to the type of output tubes to use in

Fig. 1. Method for connecting amplifier into television set without major rewiring.



this amplifier. Although triodes are usually preferred because of their excellent speaker-damping qualities and stability, they are relatively expensive and, more important, they are hard to drive, usually requiring a push-pull driver stage. After consulting the tube manuals, it was decided to use a pair of 6F6's pentode connected, operating strictly class A. When operated in this manner, 6F6's require a grid-togrid driving voltage of 58 volts for a power output of 10.5 watts. Although 6F6's can be operated as triodes, they then require a grid-to-grid driving voltage of 123 volts for a power output of 13 watts.

The split-load type of phase inverter was chosen to drive the output stage as it will easily provide the 58 volts grid-to-grid required by the pentode-connected 6F6's, with low distortion and good balance throughout the audio range. The cathode and plate load resistors in this stage should be a matched pair in order to have equal output voltages. The cathode and plate-load resistors were made rather low in value in order to assure good high frequency response and also to keep the cathode-to-heater voltage as low as possible, thus reducing hum difficulties.

A 6J5 is used as a voltage amplifier and is direct-coupled to the split-load phase inverter. This is possible due to the high positive voltage on the phase-inverter cathode. This direct coupling extends the response of this stage down to d.c. and since there is no coupling condenser, one source of phase shift is eliminated. It should be noted that there are only two coupling condensers in the circuit between the grid of the 6J5 voltage amplifier and the output transformer..

Negative feedback is applied to the unbypassed cathode of the 6J5 from the secondary of the output transformer. The amount of feedback that can be applied depends, to a large extent, upon the characteristics of the output transformer used. Therefore, a

good quality transformer should be used. The UTC CG-19 output transformer is recommended. Although not as expensive as many of the larger units. it is capable of excellent performance. With feedback, the amplifier is flat from 20 cps to over 20 kc. with no sign of instability. When installing the feedback resistor (R_{ii}) a scope should be connected to the amplifier to make sure that no ultrasonic oscillations exist when the desired amount of feedback is obtained. If a loud squeal or motorboating is heard with the feedback loop connected, reverse either the primary or secondary connections (not both) to the output transformer. The value of the feedback resistor shown in the schematic is correct when using the CG-19 output transformer. If a different transformer is used, it is recommended that a pot, be installed temporarily in place of the feedback resistor, and adjusted for the proper amount of feedback. After setting the pot, for the proper amount of feedback, measure the resistance across the pot, and install a fixed resistor in its place.

The tone control stage uses the Thordarson degenerative tone control circuit employing one half of a 6SN7. The operation of this circuit is as follows: The cathode resistor in this stage is higher in value than the plate resistor, hence most of the signal appears across the cathode resistor. The circuit being resistive, the stage gain is equal for all frequencies. For bass boost, the cathode resistor is shunted with a suitable inductance. Degeneration of the lower frequencies is greatly reduced due to the low impedance of the inductance at low frequencies, consequently the gain of the stage is greatly increased at the lower frequencies. To attenuate the bass, the same inductance is introduced into the grid circuit of the following stage. In this case, the low impedance of the inductance at low frequencies bypasses the low frequencies to ground. For treble boost, a condenser is shunted across the cathode resistor of the tone control stage. The lowered impedance of the condenser at high frequencies causes a decrease in degeneration at the higher frequencies, consequently the stage has more gain at the higher frequencies. The highs are attenuated by shunting a condenser across the next stage grid resistor, thus hypassing the high frequencies to ground.

The input stage uses the other half of the 6SN7 connected either as a grounded-grid amplifier (for low-impedance inputs) or as a conventional amplifying stage (for high-impedance inputs). For low impedance inputs, the jack of the amplifier is connected across the 1000-ohm cathode resistor R_{\circ} . As long a connecting cable as desired can then be connected to the cathode resistor of the audio output tube in the television receiver. In order to avoid elaborate surgery on the receiver, an adapter such as is shown in Fig. 1 can be made. Then it

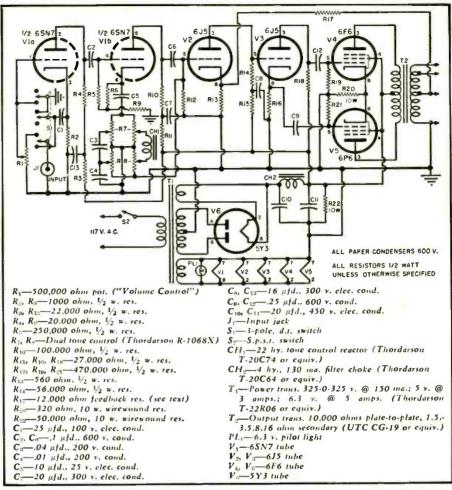
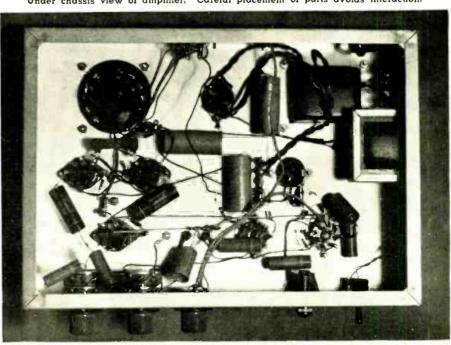


Fig. 2. Complete circuit diagram of amplifier. Quality parts are used throughout.

is only necessary to remove the audio output tube in the receiver, insert the adapter in the socket, and then insert the output tube into the adapter. It is necessary that any cathode bypass condenser connected across the output tube's cathode resistor be removed.

This may mean a slight decrease in output due to degeneration, however the response of the stage will be improved. If it is desired to silence the receiver's speaker when using the amplifier, it can be disconnected from the (Continued on page 94)

Under chassis view of amplifier. Careful placement of parts avoids interaction.



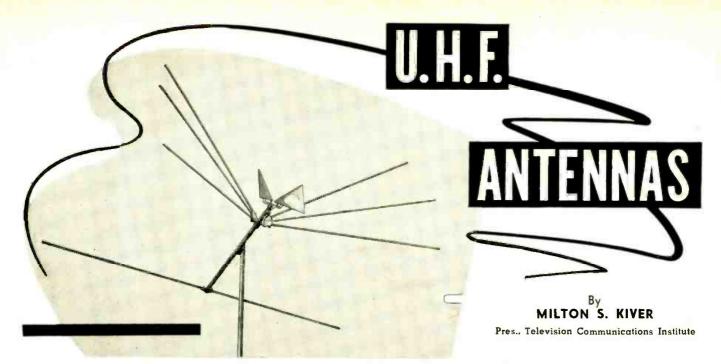


Fig. 1. A combination v.h.f.-u.h.f. antenna. This is the "Jetenna 283" made by JFD Manufacturing Co.

Part 3. Details on some of the combination v.h.f.-u.h.f. arrays which are now being marketed by antenna companies.

PROBLEM that will soon be facing many TV set owners and technicians is that of choosing the u.h.f. antenna best suited to their location and station frequency. In areas where only u.h.f. stations are assigned, the choice will be between the various u.h.f. antennas available. But in many parts of the country there will be both u.h.f. and v.h.f. signals and for these locations the following choice will exist.

1. To use one all-v.h.f. antenna and one u.h.f. antenna, each with its own lead-in line.

2. Or, to use a combination v.h.f.-u.h.f. array with a single lead-in.

Choice No. 1 is the more flexible of the two and generally will provide the set with stronger signals. Whenever you combine two arrays possessing widely differing responses, a certain amount of loss will be incurred by both sections. If the combination antenna stems from the basic "V" array, then the angle of the antenna rods which is best for v.h.f. reception will not be best for u.h.f. reception. By the same token, the best adjustment for u.h.f. reception is not the most desirable for v.h.f. signals. And, as is most common, when you choose a compromise position, then reception suffers in both regions.

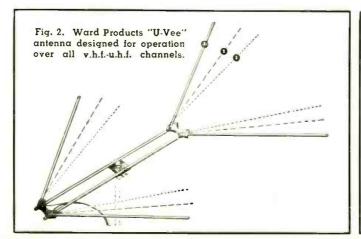
If the combination array is of the type shown in Fig. 1, some sort of decoupling network must be inserted between the u.h.f. and v.h.f. elements. In essence, what we are principally trying to do with this decoupling or filter network is to prevent the v.h.f. assembly from affecting u.h.f. response. (The u.h.f. antenna will usually have little effect on the v.h.f. response and for

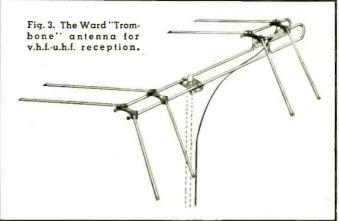
most practical purposes may be disregarded.) Signals passing through the decoupling network will suffer some attenuation and in this respect, less than optimum operation will be obtained.

On the other hand, whatever loss is occasioned by combining v.h.f. and u.h.f. elements in strong and medium signal areas will have little noticeable effect on the picture. Furthermore, combination arrays will be more economical, both from the standpoint of initial cost and of subsequent installation, and cost is a very potent factor in sales.

The consensus among antenna engineers is that while better results are generally obtainable from separate v.h.f. and u.h.f. arrays, a substantial market will exist for combination arrays and these will be manufactured in quantity.

The opening of the u.h.f. band has only just begun and the number of combination arrays is still quite limited. Many manufacturers, when asked about their plans, indicated a "waitand-see" attitude. However, several combination arrays have already been marketed and it may be of interest to





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examine these to see what form they take and how they operate.

JFD's "Jetenna 283". JFD has recently announced an array to operate over all v.h.f. and u.h.f. channels. Shown in Fig. 1, it is seen to consist of a low band conical for v.h.f. signals and a broadband triangular (or fan) dipole for u.h.f. signals. A single leadin line delivers signals to the receiver through the use of a special coupling device mounted directly at the antenna itself.

By virtue of the positioning of the various elements, the active rods of the v.h.f. array serve as reflectors for the u.h.f. dipole. The v.h.f. elements, in turn, have their own reflector. A gain close to 9 db is available from the v.h.f. section while the u.h.f section gain will be on the order of 4 db. The u.h.f. plates are stamped of aluminum, with a tip-to-tip length of 16 inches. The array will match a 300ohm line. Finally, the two triangular plates of the u.h.f. array will have a forward angle of 35 degrees to match the forward inclination of the v.h.f. elements.

Vertical directivity of this u.h.f. array is quite broad but the horizontal directivity, with the reflector elements, is good. For local areas surrounding a u.h.f. station where ground reflected signals are low, good results may be obtained with this array.

"V" Type Combination Antennas. The ability of a "V" type of antenna to receive v.h.f. and u.h.f. signals was briefly mentioned in the first article of this series. Several antenna companies have taken advantage of this property to devise modified "V" antennas which will operate over all channels with good gain.

The modified array which all manufacture in one form or another is shown in Fig. 2. Basically, the array consists of four rods; two at the front and two at the rear. The lead-in line to the receiver (300-ohm twin-lead) connects to the two rear rods. Comparing this arrangement with arrays with which we are familiar, the only conclusion we can draw regarding the front two rods is that they serve here as directors. This they do. However, closer examination of the array indicates that unlike more conventional arrays, the two front rods are electri-

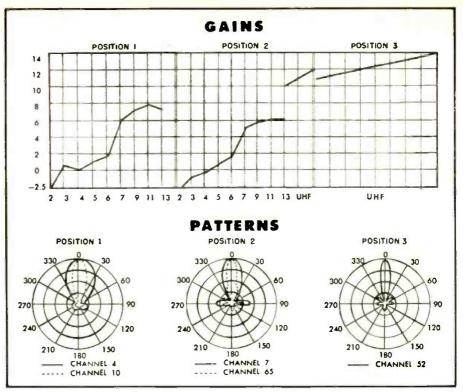


Fig. 4. A comparison of the response curves and the antenna gain for each of the three positions of the Ward Products' "U-Vee" antenna. See Fig. 2.

cally connected to the two rear units through the two rods comprising the "boom". The purpose of these connecting rods is two-fold.

First, the two connecting rods serve as a transmission line to conduct whatever signal is picked up by the two front rods to the two rear rods. In addition, the two rear rods also pick up that portion of the signal which passed over the front rods and combine this with the energy received from the front rods via the connecting rods. Obviously, to obtain maximum results from this combination, the length of the connecting rods must be carefully chosen. Signal pick-up from the rear of the array is low because the energy which approaches the array from the rear is captured by the front and rear rods and combines out-of-phase and is therefore cancelled out.

The second purpose of the connecting rods is to support both front and

rear dipoles and produce a mechanically sturdy array.

It is characteristic of "V" type antennas that the longer each side of the "V" becomes as compared to the operating frequency of the signal, the narrower the angle between the sides must be for an optimum high-gain, single-lobe pattern. Thus, if we use the same "V" for operation on low-and high-band v.h.f. and for the u.h.f. region, then the angle to which the bars must be set depends upon the conditions in your locality.

In position No. 1, Fig. 2, reception is best on the v.h.f. band. The included angle between the rods is 90°. The manufacturer also suggests application of this antenna with the 90° angle for scattered u.h.f. stations in a metropolitan area. In such strongsignal u.h.f. service areas a careful check at the time of antenna installation can determine a fixed position for the 90° array that will allow good re-

Fig. 5. The JFD "Ultra V-Beam" antenna for v.h.f.-u.h.f. use.

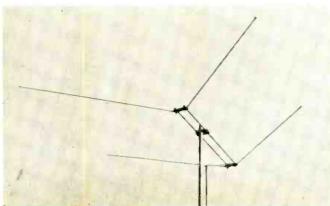
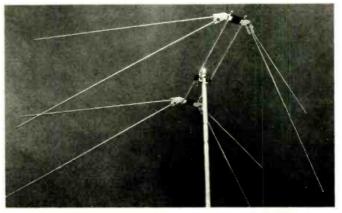


Fig. 6. Another combination v.h.f.-u.h.f. array, made by RMS.



February, 1953

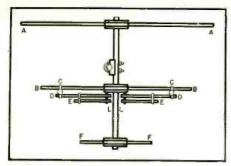


Fig. 7. The v.h.f. portion of the "Ultra Q-Tee" antenna shown below in Fig. 9.

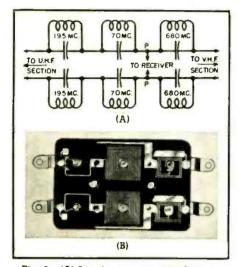


Fig. 8. (A) Low-frequency equivalent circuit filter which prevents interaction between v.h.f.-u.h.f. sections of "Ultra Q-Tee". (B) Actual appearance of filter.

ception on all nearby u.h.f. channels together with both near and distant v.h.f. channels.

In position No. 2, Fig. 2, the included angle is now 60°. Reception is divided between v.h.f. and u.h.f. channels, with the highest u.h.f. channels suffering the most due to lobe break up.

In the final position, No. 3, Fig. 2, the included angle between the dipole rods is 45° and now best reception is obtained on the u.h.f. channels, especially those located above 750 mc. The v.h.f. reception in this position is below normal and likely to be unsatisfactory except in strong v.h.f. signal areas.

A comparison of the response curves and the antenna gain for each of the

three positions is given in Fig. 4. Note in all instances how much better this array performs as the frequency rises. This is an especially desirable characteristic for u.h.f. reception.

The "U-Vee" antenna, as this array is called by its manufacturer (The Ward Products Company), can be obtained stacked for improved reception. (JFD produces a similar antenna but calls it the "Ultra V-Beam." See Fig. 5. Its rods also have provision for altering the included angle to suit the frequency or frequencies of the stations to be received.)

Ward Products has a variation of the "V" antenna which it calls the "Trombone." See Fig. 3. Use of this antenna on the u.h.f. channels is similar but not identical in principle to the "U-Vee" array. The 90° angle for all four "V's" that gives best fringe-area performance on both v.h.f. bands will produce multiple lobes over the u.h.f. range. This can still be useful in the primary service area of u.h.f. stations but it will prove unsatisfactory in weak signal areas or where there are multiple reflections.

According to the manufacturer, the "Trombone" is not peaked for a single lobe over the u.h.f. hand by using the 60° angle (mid-position) for all four "V's". This arrangement gives highest gain on only the lowest u.h.f. channels (near 500 megacycles) and reduces the gain in the v.h.f. band. A better choice for good low-channel "Trombone" performance is to set only the forward pair of "V's" to 60°, leaving the back pair (on the "Trombone" loop) at 90°. When the high end of the u.h.f. band comes into use, above Channel 62, the forward pair of "V's" can be set at 45° included angle for top performance with minimum reduction in v.h.f. gain.

The best choice for the majority of the u.h.f. channels is to set the three forward "V's" to 60° and the back "V" at 90° (widest angle). This gives optimum gain at u.h.f., with a partially-split forward lobe that is said to allow considerable latitude in lining up different u.h.f. stations, but still giving a good front-to-back ratio and minimum side lobes for ghost rejection. Performance on the v.h.f. channels is still good, with a fairly narrow main lobe and good front-to-back rejection.

Variations on the basic "V" are end-

less and it may be expected that different manufacturers will put other twists in it. The *RMS* array is shown in Fig. 6 and it is seen to possess two rods at each point where the "V" of Fig. 2 uses one. Stacking of the "V's" is shown in Fig. 10. "Q" bars are used to connect the upper and lower stacks and are so designed to raise the apparent impedance of each section so that the antenna will work effectively into a 300-ohm load.

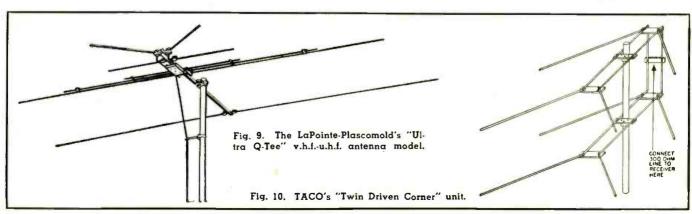
The "Q-Tee and "Ultra Q-Tee". The "Ultra Q-Tee" antenna, Fig. 9, is another combination v.h.f.-u.h.f. array that possesses a number of features which differ from the other combination antennas we have just discussed. The u.h.f. portion of this array consists of the two foremost rods that are tilted forward. The straight rod just behind them serves as the reflector. The same straight rod also serves as a director on the upper v.h.f. band for the array of rods that are positioned behind it. These other rods form the v.h.f. section of this array.

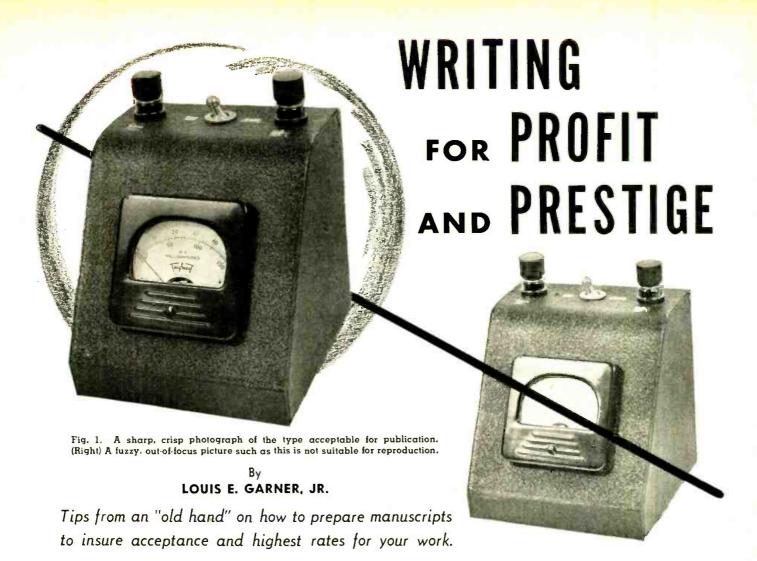
In order to understand the reason for using this particular form of antenna, let us first consider the v.h.f. section. This is shown in Fig. 7. Dipole B-B is cut for a half-wavelength at 63 me. (Channel 3) and this rod is designed to receive all of the low-band Channels (2-6). Rod A-A is the reflector for dipole B-B and its length is somewhat greater than B-B's.

Dipole D-D is cut for a full wave at the center of the high v.h.f. band C,C are printed circuit isolation filters, resonant at 195 mc. and designed to isolate the low-channel dipole (B-B) from the high channel dipole (D-D). Rod E-E, a matching and phasing section, performs a dual function and accounts for the operational characteristic of this antenna. On the high v.h.f. channels elements E-E are "T" match sections which tap the dipole (D-D) and provide a 300-ohm termination at (L-L). The high channel antenna is, therefore, a full-wave antenna "T"matched, with a half-wave director (F-F)

On the low channels the isolation filters (C,C) have a low-inductive impedance since they operate below their resonant frequency. The high channel dipole (D-D), combined with element (E-E), forms a double "T" matching section which taps dipole (B-B) to

(Continued on page 120)





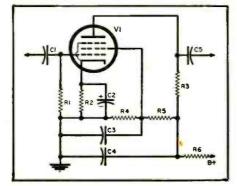
ONSIDERING the number of experimenters, technicians, and radio amateurs in the nation, the variety of available subjects, and the excellent rates paid by technical magazines, it is indeed surprising that more of these men don't turn to writing for prestige and profit. Technical writing offers a way for experimenters to make their hobby self-supporting, for radio-TV technicians to profitably fill in their "no-work" time, and for beginning engineers to gain professional recognition,

Probably every ham or engineer who has worked on or designed a new test instrument, an interesting control device, or a "gadget," and every technician who has developed a new "kink" in his service technique, could write an interesting and salable article -provided he took the time to do so and, equally important, went about the job in the right way. For good technical articles don't just "happen" -there is a definite technique to writing articles that will sell; a technique that may be applied equally well by the beginner or the experienced man, and a technique that will go a long ways towards insuring success irrespective of the comparative writing skill of the individual.

Before starting an article, or even an outline, for that matter, the prospective writer should make an important decision—whether the article is to be written primarily as a means of securing additional income, or primarily for professional recognition (although both types of compensation may result). This decision will determine to a large extent the available market, the possible subjects, and the type of presentation.

Articles published by the official organs of professional groups and societies carry the greatest prestige value, although the monetary compensation may be very low. In fact, many professional journals accept the articles as "contributions" without any cash payment whatsoever. This does not

Fig. 2. Neatly and clearly drawn diagrams, with all of the components properly identified, add value to your manuscript.



imply that their standards are low. Often, it will prove quite difficult to prepare an article measuring up to the high standards enforced. However, junior engineers find that preparing papers for professional journals offers an excellent means of gaining recognition and prestige.

Professional journals often have stringent rules for submitting manuscripts and prospective authors should obtain all the necessary information from the editors before starting an article or paper. In many cases, manuscripts must be typed in a certain manner, must be submitted in duplicate or triplicate, and all drawings must be finished ink drawings suitable for reproduction.

The more popular technical magazines, on the other hand, are not as strict concerning the mechanical preparation of the article, but may be many times more critical on the style of presentation—they all insist on an informative, easy-to-read, easy-to-understand, and, above all, interesting article. Since writing an interesting article is often more difficult than writing a "letter-perfect" but dull article, the compensation is greater. A technical writer, preparing an article for the more popular technical magazines, may be able to average as much as \$15 to \$30 an hour for actual writ-

(Continued on page 133)



Fig. 1. The "Vest-Pocket Receiver" housed in a small plastic box.

Complete construction details on a compact unit which incorporates a commercially-available printed circuit.

HERE are two basic approaches that may be used in designing a radio receiver. The more popular approach is to provide considerable r.f. (or i.f.) gain, together with comparatively little audio gain after the detector. This approach is mandatory in the case of sensitive receivers, where weak r.f. signals must be picked up, and where the signal-to-noise ratio is important.

In the case of receivers to be used only on local broadcast stations, where high signal levels are usually encountered, a different design technique may be employed. Little or no r.f. gain may be provided, together with considerable audio gain. A receiver may consist of no more than an antenna, a tuned circuit, a detector, and a high-gain audio amplifier. This approach was used successfully in designing and building the small receiver shown in Fig. 1.

Although a very short antenna is used, the receiver is sufficiently sensitive to give ample earphone volume with local AM broadcast stations (5-15 mile radius).

As can be seen in the "close-up" view (Fig. 3) the receiver is completely self-contained, with both "A" and "B" batteries within the plastic case. The extremely small size of the receiver is evident in both Figs. 1 and 3. Compare the complete receiver with the size of the standard penlight battery used as the "A" supply!

Because of its small size and light weight, this receiver is handy for use when working in the garden, mowing

the grass, hiking, cycling, or when attending sports events.

The layout and construction is such that the average skilled technician should have no difficulty assembling and wiring the complete receiver in an afternoon and evening.

Circuit Description

The complete schematic diagram for the receiver is given in Fig. 2. The circuit enclosed by the dashed line is a complete Centralab printed circuit amplifier and is mounted and wired as a single component. Hence, the individual resistors and condensers in this circuit are identified only by parts values.

The r.f. signals picked up by the antenna are coupled through C_1 to a tuned circuit consisting of L_1 and C_2 , where the desired station is selected. The r.f. signal appearing across the tuned circuit is coupled, in turn, to the grid of the first CK512A amplifier tube through C_3 , appearing across R_4 . Gridleak detection takes place at this point (due to the high value of R_1), and hence there is only an audio signal to consider in the remainder of the cir-

The amplified audio signal appearing across the 1-megohm plate load resistor of the first CK512A amplifier is coupled through a .001 µfd. condenser to the volume control, R2. From here the signal is applied to the grid of the second amplifier, another CK512A tube.

Only two stages of voltage amplification are provided, so the signal appearing across the 1-megohm plate

E. G. LOUIS

load resistor of the second CK512A tube is applied directly to the grid of the CK525A power amplifier stage through another .001 µfd. coupling condenser.

The output signal appears across a subminiature choke, L2, and is coupled through C_4 to the output jack.

Operating voltages are obtained from a 1.5 volt standard penlight cell, which acts as the "A" battery, and a 30-volt hearing aid "B" battery. If desired, one of the new mercury cells may be substituted for the "A" battery to provide longer life-a Mallory type RM-1200 mercury cell is suggested.

Construction Hints

The layout used by the author is readily apparent from the photo (Fig. 3). However, this layout need not be followed exactly-in fact, some modification will be mandatory unless the case used by the builder is exactly the same shape and size as that used by the author. When modifying the layout, take care to keep the output and input connections to the printed circuit amplifier well separated to prevent oscillation.

A suitable case for the receiver can generally be found at a dime store or at a plastic "hobby" shop. The one used by the author was obtained in an assortment purchased from the Olson Radio Warehouse (Akron, Ohio). Dimensions are approximately 21/2" x

Most of the major parts are mounted simply by cementing them in place using Duco cement. However, a pair of small cable clamps is used to hold the antenna in place along the side of the receiver case. The batteries are held in place by the spring tension exerted by U-shaped pieces of phosphor bronze cemented to the case. These "clips" also serve to make contact with the battery terminals.

The "antenna" was salvaged from the upper section of a damaged auto antenna. The length is not too critical but at least a 12" length should be used and a 14" or 16" length will give somewhat better results.

A standard "Ferri-Loop" antenna which has been modified to fit into the small space available serves as the tuning coil (L_1) . This coil, as supplied by the manufacturer, is fairly long, with most of the length represented by a cardboard tube and the mounting bracket. The excess tube length was cut off using a sharp pocket knife and the remaining coil (with its core) cemented in place. In Fig. 3, this coil is located below the trimmer condenser and at the end of the "A" battery.

Station tuning is provided by a mica compression trimmer (C2) which may be adjusted be means of a small screwdriver. Only a portion of the band is covered by the trimmer and it becomes necessary to choose a value that will permit tuning the desired station(s). The value given in the parts list covers the upper portion of the broadcast band (1000 to 1500 kc.). To cover lower portions of the band, use a trimmer having a greater maximum capacity values of 270 µµfd., 360 µµfd., 480 μμfd., etc. are satisfactory. The exact portion of the band covered will depend not only on the trimmer size but also on the exact positioning of the iron core in the coil.

A miniature output jack was obtained by cutting a Walsco type 791 jack to almost half its normal length and cementing it in place in the plastic case. This component is visible in Fig. 3 and is located just above the output choke. The phone plug supplied with the Telex midget earset was removed and a Walsco type 790 plug used instead (to match the miniature jack).

The output choke, L_z , may be replaced by a 50,000 ohm, $\frac{1}{4}$ watt resistor if desired, giving somewhat less gain, but saving considerable space as well as reducing the cost of the completed receiver. In fact, in the model shown, the choke was accidentally damaged and later developed an "open." Rather than attempt to remove the choke, a 50,000 ohm resistor was simply soldered in parallel with the choke connections, giving satisfactory results.

Somewhat higher over-all gain may be realized by using a crystal head-phone in place of the 2000-ohm magnetic earset shown. However, when this is done it may become necessary to shield the case to prevent feedback and oscillation.

Adjustment and Tuning

Since the wiring and assembly of the small receiver are straight-forward, little or no difficulty should be encountered. There are two points on which some builders may run into a little trouble, however.

First, if care is not taken in layout and wiring, it may be found that overall oscillation takes place. In such a case, better separation between the output and input is advisable. In a few instances it may become necessary to shield the entire receiver, either by assembling it in a small metal case (such as a cigarette case)

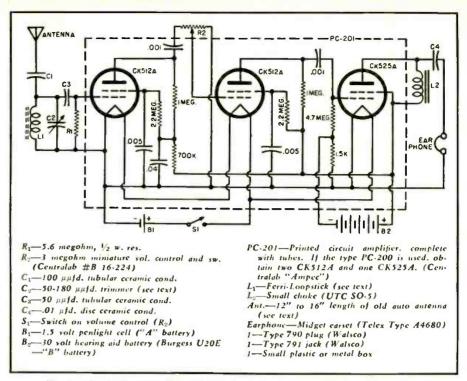


Fig. 2. Circuit diagram. The printed circuit is shown within the dotted lines.

or by cementing aluminum foil to the outside of the plastic case, connecting it to circuit "ground."

If over-all shielding proves necessary, care should be taken that no wiring connections are shorted, that the antenna is not shorted, and that the mounting screws of the "switch-volume control" are not shorted.

If the receiver is assembled in a metal case, slightly different construction techniques will be necessary in order to avoid shorts. One technique is to wire the entire receiver on a plastic "sub-chassis" which, in turn, is mounted in the metal case. A feed-through insulator should be used for mounting the antenna,

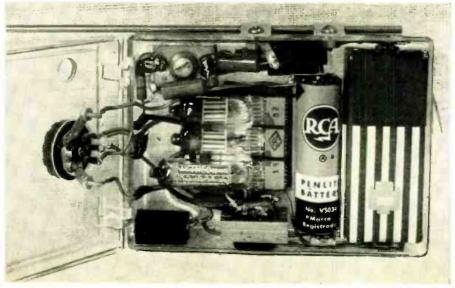
Another minor difficulty that may be encountered is an apparent lack of gain, in other words, insufficient "pickup." This will be noticed if the signal level of the local stations is low in the locality where the receiver is to be used—in another location, ample volume might be obtained.

While the over-all gain of this receiver is many times that of a simple detector, it must be remembered that the antenna length has been kept extremely short to increase portability. Because of this, the ability of the receiver to "pull-in" stations is not appreciably greater than a crystal receiver with a good outside antenna and earth ground.

If desired, a longer antenna may be used to increase signal pickup,

Touching the antenna with the hand or body will reduce signal pickup by "loading" the tuned circuit and reduc-(Continued on page 157)

Fig. 3. Close-up view—layout may be varied to conform to builder's requirements.



SINGLE-CHANNEL

REMOTE BROADCAST AMPLIFIER

By LEON A. WORTMAN

N THE operation of a 250-watt standard broadcast station there are the usual problems of equipment costs, maintenance, and operation. The cost of equipment for a 250 watter is the same as for a 50 kilowatter, per unit. However, because of lower rate cards and comparatively smaller, though not inadequate staffs, the methods of attacking these problems differ from those of higher powered stations serving larger areas and commercial listening audiences. One such station is KRUX in Phoenix, Arizona. KRUX operates as the "News, Music, and Sports Station" of this southwestern area, and as such finds itself with a heavy schedule of remote broadcasts. These range from church services, public service features, to the entire gamut of sports events, local and national.

Commercially-manufactured remote amplifier "boxes" are expensive; understandably so because of the design and development costs and the comparatively limited demand. An operation such as that at KRUX requires more than the usual number of remote amplifiers. Public service remotes tie up equipment and the engineer's time, and because of sequential remotes



Single-channel remote b.c. amplifier shown mounted under table at ball park. Power supply and amplifier are spaced at least $1\frac{1}{2}$ feet apart to reduce hum pickup.

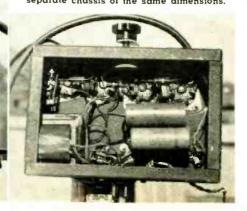
An inexpensive unit for the small station which can be built from spare parts and needs no tricky adjustments.

some economical solution had to be found. So, it was decided to "roll our own." Since there are undoubtedly other stations and engineers with the same problem, the following design, description, photographs, and general information are offered as an "assist."

The unit shown in the photographs was constructed to solve the problem of maintaining standard broadcast quality, when carrying the full schedule of the Phoenix Senators baseball games. This schedule includes approximately 125 broadcasts, exclusive of numerous commercial and public service remotes, during the months from March to September. That meant that about 500 engineer-hours would be required for setting up, riding gain, and tearing down the equipment during the season.

If it could be arranged so that the

Top and underchassis views of the amplifier. It is constructed on a standard 7" x 5" x 2" chassis. Spare parts were used throughout. The power supply is built on a separate chassis of the same dimensions.



equipment remained permanently installed at the ball park, the engineer's time could be cut and his services utilized for other duties. Since it was decided that one microphone was to be used for the broadcast, requiring no mixing, the engineer on duty at the main studio console could do all of the "gain riding" and "zero peaking" necessary for the full modulation of the transmitter. Thus engineering time could again be saved and utilized elsewhere. The final problem of equipment costs was eliminated by constructing a single-channel remote amplifier using existing station facilities.

The equipment had to be small enough to be mounted unobtrusively and without causing any additional crowding in the radio-press box. The amplifier and power supply, as seen in the photographs, are mounted on separate $7" \times 5" \times 2"$ chassis. Not one of the components is custom or specially built. All were and can be bought from the local supply houses or ham parts distributors. Many of the components are to be found in the spare parts cabinet, as were most of the ones used in this unit, of any standard broadcast station. Only two different types of tubes are used in order to keep the spare requirements at a minimum.

In the design and construction of any high-gain audio frequency amplifier several precautions must be taken. This type of amplifier is subject to the bugaboos of hum, distortion, and high-frequency thermal noises. A unique method for eliminating such high-frequency thermal agitation noises was the use of standard p.a. transformers instead of flat-response,

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high-fidelity units. In view of the fact that the remote amplifier is primarily intended for use by a sports announcer and not for the broadcast of music, the 5 kilocycle top of the output transformer used is more than adequate and in no way lends a false or unnatural quality to the voice. This is an economical and practical method of eliminating the noise. "bug."

Power supply ripple is eliminated through the use of heavy plate filtering. The power supply chassis uses an 8 µfd. and a 16 µfd. condenser. in addition to a filter choke for a.c. ripple minimization. The 6C5 input stage has an extra ripple filter and decoupling section provided by a 15.000 ohm, I watt resistor bypassed by an 8 #fd. electrolytic. The second singleended 6C5 has a 15.000 ohm, 1 watt resistor in series with the plate supply and bypassed by a .25 #fd. paper condenser to provide audio decoupling for this stage. A single plate to pushpull grids transformer is used here to provide the advantages of transformer coupling amplification. Again a standard p.a. transformer is used in preference to a flat-response, highfidelity transformer in the interest of economy and lower high frequency cut-off.

The input transformer can be any grade of microphone-to-single-grid transformer of the proper impedance to match the impedance of the mike to be used. Most broadcast stations use microphone impedances of 30. 50. 250, or 500 ohms. At KRUX, 250 ohm impedances are used throughout the installations. One precaution which must be taken is that the input transformer must be thoroughly shielded

against hum pickup.

To return to the hum problem: it was found impossible to mount the power transformer on the same chassis with the audio transformers without introducing a highly audible hum. In fact a minimum physical separation of 11/2 feet was found necessary between the power supply unit and the audio transformers. The power supply output of 6.3 volts a.c. and 250 volts filtered d.c. terminates at the back of the chassis with an Amphenol 4-prong tube socket. The power supply connections for the audio unit come out to a male chassis mount plug made by Amphenol to fit a 11/2 punched hole. A four-wire cable, with one male and one female Amphenol plug at either end and covered with heavy cambric "spaghetti" to provide protection, is used to interconnect the two chassis.

The gain control, normally an expensive component in broadcast audio equipment, is the well-known carbon type potentiometer used to control the volume in public address equipment and radio receivers. It costs only about 79 cents as opposed to attenuator pads costing about \$17. In view of the fact that it is not varied during the broadcast time and is in a high-impedance circuit, it is thoroughly adequate in this remote amplifier.

R₁, R₄—1000 ohm, I w. res.
R₂—100,000 ohm, I w. res.
R₃—250,000 ohm, I w. res.
R₄—250,000 ohm, I w. res.
R₅—15,000 ohm, I w. res.
R₆, R₇—15,000 ohm, I w. res.
C₁, C₄—10 µfd., 25 v. elec. cond.
C₃—8 µfd., 600 v. cond.
C₆—25 µfd., 600 v. cond.
C₆—25 µfd., 600 v. cond.

Circuit diagram of amplifier. A single tube type eliminates replacement problems.

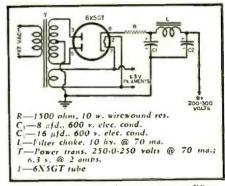
As in all broadcast equipment, precautions must be taken to eliminate the hazard of component breakdown. Loss of air time is inordinately expensive as it is the one commodity radio stations have to sell. Thus all condensers are oversized for working voltages and resistors are oversized for working wattages. The 1500 ohm, 10 watt resistor in series with the power supply high voltage acts as an additional voltage limiter and prodensers.

A single ground tie point is used in the wiring of both chassis. One exception was found necessary; some a.c. hum was being amplified and was traced to the filament wiring. It was found further that grounding one side of the filament terminals of the second audio stage at the chassis gave the greatest degree of hum elimination. Of course, shielding the filament wiring should eliminate this difficulty if included in the original wiring.

The grid connection from the microphone input transformer is only a few inches long and runs close to the chassis. Some hum pickup was experienced through this short lead. However, shielding it immediately eliminated all trace of hum from this source.

The earphone monitor is connected directly across the radio line in scries with two 1500-ohm resistors. The resistors effectively isolate the monitor circuit from the radio line to the studio in case of a short circuit in the earphone plug and cord. The audio output is brought directly out from the rear of the chassis and is connected to the terminal block of the radio line supplied by the local telephone company. This connection need never be disturbed.

The amplifier has more than sufficient gain to cover the radio line from the Phoenix Municipal Stadium to the main studios, some 12 miles distant, without the use of telephone repeater amplifiers, and without any audible line noise under the program level. The cambric-covered power cord is rigidly mounted under the table with cable

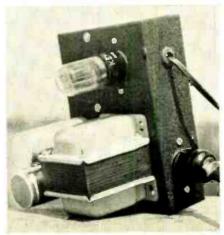


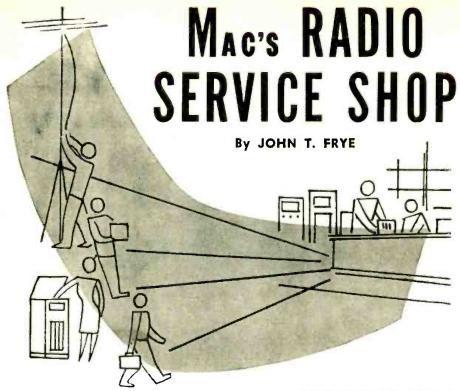
Power supply for the remote amplifier.

clamps. The microphone cord and earphone monitor cords and plugs are also secured to the bottom of the table and in such a position that the announcer-operator can easily make his own connections. Of course, the units are bolted to the bottom side of the table directly in front of the announcer.

The sportscaster takes a microphone and a pair of earphones with him when he goes to the ball park. All he has to do on arrival is plug in his mike and phones, then insert the a.c. plug in the outlet mounted next to the (Continued on page 154)

Over-all view of the power supply chassis. It is connected to the amplifier chassis by means of a shielded four-wire cable.





SERVICING WITH THE GDO

RDINARILY Barney was not eager to get to work, but on this particular morning he was glad to step out of the howling February snowstorm into the warm sanctuary of the service shop.

"Whew!" he exclaimed as he beat the snow from his sock cap and wiped the water from his freckled face. "'Tain't fit for man nor beast out there today; and I keep remembering that last fall, when old Indian Summer hung on and on, I was the one who told everyone we weren't going to have any winter weather this year. Hey, Mac, what's the gadget you've got there? Something new?"

"Yes," his boss answered as he fondly cradled the little gray, cracklefinished instrument in the palm of his hand. "Let me introduce you: Barney, this is Mister Grid Dip Oscillator, familiarly known as GDO; Mister GDO, this is Barney, familiarly known as Red, Sorrel Top, or Scarlet O'Gallagher. I want the two of you to become better acquainted."

"How do you do?" Barney inquired politely of the instrument. "I've heard a lot about you on the ham bands."

And from here on in, unless I miss my guess, you're going to hear a lot about him from technicians," Mac stated. "I'm confident the GDO is about to join the parade of instruments from the laboratory to the service bench that began with the cathoderay oscilloscope and the vacuum tube voltmeter. Engineers and amateurs have long known how useful this rather simple little instrument is; but it was not until the last few months, when several manufacturers brought out grid dip oscillators in both kit and assembled forms at down-to-earth prices, that technicians felt they could afford to buy one of the units just to see what could be done with it in service work. Now that they have found out, the things are selling like

bottle-openers at a bartenders' picnic," "How does it work?"

"Here's a diagram (Fig. 1) of this particular instrument, the Heathkit Model GD-1," Mac said as he slid a paper across the bench. "You can see that it is essentially a high-frequency triode connected as a Colpitts oscillator with plug-in inductances, A 500 microampere meter is connected in the grid return circuit and reads rectified grid current. There is also provision for plugging earphones into this gridreturn lead.

"Now watch what happens when I bring the inductance of the GDO close to this coil-and-condenser circuit and tune the grid dip oscillator through the resonant frequency of the combination. See that meter pointer dip downward as I pass through reso-

"How come?" Barney demanded.

"The tuned circuit at its resonant frequency absorbs energy from the oscillator and lowers the amplitude of the oscillation, which, in turn, makes the rectified grid current go down. All I have to do is note on this calibrated dial of the tuning condenser of the GDO the frequency at which this dip occurs, and I know the resonant frequency of that tuned circuit."

What does the variable resistor,

R. do in the circuit?"
"That's a sensitivity control. You can see that the negative rectified grid voltage appears at the bottom of this resistor and a positive potential fed through R_2 appears at the top. The resultant of these two opposing voltages causes a current to flow through the meter to ground. If the slider is clear to the top, the positive voltage is grounded and only the grid current registers on the meter. As the slider is moved down, more and more positive voltage is allowed to buck this developed grid voltage."

'But why?"

"The object is to keep the 500 microampere meter on scale for various values of grid current. Different coils and different settings of the tuning condenser will produce different values of grid current. A meter to read this wide range of current without going off scale would have to be one with a relatively high current range; and that would mean a small, hard-to-detect dip with the loose coupling to a tuned circuit required for best accuracy. By using a variable positive bucking voltage, the pointer can be kept on scale for all values of grid current, yet the greater dip-indicating sensitivity of the 500 microampere movement can be retained."

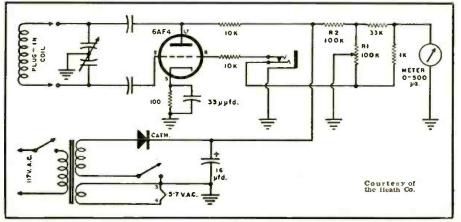
"Is that all it will do: indicate the resonant frequency of tuned circuits?"

"By no means. Watch the screen of the TV set over there on the other bench."

As he said this, Mae plugged another inductance that looked like a fat, king-sized hairpin into the GDO and moved the tuning dial with his thumb. Suddenly the picture was re-

(Continued on page 111)

Fig. 1. Circuit diagram of a commercially-available grid dip oscillator kit.





Compiled by KENNETH R. BOORD

T IS A privilege this month to dedicate the ISW DEPARTMENT to radio broadcasting in the Republic of Korea. Thanks goes to Hahn Ki Syun, chief of the engineering section, Radio Korea, Office of Public Information, Pusan, Republic of Korea, for this data:

"Due to the war, we have lost almost all of our broadcasting equipment, but our engineers have been trying to rebuild our facilities one by one. We have constructed a 10 kw. broadcasting (medium-wave) at Taegu, a part of our Rudio Korea Network, and a similar station was completed at Taejon in November. We expect to build up the 1 kw. short-wave station at Seoul and the 400 w. shortwave station at Taejon within a few weeks. And within a few weeks more, short-wave listeners should be able to listen to our 'Voice of Freedom' on a 10 kw. short-wave outlet from Seoul; a further 10 kw. medium-wave station will follow at Seoul. We have had much difficulty through shortages of equipment, materials, and even engineering books."

Mr. Hahn gives this picture of current broadcasting in Korea:

Seoul, HLKA, 970 kc., 5 kw., and 9.555, 300 w. Pusan, HLKA, 800 kc., 5 kw.; 2.510, 1 kw., and 7.935, 1 kw.; former HLKB, 650 kc., 500 w., is now a 1 kw. "spare" medium-wave outlet. Iri, HLKF, 570 kc., 500 w.; Taegu, HLKG, 710 kc., 10 kw.; Kwangju, HLKH, 780 kc., 500 w.; Taejon, HLKI, 880 kc., 10 kw.; Namwon, HLKL, 1030 kc., 500 w.; Chunchon, HLKM, 1230 kc., 300 w.; Mokpo, HLKN, 650 kc., 500 w.; Masan, HLKO, 600 kc., 50 w.; Chungju, HLKQ, 600 kc., 500 w.; Kangneung, HLKR, 1080 kc., 500 w., and Cheju, HLKS, 1080 kc., 500 w. These stations make up the Radio Korea Network which is currently scheduled 1600-1830, 2130-0030, 0500-0900, Various Asiatic languages are used, and at least the short-wave outlets occasionally identify in English. By the time you read this, the new short-wave outlet at Taejon and the further shortwave outlet at Seoul (10 kw.) may be on the air.

Best wishes go to the Radio Korea Network and its personnel in the further resumption of radio broadcasting in the Republic of Korea.

Club Notes

England — The World Friendship Society of Radio Amateurs, 35, Bell-

wood Road, Waverley Park, Peckham Rye, London, S.E. 15, England, now has a *new* bulletin especially for its Junior Section members; it is called "Wave-Guide" and is edited by D. F. Shaw and J. I. Meardon.

New Zealand—The New Zealand Radio DX League has named Frank W. Wilson as president to succeed Arthur T. Cushen who had headed the group for the past two years.

USA—The Newark News Radio Club, Newark, New Jersey, recently passed its 25th milestone. And the Universal Radio DX Club, located at Hayward, California, recently observed its 19th anniversary. Congratulations to both!

This Month's Schedules

Albania—Radio Tirana is reported now using 6.560, 7.850A at 2300-0100, 1000-1130, 1215-1700. Chatfield, N. Y. notes the 7.850A channel at fair level 1500-1600. Levy, N. Y., notes it with news 2345.

Algeria—Radio Algeria, 6.160, noted signing off Arabic session with "La Marseillaise" 1745; had news headlines in Arabic just before closing; the 9.570 outlet, used for French sessions,

(Note: Unless otherwise indicated, all time is expressed in American EST; add 5 hours for GCT. "News" refers to newscasts in the English language. In order to avoid confusion, the 24 hour clock has been used in designating the times of broadcasts. The hours from midnight until noon are shown as 0000 to 1200 while from 1 p.m. to midnight are shown as 1300 to 2400.) The symbol "V" following a listed frequency indicates "varying." The station may operate either above or below the frequency given. "A" means frequency is approximate.

The antenna for the 10 kw. transmitter at Taegu, a "Radio Korea" network affiliate.



noted closing 1800 with "La Marseillaise," after news in French 1751. (Pearce, England)

Anglo-Egyptian Sudan—Radio Omdurman, 9.737A, is occasionally audible to fair in its 2315-2345 all-Arabic session. (Niblack, Ind., others)

Angola — Radio Clube de Angola, 11.862A, Luanda, has been fading in lately as early as 1340. (Niblack, Ind.) Radio Clube de Huila, 10.048A, Sa da Bandeira, more recently has been running to 1600 closedown (formerly closed 1500). (Pearce, England; Ridgeway, South Africa) Radio Diamang, CR6RG, Dundo, recently moved from 6.870, is now using 7.065 parallel with 9.344 at 1300-1430 daily; CR6RD, Nova Lisboa, has been heard on Saturday opening 0930, Sundays and weekdays 1230, using 9.705, 9.7096 to 1530 closedown. (Ridgeway, South Africa)

down. (Ridgeway, South Africa)

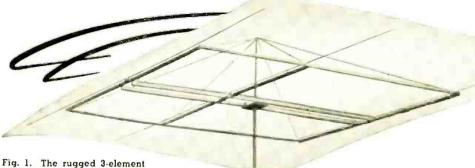
Argentina—LRX, 9.66, Buenos Aires,
Radio El Mundo, noted at strong level
around 2045. (Stein, Calif.) SIRA announces English for 17.720 at 17001930; 11.880 at 1300-1400; 15.290 at
2300-0100. (Villela, Md.) Radio Belgrano, 9.755A, has hourly national and
world news in Spanish at 55 minutes
past the hour, according to Villela; at
1825 ("las 20:25, hora que Eva Peron
entro en la eternidad"—"at 2025, the
hour that Eva Peron entered Eternity") has a 5-minute official news
bulletin in Spanish.

Belgium—ORU, 17.865A, Brussels, noted in French and Dutch 0500. (Pearce, England) The 6.065 outlet noted with dance music 2240, signing off North American transmission 2400. (Lieberman, N. Y.) English for North America is currently carried over ORU, 6.065, beamed to North America, and 9.745 beamed to Belgian Congo, and relayed by OTC, 9.655, Leopoldville, at 2100-2400. Kelting, N.Y., notes ORU, 9.745, with French program 2045-2130, then English.

Belgian Congo—OTM1, 6.295. appears to have replaced 11.720A, audible around 1500 parallel with OTM2, 9.380, in the Radio Congo Belge transmission to 1600 closedown. (Kary, Pa.) OTH, 9.210. is heard in Sweden 1245-1330. (Nattugglan, Sweden) Radio Elizabethville, OQ2AB. 11.90, has been noted recently on Tue. as well as Sun. with the 0930-1100 session. Radio Leo, OQ2AA, 11.717. on Sun. only has a session 0300-0430 which is all-French; OTM4, 11.72A, now opens 0300 with French and Flemish programs to 0730

(Continued on page 127)

3-ELEMENT 14mc. ROTARY BEAM ANTENNA



By C. A. WEST, W2IYG
Tube Department, RCA
Harrison, N. J.

High front-to-back ratio, good forward gain, and a beam that stays up in the wind are the result of careful design. Simplified construction and adjustment are also featured.

NE sure aid in working DX is the use of a rotary-beam antenna. This article describes the construction of a 3-element, 14-megacycle rotary beam which was built by the author. The antenna, which has been in use for more than three and a half years, remains in excellent condition in spite of several of the worst wind and ice storms ever experienced in New Jersey.

beam after 31/2 years aloft.

There can be very little doubt that sound mechanical planning is of the utmost importance when the construction of an array of this sort is contemplated. Some of the questions which should be answered before actual planning gets under way are:

Is the cost within reason?
Is the array simple to construct?
Can it be assembled easily at its final location?

Is maintenance relatively light? Will it stay up?

For the beam antenna described in this article, the answer to all of these questions is "yes." The entire cost of the array was about \$75.00. No special tools were required for the construction: anyone familiar with saw, hammer, screwdrivers, and pliers could do the job. The final assembly of the beam on a rooftop was completed by three people in about one and a half hours. The only maintenance required so far was the replacement of the guy wires, a two-hour, one-man job which would have been unnecessary if rustproof cable had been used initially, Fig. 1 is a photograph of the antenna taken more than three and a half years after its construction.

Preliminary Considerations

It was decided to mount the beam on the roof of the house to avoid the added work and expense of constructing a tower. Mounting the antenna on the roof also provides for the housing of the motor, gear box, direction-indicating equipment, slip rings, transformer and relay, and associated wiring in the attic, thus providing for their protection against the elements and making maintenance work much easier.

Roof mounting also solves the problem of mounting the parasitic array itself. When a tower or pole is used to support the array, it is usually necessary to assemble the array before it is finally placed atop the tower or the pole. Needless to say, a 3-element, 14megacycle array, 34 feet long and 17 feet wide, is a rather cumbersome assembly to raise to the top of any tower or pole. Roof mounting, however, provides for assembly at the final location.

Another advantage of mounting the

Fig. 2. A pipe shaft runs up through the roof inside a larger pipe bushing, steadied by pipe straps. At the top are two 2 x 6 roof supports. Note the BX cables.



beam on the roof is that provision is made for short feedlines and other wires and cables for carrying power to the rotator, and to the electric-indicating system, if one is used.

Whether the antenna is to be supported by a roof, a tower, or a pole, many of the ideas presented in this article should prove quite useful. It is recommended that a lot of thought be put into the planning of the beam. Many arrays have been completely destroyed by wind and sleet storms due to poor mechanical construction.

Main Supports

It was estimated that the entire array plus the rotator (propeller-pitch type) would weigh about 150 to 200 pounds. The supports in the attic would have to hold this weight safely and would also have to have enough strength to provide for bending and twisting torque created by the wind striking the array. For this reason, two pieces of 2" x 8" lumber were used to support the platform on which the shaft of the array and the rotator were mounted, as shown in Fig. 2. These 2" x 8" pieces were bolted securely to two of the 2" x 8" rafters in such position that about two-thirds of the shaft supporting the array was below the roof top. It is important that this length of the array be below the roof to provide for bending torque on the shaft, and to reduce the hazard of damage to the roof if strong winds strike the array broadside. Two 2" x 4" pieces of lumber were also bolted to the main supports as shown in Fig. 2 to provide for torque at right angles to the main supports and to give added strength.

After the main supports had been bolted into place, the rotator platform was prepared. Two pieces of 2" x 12" lumber were cut to the width of the main supports, allowing a little overhang for later centering of the shaft of the array on the rotator flange. A hole large enough to pass the array shaft was cut in the center of the joined 2" x 12" pieces and, with the rotator mounting plate used as a template, holes were drilled for fixing

the rotator in place. The mounting plate is used on top of the wood rotator platform for added strength.

At this point, consideration was given to the shaft and its bushing. A 2-inch pipe was used for the bushing and a 1½-inch pipe for the shaft. The two slipped together very easily with a fraction of an inch play, but there was no problem with rattling. When the 2-inch pipe used for the bushing was cut with a pipe cutter, a small edge protruded at the inner circumference; this edge was filed until the 1½-inch pipe shaft fit snugly into the bushing.

It is preferable to install the shaft bushing before the initial assembly of the array. When the proper point was located on the roof, a hole was made in the roof to hold the hushing, as shown in Fig. 4. The roof peak was re-inforced by means of two pieces of 2" x 6" lumber, and a plumb line was dropped through the bushing so that the bushing could be brought into a vertical position. The steel straps were then fastened in place, as shown in Figs. 2 and 4. The bushing must be sealed at the point where it comes through the roof to prevent rain coming into the attic.

Rotator Preparation

There are several difficulties involved if the rotator (propeller-pitch type) is used "as is." chief of which is slow rotation speed. Another difficulty is the burning of brushes and commutator when a.c. is used to energize the d.c. motor. In addition, a considerable amount of electrical noise is generated, which wreaks havoc in the receiver when the array is rotated to peak a signal.

All these difficulties can be avoided by making the last set of planetary gears inoperative. These gears may be disabled quite simply by removing the upper spline from the gear box assembly and fastening the shaft pipe flange right on top of the planetary gear housing, as shown in Fig. 4. This operation makes possible a much greater shaft rotation speed for a given voltage applied to the rotator motor. Before the spline was removed, about 25 volts a.c. was required to obtain a shaft rotation of 1 rpm. With the spline removed, only about 15 volts a.c. was required for one rpm. Two other improvements are also obtained: (1) electrical noise is cut to a much lower value; (2) burning of the brushes and commutator is prevented and heating of the motor is reduced.

While the rotator is being modified, it is a good idea to remove the motor from the gear box and disassemble it for inspection. If the commutator has a ridge burned in it, the armature should be removed and the commutator turned down. The insulating surfaces between the commutator faces should be cleaned with a sharp pointed tool to remove any small metal particles which accumulate during the commutator turn-down. The entire motor may be cleaned in kerosene with the

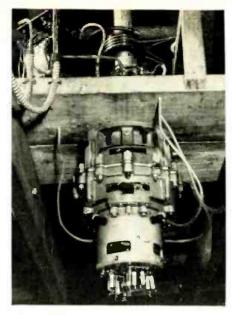


Fig. 3. The motor and gear box are mounted below the platform. The motor housing is removed to show the bypass condensers for the brushes. At top, brass rod brushes bear against slip rings on the shaft.

aid of a brush, then wiped dry and re-assembled.

Electrical noise generated by brush sparking may be reduced by connecting a 0.01 µfd. condenser between each brush lead and the case of the motor, as shown in Fig. 3. The reduction in noise on 20 meters is sufficient to allow rotation of the array without drowning out weak signals, even when there is no noise limiter on the receiver.

Array Design

There are two general classifications of array construction, self-supporting and frame with guy-wire supports. The author discarded the self-supporting type almost immediately because of the lack of strength exhibited by several of these beams in his neighborhood. The design shown in Fig. 5 was chosen for several reasons: 1. economy and availability of

GUY SUPPORT PIPE 2 x 4 BOOM TO PADIATOR 2 X 12 ARRA FLANGES 721 COAX LINE INSULATOR (CEMENT IN PLACE) 2X6 ROOF RUBBER HOSE SLIP RINGS PULLEY BELT ROTATOR TEMPLATE ROTATOR FLANGE (SEE TEXT) GEAR BOX MOTOR

Fig. 4. Detail drawings of the rotator and beam support. One of the two slip ring and brush assemblies is shown at upper left.

materials, 2. strength, 3. ease of construction and assembly, 4. ease of tuning.

Basically, a parasitic array requires at least two elements, a radiator and either a reflector or a director. If greater gain or front-to-back ratio is desired, additional directors and reflectors may be added. The 3-element array was chosen to provide maximum front-to-back ratio. Although a 3-element array may be tuned for either maximum forward gain or maximum front-to-back ratio, the latter was chosen for two reasons: (1) it was

Fig. 5. Construction details of the beam and tuning stubs. The guy wires are broken into non-resonant lengths by the insulators. Aluminum should be used for the tuning stubs, if possible, as copper-to-aluminum contacts may corrode. The wooden braces keep elements from whipping in the wind, changing beam characteristics.

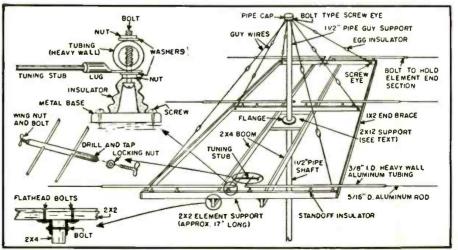




Fig. 6. The "on-off" switch, fuse, and pilot lamp are mounted at the beam-indicator map. The control switch is at the operator's desk. A selsyn drives the arrow.

highly desirable to be able to reduce to a minimum the strength of all signals not coming from the direction of the desired signal; (2) the comparative difference in forward gain between the two systems of tuning is negligible.

When maximum front-to-back ratio is desired, the satisfaction gained by tuning a parasitic array is well worth the small amount of additional effort involved. There are two popular methods of tuning the director and reflector. One is to lengthen or shorten the outer ends of the elements, and the other is to lengthen or shorten the center section of the elements by means of adjustable stubs.

The latter method was chosen for two reasons: (1) the r.f. potential at the center of each element is close to zero, thus preventing r.f. burns when the energized array is being adjusted; (2) correct adjustment is assured because element symmetry is maintained by one adjustment which can be made from a single position on the roof. If the first method of adjustment were used, it would be necessary to move back and forth from the end of each element continually, making an adjustment, testing, and repeating the procedure until the correct element length was obtained. With the second method, it is necessary only to slide the shorting bar back and forth until tuning is correct and then lock the bar in place. The method of making this adjustment will be described later.

Copper-to-aluminum contacts should be avoided in the stubs because they may cause galvanic action, with resultant deterioration of the aluminum. Small copper parts such as lugs, washers, etc., should be carefully tinned, and the final joints covered with a good varnish. It would be a good idea to varnish all the elements when the beam is completed.

Because the author was interested

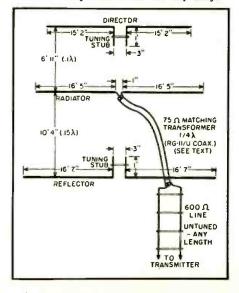
primarily in best performance in the phone section of the 20-meter band, the design frequency chosen was 14.25 megacycles, the center of the American phone band. The length in feet of the radiator, director, and reflector were determined from the following relations, in which the decrease of 4 per-cent in director length and the increase of 5 per-cent in reflector length, as compared with the length of the radiator, were taken into consideration:

Length (radiator)
$$= \frac{468}{f(mc.)} = \frac{468}{14.25} = 32' 11''$$
Length (director)
$$= \frac{450}{f(mc.)} = \frac{450}{14.25} = 31' 7''$$
Length (reflector)
$$= \frac{492}{f(mc.)} = \frac{492}{14.25} = 34' 6''$$

The length of the two tuning stubs and the shorting bar must be taken into consideration, as shown in Fig. 7. For example, the length of each half of the director is 15 feet, 2 inches; thus, the length of the whole director is 30 feet, 4 inches. The length of each tuning stub is 12 inches, but the shorting bar is set initially at 6 inches; thus, the total effective length of the stubs is 1 foot. The shorting bar itself is 3 inches. Therefore, the total length of the director is 31 feet, 7 inches, the desired calculated length. Because the director should be about 4 per-cent shorter in length than the radiator, as mentioned previously, the 12-inch stubs allow for a variation of from 1 per-cent to 7 per-cent, with the mean at about 4 per-cent.

Tests have shown that maximum gain is obtained with a director-radiator spacing of 0.1 wavelength and a reflector-radiator spacing of 0.15 wavelength. The following equations may be used to determine the length in feet between the director and the ra-

Fig. 7. Dimensions of the beam proper. The elements are aluminum tubing. The radiator is fed through a 1/4-wave coaxial matching transformer via slip rings.



diator, L_d , and the length between the reflector and the radiator, L_r .

$$L_{d} = \frac{0.1K}{f} = \frac{98.4}{14.25} = 6' \, 11''$$

$$L_{r} = \frac{0.15K}{f} = \frac{147.5}{14.25} = 10' \, 4''$$

where: K = one wavelength = 984 feet. f = frequency in megacycles.

The construction of the array, as shown in Fig. 5, is relatively simple. Because the entire array is supported by six guy wires, pieces of 2" x 4" lumber were used for the boom. The length of the boom is determined by the distance between the director and the reflector. Three pieces of 2" x 2" lumber used to support the elements were bolted to the boom by means of 90-degree angles. After the entire array had been assembled on the ground to determine the "center-of-gravity" point, a piece of 2" x 12" lumber the width of the boom was fastened to the boom at this point. The use of these pieces prevents bending torque on the shaft and balances the entire array on the shaft.

One advantage of the frame construction is that elements of small diameter may be used. About half of the length of each element is supported by the 2" x 2" pieces of lumber, which are approximately 17 feet long. The array shown in Fig. 5 used two 12-foot lengths of heavy-wall aluminum tubing having an inside diameter of %-inch, with a length of solid aluminum rod having a 5/16-inch diameter inserted into the tubing at the outer end to provide the proper length. Two pieces of 1" x 2" lumber were screwed to the ends of the element supports, as shown in Fig. 5, to prevent the element supports from whipping in the wind and thus changing the spacing between elements.

The main strength of the entire array lies in the six guy wires and their arrangement. A molded steel pipe flange was used to support a five-foot length of 11/2 inch pipe, the top of which is used as the focal point for the six guy wires. Two egg insulators break each guy wire into three equal sections and prevent any resonant effect from the guy wires. Rustproof wire or cable should be used for the guy wires to prevent rusting and snapping. If steel wires are used, they should be coated with some rustinhibiting material, such as aluminum paint. The use of rustproof and rustinhibiting materials throughout the array will save considerable maintenance time and effort later on. Wooden members should be undercoated and painted with good enamel, with a top coat of spar varnish.

Feeding the Array

There are several methods for feeding a parasitic array, such as the "T" match, delta match, and quarter-wave transformer match. The quarter-wave transformer match was chosen for reasons of cost, simplicity, and ease of adjustment. (Continued on page 142)

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RCA INSTITUTES, INC., Home Study Dept. RN253 350 West Fourth Street, New York 14, N.Y.

Without obligation on my part, please send me copy of booklet "RCA INSTITUTES Home Study Course in Television Servicing." (No salesman will call.)

Name		
1141110	(please print)	
Address		_
City	Zone State	

Thousands depend on **PHOTOFACT!**THEY TELL YOU WHY

Unsolicited letters tell what the world's finest TV and Radio Data means to Service Technicians



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Learn for yourself—at our expense—how PHOTO-FACT pays for itself by earning bigger repair profifs for you! Select any Folder from the PF Index (if you haven't an index, get a copy from your distributor). When you write us for your Free Folder, be sure to state Photofact Set and Folder Number as shown in the Index. Get your Free Folder now. Examine, use, compare—see why you can't afford to be without PHOTOFACT!

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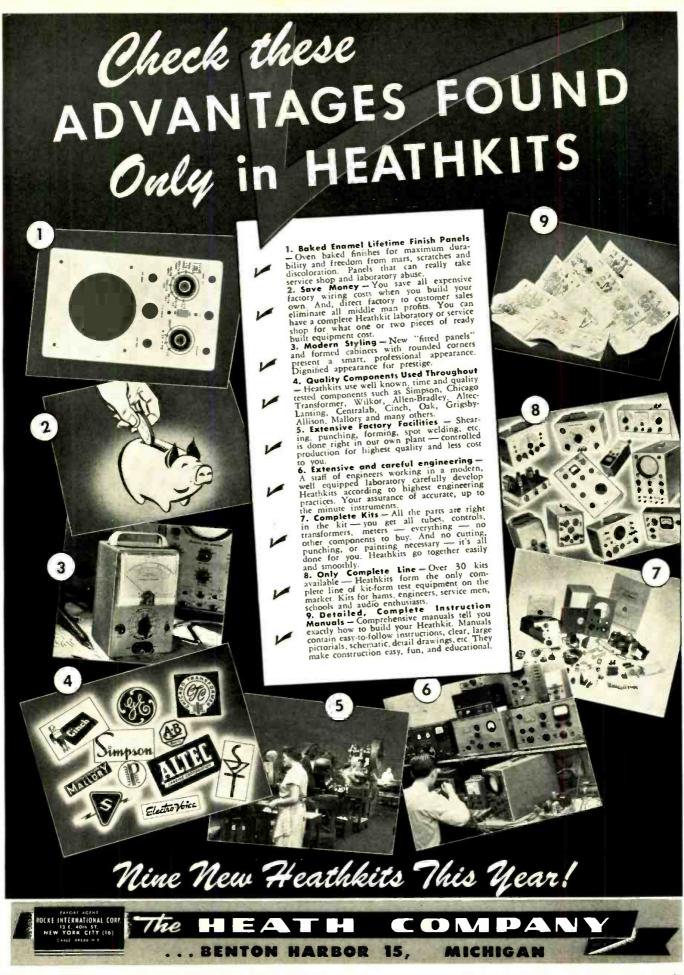
NEW TV GRANTS SINCE FREEZE LIFT

Partial listing of construction permits granted by the FCC since lifting of freeze. Additional stations will be listed next month.

litting of fre	stations will	be listed next month.			
STATE	CITY	CALL**	CHANNEL	FREQUENCY (mc.)	POWER (Video)*
Alabama	Gadsden	WTVS	21	512-518	22
n. n	Mobile	WALA	10	192-198	316
11	Mobile	WKAB-TV WCOV-TV	48	674-680	22.5
Ārizona	Montgomery Tucson	KVOA-TV	20 4	506-512 66-72	88 11
Arizona	Tucson	KOPO-TV	13	210-216	316
Ārkansas	Fort Smith	KFSA-TV	22	518-524	265
M	Little Rock	KETV	23	524-530	17.5
a	Little Rock	KRTV	17	488-494	22
California "	Santa Barbara	KEYT KITO-TV	3 18	60-66 494-500	50 87
u	San Bernardino Fresno	KMJ-TV	24	530-536	105
Colorado	Colorado Springs		13	210-216	11.5
II .	Denver	KIRV	20	506-512	89
n n	Denver	KFEL-TV	2	54-60	56
u.	Denver	KBTV	9	186-192	240
n.	Denver Pueblo	KDEN KCSJ-TV	26 5	542-548 76-82	105 12
n.	Pueblo	KDZA-TV	3	60-66	10.5
Connecticut	Bridgeport	WSJL	49	680-686	99
	Bridgeport	WICC-TV	43	644-650	81
0	New Britain	WKNB-TV	30	566-572	180
	Waterbury Ft. Lauderdale	WATR-TV WITV	53 17	704-710	245
Florida	Ft. Lauderdale	WFTL-TV	23	488-494 524-530	18.8 100
g .	Pensacola	W1 1 1 1 4	15	476-482	20
PI .	St. Petersburg	WSUN-TV	38	614-620	83
Illinois	Belleville	WTVI	54	710-716	115
11	Decatur	WTVP	17	488-494	18 175
n	Peoria Rockford	WEEK-TV WTVO	43 39	644-650 620-626	15.5
Indiana	Muncie	WLBC-TV	49	680-686	16.5
III III	South Bend	WSBT-TV	34	590-596	170
Iowa	Sioux City	KVTV	9	186-192	29
77	Sioux City	KWTV	36	602-608	18.5
Kentucky	Ashland Henderson	WPTV WEHT	59 50	740-746 686-692	250 26
11	Louisville	WKLO-TV	21	512-518	200
Louisiana	Baton Rouge	WAFB-TV	28	554-560	225
Maryland	Frederick	WFMD-TV	62	758-764	105
Massachusetts	Fall River	WSEE-TV	46 55	662-668 716-722	19.5 65
II .	Holyoke New Bedford	WHYN-TV WNBH-TV	28	554-560	200
11	Springfield	WWLP	61	752-758	115
Michigan	Ann Arbor	WPAG-TV	20	506-512	1.75
U	Battle Creek	WBCK-TV	58	734-740	18.5
n	Battle Creek Flint	WBKZ-TV WCTV	64 28	770-776 554-560	24.5 17.5
n	Flint	WTAC-TV	16	482-488	59
n	Jackson	WIBM-TV	48	674-680	225
и	Kalamazoo	WKMI-TV	36	602-608	83
11	Saginaw	WKNX-TV	57	728-734	17.5
Minnesota Mississippi	Duluth Jackson	WFTV WJTV	38 25	614-620 536-542	17 180
Missouri	St. Joseph	KFEQ-TV	2	54-60	52
11	Springfield	KTTS-TV	10	192-198	12.5
Nebraska	Lincoln	KOLN-TV	12	204-210	21.5
NT T	Lincoln	KFOR-TV	10	192-198	56
New Jersey	Asbury Park Atlantic City	WCEE WFPG-TV	58 46	734-740 662-668	100 18
New York	Elmira	WTVE	24	530-536	58
11	Poughkeepsie	WEOK-TV	21	512-518	105
North Carolina	Asheville	WISE-TV	62	758-764	23
U	Greensboro	WCOG-TV	57 28	728-734	115 280
Ohio	Raleigh Akron	WETV WAKR-TV	49	554-560 680-686	145
11.	Dayton	WONE-TV	22	518-524	210
	Lima	WLOK-TV	73	824-830	20
u u	Massillon	WMAC	23	524-530	99
N	Youngstown	WUTV WHHH-TV	21 67	512-518 788-794	1 70 80
II .	Warren Youngstown	WFMJ-TV	73	824-830	175
U	Youngstown	WKBN-TV	27	548-554	200
Oregon	Portland	KPTV	27	548-554	91

*ERP = (effective radiated power). **Call letters without TV suffix from application files and subject to change; except where included in calls such as KBTV.

.. = Call letters to be announced.



NEW Heathkit "Q" METER KIT

A HIGH QUALITY Q METER AT LOW COST.

Measures Q and in-ductance of coils.

Measures Q and capacity of capacitors.



Slant face cobinet for ease in reading the





MODEL QM-1

• First Q METER within the price range of all.

● Read Q's of 0 - 500 directly on calibrated scale.

 Stable oscillator supplies R.F. frequencies of 150 kc to 18 megacycles.

 Calibrated capacitor with range of 40 mmf to 450 mmf with vernier of ±3 mmf.

Simple, easy operation.

 Can be used to measure small inductances ar capaci-

• Measures Q of condensers, RF resistance and distributed capacity of coils.

• Measures capacity by substitution, capacity by resonance, inductance by resonance.

 Slanted panel for convenient operation.

Another outstanding example of progressive HEATH-KIT engineering. Now a highly desirable Q METER within the price range of all laboratories, schools and experimenters. No longer is it necessary to deny your-

self the many measurement advantages offered by this instrument.

Use the new HEATHKIT Q METER for the following simple basic measurements: capacity by substitution, capacity by resonance, inductance by resonance and Q at the OPERATING frequency all can be read on the calibrated scales. The method used to obtain information regarding the Q of condensers, RF resistance, distributed capacity in coils, etc., is only slightly more involved. In the HEATHKIT Q METER, the generated RF signal is coupled through a cathode follower and injected across a low impedance condenser which is included in the resonant circuit under test. Large 4½" 50 microampere Simpson meter reads Q directly. The resonating condenser and vernier condenser are calibrated in mmf for substitution method capacity tests. The resonating condenser is also calibrated in effective capacity for resonance tests. The inductance calibration serves for rapid determination of the approximate inductance of a coil. The HEATHKIT Q METER has a generator frequency range of 150 kc to 18 megacycles. Vernier capacity covers ± 3 mmf and the resonating condenser is calibrated from 40 mmf to 450 mmf actual capacity or 40 mmf to 350 mmf effective capacity. Meter reads Q directly up to

250. Higher and lower full scale readings can be obtained by varying the injection voltage levels. The entire kit consists of 12AT7, 6AL5, 6C4, OD3 and 6X5 tubes, 50 microampere Simpson meter, power transformer, cabinet and all other parts necessary for construction as well as instructions for assembling, testing and operation of the completed instrument.

Heathkit DECADE RESISTANCE KIT

The HEATHKIT DECADE RESISTANCE KIT is widely used by schools, experimenters and laboratories because of the extremely wide resist-ance range offered and the useful, dependable service provided. The DECADE con-sists of 5 rotary 2 deck ce-

ramic wafer switches with silver plated contacts and twenty 1% precision resistors in a circuit which provides the resistance range of 1 ohm to 99,999 ohms in 1 ohm steps. The HEATHKIT DECADE RESISTANCE KIT is simple to construct and is housed in a beautiful polished birch cabinet with an attractive panel. The DECADE will furnish years of accurate trouble-free service.

Individual decade sections of above can be purchased separately for special



NEW Heathkit DECADE CONDENSER KIT

Extremely useful in all experimental and design work such as determination of condenser values for: compensating networks, filters, bridge impedances, tuned circuits, etc. Uses all precision silver mica condensers within ±1% accuracy. Values

run in three decades from 100 MMFD to 0.111 MFD in steps of 100 MMFD. Smooth acting, positive detent, highest quality ceramic wafer switches make all capacitor values easy to set up and keep losses to a minimum. Low loss dielectric terminal board mounts on outside of panel for easy cleaning. Heathkit binding posts accommodate a wide variety of test leads. Comes complete with all parts, including polished birch cabinet.

Individual decade sections of above can be purchased separately.



MODEL DC-1 SHIPPING WT. 4 LBS.

OCKE INTERNATIONAL CORP. 13 E. 40th ST. NEW YORK CITY (16)

BENTON HARBOR 15. MICHIGAN



W Heathkit OSCILLOSCOPE KIT

ullet NEW WIDE BAND VERTICAL AMPLIFIER \pm 2 DB 10 CYCLES TO 1 MC.



Direct plate conulation tests

Displays TV correctly.

Good square wave response at 100 kc.

MODEL 0-8

WT. 29 LBS.



• New wider band vertical amplifier ± 2 db from 10 cycles I megacycle useful to over megacycles.

High sensitivity in vertical amplifier. .025 volts RMS per inch deflection.

New 3 step input attenuator input ranges X1, X10, X100.

New SCP1 intensifier type tube for greater brilliance.

• Terminal board and rear cabinet opening provisions for direct connections to deflecting plates.

Newly styled formed and ventilated aluminum cabinet.

Wide band sweep generator, 15 cycles to over 100 kc. Will synchronize with 5 megacycle signal.

• 10 tube circuit featuring push pull operation of vertical and horizantal amplifiers.

 Internal synchronization on either positive or negative neaks.

 Reproduces faithfully the front and back porches of TV sync pulses. Excellent square wave reproduction to over 100 kc.

• Optional Intensifier kit available for 2200 volt aper-

Proudly announcing the new 1953 HEATHKIT Model O-8 OSCILLOSCOPE featuring the finest performance ever offered in this extremely popular kit instrument. Improved wider band vertical amplifier featuring a new 3-stop input attenuator affording smooth control of the excellent 0.25 volts per inch vertical sensitivity. Possibility of overloading the vertical input circuit is minimized. Greater band width in the vertical channel is a decided advantage to TV service men. Permits clear observation of all TV sync pulse detail and excellent square wave reproduction over 100 kc. SCP1 intensifier type CR tube provides a brilliant trace with normal accelerating voltages. A handsome, ventilated cabinet with smooth rounded corners and a snug fitting drawn panel adds to the smartly styled professional appearance. Longer life is assured through cooler instrument operation. Push pull output stages in both vertical and horizontal amplifiers for balanced deflection of the spot. All of the many fine features of the previous model have been retained. Rear cabinet access to terminal board for direct connection to CR plates. The entire kit of all 10 tubes, parts, cabinet and panel as well as detailed construction manual for assembly and operation of the instrument included.

INTENSIFIER KIT: For extreme trace brilliance in special applications such as photography, group demonstra-tions or operation in brightly lighted areas an optional Intensifier kit providing 2200 volt operation of the CR tube is available. Kit includes high voltage filter condenser, high voltage selenium rectifier, etc. \$7.50.



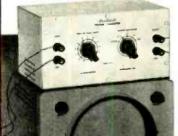
SCOPE PROBE KIT DEMODULATOR

Trouble shooting or aligning TV, RF, IF and video stages requires demodulation of high frequency signals before Oscilloscope observation. The HEATHKIT SCOPE DEMODULATOR PROBE KIT was specifically de-

No. 337 SHIP, WT. 1 LB. \$4.50

veloped for this application. Kit consists of a probe housing, crystal diode detector circuit, shielded cable and spade lugs. Assembly is simple and the probe will quickly prove its usefulness as an Oscilloscope accessory

NEW Heathkit **VOLTAGE CALIBRATOR KIT**



MODEL VC-1 SHIPPING WT. 5 LBS.

\$9.50

Use the Heathkit Voltage Calibrator with your oscilloscope to measure peak-to-peak TV com-plex waveshapes. TV manumeasure peak-to-peak TV com-plex waveshapes. TV manu-facturer's specifications indicate correct peak-to-peak voltages and this kit will permit making

and this kit will permit making these important measurements.

A big help to engineers in circuit work. Makes peak-to-peak voltage measurements of complex waveshapes of all kinds. Flat topped semi-square wave output of calibrator assures fast and easy measurement of any voltage between .01 and 100V peak-to-peak.

The Voltage Calibrator can remain connected to your oscilloscope at all times for instant use. "Signal" position connects signal under study directly through calibrator and into scope input circuit for direct observation. Eliminates transfering leads from calibrator. A wonderful scope accessory.

Heathkit **ELECTRONIC SWITCH KIT**

A few dollars spent for this accessory will increase the usefulness of a scope immeasurably. An electronic switch will open up a whole new field of scope applications for you. The S-2 allows TWO SIGNALS to be observed at the SAME TIME—this important feature allows you to immediately spot phase shift, clipping, disrortion, etc. The two signals under observation can be superimposed or separated for individual study. Each signature of the statement of the nal input has an individual gain control for properly adjusting scope trace patterns. Has both coarse and fine frequency controls for adjusting switching time. Multivibrator switching frequency is from less than 10 cps to over 2000 cps in three overlapping ranges. Kit comes complete including 5 tubes, power transformer, all controls, instruction manual, etc Every scope owner should have one!



MODEL S.2 SHIPPING WT. 11 L3S.

\$19.50

ROCKE INTERNATIONAL CORP.
13 E. 40th ST.
NEW YORK CITY (16)

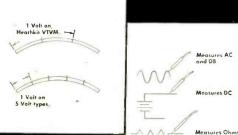
COMPAN The

... BENTON HARBOR

MICHIGAN

Heathkit VOLTMETER KI

• NEW 11/2 VOLT RANGE ON 1953 VTVM



MODEL V-6 SHIPPING WT., 7 LBS.



- New 1½ volt low range gives over 2" of scale per volt instead of less than ¾" found on 5 volt range type.
- Increased accuracy due to expanded scales. New 1500 volt DC high range
- gives 50% greater caverage. ◆ Seven ranges in all. 1½, 5, 15, 50, 150, 500 and 1500 volts DC (1000 volts maximum AC
- only),
- Provides proper service ranges 150 volts for AC DC work and 500 valts for AC type service.
- High input impedance, 11 megohms minimizes circuit laoding.
- Variety of accessory probe kits available. • 1% precision resistors in multiplier circuits.
- 200 microampere Simpson meter.
- · Center scale zero adjust.
- Transformer aperated.
- · Yest leads included.
- New cabinet styling.
- Large, clearly marked meter scales indicate ohms, AC volts, DC volts and DB.

The 1953 Heathkit V-6 VTVM has improved ranges! The lowest range has been moved way down to 1.5V full scale. This gives 3½" of actual scale length for the 1.5V covered—that's 2½ inches per volt!! Now you can make your low level measurements faster and with greater accuracy.

make your low level measurements faster and with greater accuracy.

And the upper range has been moved up. Readings up to 1500V DC can be readily made with new, improved VTVM—plus readings up to 1000V on AC. Higher ranges for extended use.

New vertical chassis mounting gives added chassis space for really easy wiring—no tight corners to worry about. Uses only highest quality components throughout. Simpson 200 microampere meter movement combined with 1% precision resistors in multiplier circuit insure highly accurate and dependable teadings.

AC and DC voltage ranges are 0-1.5V-5V-15V-50V-150V-500V-1500V. (1000V max. reading on AC)—a rotal of seven ranges for convenient, accurate readings. Instrument also measures resistance from .1 ohm to over 1 billion ohms in seven handy ranges of RX1, X10, X100, X1000, X10K, X1 Meg.,—all convenient multiples of 10 with no skips. Has Db scale in red for easy indentification.

New panel has tough baked on enantel finish for freedom from scratches and maximum durability. Modern styled, formed, compact cabinet with rounded edges and crackle finish truly handsome.

Comprehensive, detailed instruction manual with step-by-step instructions, figures, pictorials, etc. makes assembly a cinch.

assembly a cinch.

Be sure and look over the special accessory VTVM probes below — for added usefulness.

Heathkit R. F. PROBE KIT

> SHIP. WT 1 LBS. 55.50 No. 309

Extends RF range of HEATHKIT 11 megohm VTVM to 250 megacycles ± 10%.

Heathkit 30,000 V. D.C. PROBE KIT

SHIP. WT. 2 LBS. \$5.50 No. 336 Provides DC multipli-cation factor of 100 for any 11 megohm VTVM. Heathkit PEAK TO PEAK

VOLTAGE PROBE KIT No. 338

56.50

Reads on DC scale of any 11 megohm VTVM 5 kc to 5 megacycle range.

NEW Heathkit BATTERY TESTER KIT

The new Heathkit Battery Tester measures all types of dry batteries between 1½ volts and 150 volts under actual load conditions. Readings are made directly on a three-color GOOD-WEAK-REPLACE scale that your customers can readily under-stand. Operation is extremely simple and merely requires that the leads be connected to the battery under test. Only one control to adjust in addition to a panel switch for A or B battery

The Heathkit Battery Tester features compact assembly. An accurate meter movement and wire wound control mount in the portable, rugged plastic case.

Use the BT-1 to check portable radio batteries, hearing aid batteries, lantern batteries and photo flash gun batteries



SHIPPING WT. 3 LBS.

\$750

Heathkit AC VACUUM TUBE **VOLTMETER KIT**

A new AC VTVM that makes possible those sensitive AC measurements required by laboratories, audio enthusiasts and experimenters. Ten full scale ranges of .01, .03, .1, .3, I, 3, 10, 30, 100 and 300 volts RMS. 10 DB ranges from - 52 to +52 DB. Frequency response within 1 DB from 20 cycles to 50 kc. Simpson 200 microampere meter with large plainly marked meter scales. Precision multiplier resistors. Two amplifier stages using miniature tubes. A unique bridge rectifier meter circuit and a clean layout of parts. Order the AV-2 to-

day and become acquainted with the interesting possibili-ties offered by this instrument.



MODEL AV-2 SHIPPING WT. 5 LBS.

\$2950

ROCKE INTERNATIONAL CORP.

13 E. 40IN ST.

NEW YORK CITY (16)

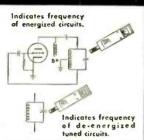
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The

 \mathbf{COM} ... BENTON HARBOR 15. MICHIGAN



NEW Heathkit GRID DIP METER KIT





Complete unit easily held and operated with one hand,

MODEL GD-1

SHIPPING WT. 4 LBS.

\$1950



New GRID DIP METER with assembled calibrated coils.

 Uses quality Simpson 500 microampere meter.

- One hand operation, extremely compact, Only 21/2" wide by 3" high by 7" long. Variable meter sensitivity control.
- Uses newest type 6AF4 high frequency triode in a Colpitts oscillator circuit.
- Continuous coverage from 2 megacycles to over 250 megacycles in 6 ranges. • Head phone monitoring jack
- AC power transformer operated for maximum safety.

Here is the GRID DIP METER KIT you have been asking for. This new HEATHKIT instrument is compact, highly sensitive and easy to use. Housed in a handsome formed aluminum cabinet—rounded corners—durable oven baked finish on panel and cabinet. The entire instrument can be easily held and operated in one hand, tuning accomplished with the thumb wheel drive. This excellent design feature leaves the other hand entirely free for making circuit.

wheel drive. This excellent design feature leaves the other hand entirely free for making circuit adjustments. The instrument with many applications — with oscillator energized, use it for finding the resonant frequency of tuned circuits, locating parasitics, determining characteristics of filter circuits, roughly tuning transmitter stages with power off, and neutralizing transmitters. Useful in TV and radio repair work for alignment of traps, filters, IF stages, peaking and compensation networks within the 2 to 250 megacycle range. With the oscillator not energized, the instrument acts as an absorption wave meter and indicates the frequency of radiating power sources. Locates spurious oscillations, as a relative indication of power in various transmitter stages, ctc. Phone jack permits monitoring of AM transmitter for determination of radiated hum, audio quality, etc. (Head phones not toring of AM transmitter for determination of radiated hum, audio quality, etc. (Head phones not included). Complete kit includes plug-in coils, tube, all necessary parts and detailed assembly and instruction manual.

Heathkit IMPEDANCE BRIDGE KIT



ANCE BRIDGE is especially useful in educational training programs, industrial laboratories and for experimental work Use it for measuring AC and DC resistance value of resistors,

determination of condenser capacitance and dissipation factor, finding coil determination of condenser capacitance and dissipation factor, finding coil inductance and storage factor, electrical measurements work, etc. Quality components: GR 1000 cycle hummer, GR main control, Mallory ceramic wafer silver plated contact switches, ½% precision resistors, etc. The basic circuit is a self powered, 4 arm bridge. Choice of Wheatstone, Capacitance comparison. Maxwell or Hay bridge circuits. Resistance from 10 milliohm to 10 megohm. Capacitance 10 mmf to 100 mfd. Inductance 10 microhenry to 100 henries. Dissipation factor .002 to 1. Storage factor (Q) I to 1000. The IMPEDANCE BRIDGE has provisions for external generator use for measurement at other than the 1000 cycle level. Take the guess work out of electrical measurements. The HEATHKIT IMPEDANCE BRIDGE mounted in a beautiful polished birch cabinet with large easy reading panel calibrations will furnish years of accurate, trouble free measurement service.

Heathkit HANDITESTER KIT

The HEATHKIT Model M-1 HANDITESTER fulfills requirements for a portable volt ohm milliammeter. This kit features precision 1% resistors, 3 deck switch for trouble free mounting of parts, specially designed battery bracket, smooth acting ohms adjust control, beautiful molded bakelite case and a 400 microampere meter movement. 5 convenient AC and DC voltage ranges as follows: 10 - 30 - 300 -1000 - 5000 volts. Ohms ranges 0-3000 and 0-300,000. DC milliampere ranges 0 - 10 milliamperes and 0-100 milliamperes. The instrument is easily assembled from complete instruc-

tions and pictorial diagrams. Test leads are included. Carry the HEATHKIT M-1 HANDITESTER in your tool box at all times for those simple jobs and eliminate that extra trip for additional testing equipment.



MODEL M-1 SHIPPING WT. 3 LBS.

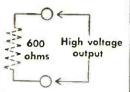


The

... BENTON HARBOR 15. MICHIGAN

Heathkit AUDIO GENERATOR KIT

• RANGE EXTENDED TO 1 MEGACYCLE



Low impedance output High voltage output

Sine wave output from 20 cycles to 1 megacycle.

MODEL AG-8 SHIPPING WT. 16 LBS.

• Improved design - new low price.

• Frequency coverage in five ranges from 20 cycles per second to 1 megacycle.

Response flat 1 DB from 20 cycles to 400 kilocycles. Down 3 DB at 600 Elocycles. Down only 8 DB at 1 megacycle.

• Five calibrated output voltage ranges, continuously variable 1 mv, 10 mv, 100 mv, 1 v, 10 v.

• Low impedance output circuit. 600 ohms.

Distortion less than .4 of 1% from 100 cycles per second through the audible range.

 New HEATHKIT universal type binding posts.

 Durable infra-red baked enamel panel.

 Transformer operated for safe operation.

Sturdy, ventilated steel

A new Audio Generator with features hererofore found in only the most expensive generators. Such features as complete coverage from 20 cycles to 1 Mc — response flat ±1 db from 20 cycles to 400 Kc, down 3 db at 600 Kc and down only 8 db at 1 Mc.

And it has calibrated output . . . Calibrated continuously variable and step attenuator output controls allow you to easily set calibrated output voltage. Moreover, distortion is less than .4 of 1% from 100 cps through the audible range.

Oscillator section consists of a two stage resistance coupled amplifier (6SJ7 and 6AK6) utilizing both positive and negative feedback for oscillator operation and reduction of distortion. Oscillator section drives a cathode follower output power amplifier (6AK6) which isolates the oscillator from variations in load and presents a low impedance output (600 Ohms). Power supply is transformer operated and utilizes 6X5 rectifier with 2 sections of RC filtering.

An unbeatable dollar value — for here is an audio generator with wide frequency coverage, excellent frequency response, stepped and continuously variable calibrated output, high signal level, low impedance output, and low inherent distortion.

Heathkit Audio Frequency Meter Kit



The HEATHKIT AUDIO FREQUENCY METER provides a simple and easy way to check unknown audio frequencies from 10 cycles to 100 kc between 3 and 300 volts RMS. The The meter itself has a quality 200 microampere Simpson movement and large clearly marked scales. The AUDIO FREQUENCY METER is transformer operated and features

SHIPPING WT. 15 LBS.

MODEL AF-1 \$34.50

a voltage regulator tube to maintain constant plate voltage on the second stage. Kit sup-plied complete with all necessary construction

material and a detailed construction manual.

NEW Heathkit **AUDIO OSCILLATOR KIT**

MODEL AO-1

A new Audio Oscillator with both sine and square wave covetage from 20 to 20,000 cycles... An instrument designed to completely fulfill the needs of the audio engineer and enthusiast — Has numerous advantages such as high level output (up to 10V obtainable across the entire range), distortion less than .6%, and low

impedance output.

Special design features include the use of a thermistor in the second amplifier stage for keeping the output essentially flat across the entire range.

A cathode coupled clipper circuit produces good, clean, square waves with rise time of only 2 microseconds. Oscillaror section uses precision resistors in range multiplier

circuit for greatest accuracy.
You'll like the operation of this fine new kit.

Heathkit SQUARE WAVE GENERATOR KIT

The HEATHKIT SQUARE WAVE GENERATOR is an excellent square wave frequency source with wide range coverage from 10 cycles to 100 kc continuously variable. This feature makes it useful for TV and wide band amplifier work as well as audio experimentation. The output voltage is continuously variable between 0 and 20 volts. The circuitry consists of a multivibrator stage, a clipping and squaring stage and a cathode follower low impedance output stage. The power supply is transformer operated and utilizes a full wave rectifier, circuit with two sections of filtering. Another excellent HEATHKIT value at this remarkable low price. Kit includes all necessary construction material as well as complete instruction manual for assembly and operation.



MODEL SQ-1

\$29.50



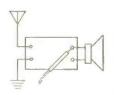
The

NEW Heathkit SIGNAL TRACER KIT

• NEW NOISE LOCATOR AND WATTMETER CIRCUITS.

Both visual and oural





Traces signals from antenna lear through speaker

SHIPPING T. 8 LBS.

MODEL T-3



 Permits visual signal observation as well os aural oper-

ation.

Two separate input channels.

Tremendous RF channel sensitivity. Adequate for actual signal detection at receiver

Separate high gain RF and low gain audio channels.
A unique and useful noise locoter circuit.

Built-in colibrated wattmeter.

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provides a means of correct-ly aligning TV receivers. The instrument furnishes a frequency modu-lated signal covering in 2 bands the range of 10 to 90 megacycles and 150 to 230 megacycles. An absorption type frequency marker covers from 20 to 75 megacycles in 2 ranges; therefore you have a simple, convenient means of checking IF's independent of oscillator calibra-tion. Sweep width is variable from 0 to 12 megacycles. Other excellent features are horizontal sweep voltage controlled with a phasing control — both step and continuously variable attentuation for setting the output signal to the desired level — a convenient stand by switch and blanking for establishing a single trace with a base reference level. Make your work easier, save time and repair with confidence. Order your HEATHKIT TV ALIGNMENT GENERATOR now.



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Checks 7, 8, 9 prong tubes, octals, loctals, 7 and 9 prong miniatures, 5 prong Hytrons, pilot lights.



emission, filament and filament tap continuity,

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 Beautiful counter type birch cabinet.

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MODEL RS-1

\$550

NEW HEATHKIT RESISTANCE SUBSTITU-NEW HEATHKIT RESISTANCE SUBSTITU-TION BOX KIT provides switch selection of any single one of 36 RTMA 1 watt 10% standard value resistors, ranging from 15 ohms to 10 meg-ohms. This coverage available in 2 ranges in decades of 15, 22, 33, 47, 68 and 100. Housed in rugged plastic cabinet featuring new HEATHKIT universal type binding posts. The entire kit priced less than the retail value of the resistors alone.

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MODEL VT-1

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Modulated or unmodulated RF output.



MODEL SG-7

SHIPPING WT. 7 LBS.

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400 cycle sine wave



• Step attenuated RF ouput.

- 6 to 1 vernier dial ratio.
- Turret mounted coil sub-
- Pre-calibrated and adjusted coils.
- Hartley RF oscillator circuit.
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- Modulated or unmodulated RF output.
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- RF output in excess of 100,-
- Audio output 1½ to 2 volts.
- AC transformer aperated.
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Heathkit AMPLIFIER KIT WILLIAMSON

The new HEATHKIT WILLIAMSON TYPE AMPLIFIER incorporates the latest improvements described in Audio Engineering's "Gilding the Lily." 5881 output tubes and a new Peerless output transformer with additional primary taps afford peak power output of well over 20 watts. Frequency response ±1 db from 10 cycles to 100 kc. allows reproduction of highs and lows with equal crispness and clarity. Harmonic and intermodulation distortion have been reduced to less than ½ of 1% at 5 watts. This eliminates the harsh unpleasant qualities which contribute to listening fatigue. Make this amplifier the heart of your radio system to achieve the fine reproduction that is the goal of all music lovers.

The HEATHKIT PREAMPLIFIER (available separately or in combination with the amplifier kit) features inputs for magnetic or low level cartridges, crystal pickups and tuners, turnover control for LP or 78 type records, individual bass and treble tone controls each providing up to 15 DB of boost or attenuation. Special notched shafts on preamplifier controls and switches adaptable to custom installation. The preamplifier can be mounted in any position and a liberal length of connecting cable is supplied. No radio experience is required to construct this amplifier. All punching, forming, or drilling has already been done. The complete kit includes all necessary parts as well as a detailed step by step construction manual with pictorial diagrams to greatly simplify the construction.

ACROSOUND TRANSFORMER OPTION. If desired, the output transformer with the kit will be the Acrosound output transformer, type TO-300. The use of this transformer permits ultra-linear operation as described in Audio Engineering's "Ultra-Linear Operation of the Williamson Amplifier."



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Heathkit FM TUNER KIT



MODEL FM-2 SHIPPING WT. 9 LBS.

HEATHKIT MODEL FM-2 The HEATHKIT MODEL FM-2 TUNER specifically designed for simplified kir construction features a preassembled and adjusted tuning unit. Three double tuned IF transformers and a discriminator transformer are used in an 8 tune circuit.

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Heathkit ECONOMY 6 WATT

AMPLIFIER



MODEL A-7 SHIPPING WT. 10 LBS.

\$ 450

The HEATHKIT Model A-7 amplifier features beam power, push pull output with frequency esponse flat ± 1½ DB from 20 to 20,000 cycles. Separate volume, bass and treble controls. Two inbass and treble controls. Two input circuits, output impedances of 4, 8, and 15 ohms. Peak power output rated at full 6 watts. High quality components, simplified layout, attractive gray finished chassis, break off type adjustable length control shafts and attractive lettered control panel.

THE MODEL A7A amplifier incorporates a preamplifier stage with special compensated network to provide the necessary voltage gain for operation with variable reluctance or low out-...\$16 50

Heathkit HIGH FIDELITY 20 WATT AMPLIFIER KIT

The HEATHKIT MODEL A-8 amplifier kit was designed to deliver high fidelity performwas designed to deliver high indelity performance with adequate power output at moderate cost. The frequency response is within ± 1 DB from 20 to 20,000 cycles. Distortion at 3 DB below maximum power output at 1000 cycles is only .8%. The amplifier features a Chicago power transformer in a drawn steel case and a Peerless output transformer with output impedances of 4.8 and 16 others available. Senerate Peerless output transformer with output impedances of 4, 8, and 16 ohms available. Separate bass and treble tone controls permit wide range of tonal adjustment to meet the requirements of the most discerning listener. The amplifier uses a 6SJ7 voltage amplifier, a 6SN7 amplifier and phase splitter and two 6L6's in push pull output and a 5U4G rectifier. Two input jacks for either crystal or tuner operation. The kit includes all necessary material as well as a detailed step by Step construction manual. step construction manual.



MODEL A-8 SHIPPING WT. 19 LBS.

MODEL A8-A features an added 6SJ7 stage (preamplifier) for operating from a variable reluctance cartridge or other low output level phono pickups. Can also be used with a microphone. A 3 position panel switch affords the desired input service.



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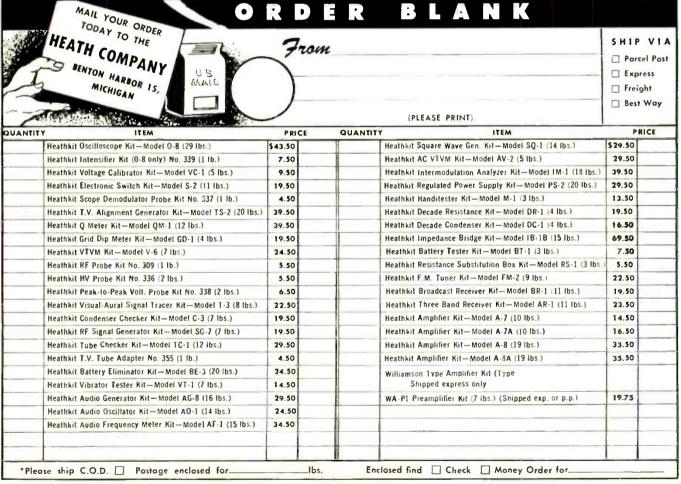
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ELIMINATING OSCILLATOR HUM IN FM RECEIVERS

BY HERBERT MICHELS

AN OFTEN troublesome problem, especially in high fidelity systems, is the elimination of 60-cycle hum originating in the local oscillator of an FM receiver. This hum, noticeable only when a station is tuned in, is the result of the a.c. heater voltage applied to the oscillator tube causing frequency variations in the local oscillator's output at a 60-cycle rate.

The discriminator circuit, responding to modulation of the local oscillator as well as the incoming station, will feed this 60-cycle component on to the audio

system

Oscillator hum is most apparent in circuits in which the cathode is not at r.f. ground potential; however, it also can be troublesome in other types of oscillator circuits. Fig. 1A illustrates the most common circuit wherein the 60-cycle potential between the cathode and the heater of the tube will result in frequency modulation of the oscillator.

There are various methods of eliminating the hum—the easiest, but perhaps least practical, is the careful selection of tubes. However, this can be rather expensive if it means buying extra tubes for the purpose. Fig. 1B shows another, and far more practical, method of hum elimination.

In the circuit as shown in Fig. 1B one side of the heater is connected to the cathode which is connected to ground through the coil. This places the heater at an above ground potential as far as r.f. is concerned. Therefore, it is necessary to place an r.f. choke (20 turns of #12 wire on a ½ inch form closewound) in series with the other heater lead. This often brings satisfactory results; however, it also changes the resonant frequency of the tuning circuit. A frontend realignment of the receiver is necessary to assure proper tracking.

A third method as shown in Fig. 1C often brings successful results without

the necessity of realignment. This method is to place a high d.e. potential on the heater system. This potential must not be higher than the maximum allowable heater-eathode potential for the tube being used. It may be necessary to use a tapped bleeder across the "B+" supply to secure the proper potential.

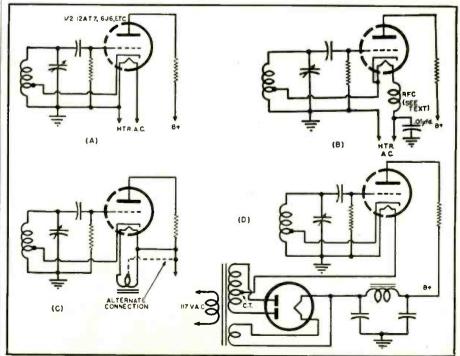
Since a heater circuit in which one side of the heater supply (or transformer center tap) is grounded would result in a shorted plate voltage supply, it is necessary to first remove any ground connections from the heater circuit before connecting the "B+" to the heaters.

One is fortunate if the total current drawn from the d.c. supply in the reeciver closely approximates the required heater current of the oscillator tube. If so, this permits the use of the circuit as illustrated in Fig. 1D; a superior method of hum climination.

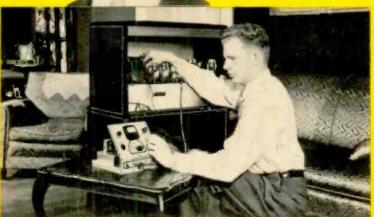
The rated values of plate current as listed in a tube manual, or more accurately an actual meter measurement, will determine the current in the d.c. supply. The heater should be connected in the power transformer center tap ground return circuit—this eliminates the possibility of damaging the filter condensers in the event of a tube failure.

One final note: hum in an FM receiver may originate from many sources. This could be due to improper d.e. supply filtering, poor circuit design, insufficient shielding, etc. Determine if the local oscillator is the cause of the hum before proceeding to take corrective measures. To do this, disconnect the heater supply voltage from the oscillator tube heater pins. Then connect a battery of the required voltage to light the tube. If the hum disappears when the battery is substituted for the a.c. heater supply it is an indication that the oscillator is the cause of the hum.

Fig. 1. (A) Typical FM receiver oscillator circuit. (B) Heater circuit modified for hum reduction. (C) Heater at high d.c. potential. (D) A d.c. heater supply.



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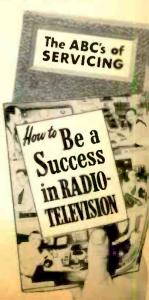
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For additional information on any of the items described herein, readers are asked to write direct to the manufacturer. By mentioning RADIO & TELEVISION NEWS, the page and the issue number, delay will be avoided.

NEW "PILOTUNER"

An FM-AM radio tuner for use as the central control head of a hi-fi music system is now available from *Pilot Radio Corporation*, Long Island City, N.Y.

The Model AF-821 is a 9-tube unit with a two-stage preamp with adjust-



able equalization for various makes of reluctance cartridges, separate input connections for phono and TV operation, extended range bass and treble controls, temperature compensated oscillator for drift-free FM reception, a.f.c., built-in antennas, and full shielding.

G-E CARTRIDGES

General Electric Company has added three wide-range variable reluctance phonograph cartridges to its line.

The RPX 053 dual and the RPX 061 and RPX 063 single are 15,000 cycle units and all feature diamond styli. The new cartridges feature 6 to 8 grams tracking pressure for all types of records, uniform velocity scratch and needle talk. The stylus is retractable.

"STEREOPHONIC RECORDER"

Ampex Electric Corp., Redwood City, Calif. is marketing a stereophonic recorder which employs a dual-track head assembly that records or plays back two separate channels simultaneously.

Material recorded by two properly placed microphones may be played back through two similarly spaced speakers to give a directional effect. The Model 403-2 incorporates separate



electronic assemblies for each track. These assemblies are identical except that the second sound track has a bias buffer amplifier rather than the bias oscillator of the first assembly. This is done to provide the same bias frequency to each record head.

The new model will operate at either 7½ or 15 inches-per-sec. tape speeds. Frequency response is to 15,000 cycles at the 7½" tape speed and signal-to-noise ratio is over 55 db.

CABINET SPEAKER

White Sound, Inc., 105 W. Madison St., Chicago, Ill. is marketing a new line of cabinet speakers based upon development of an exponential horn, folded within an enclosure.

There are four of these horn-loaded units available at the present time. The company will provide complete specifications on request.

PLUG-IN AMPLIFIERS

Four basic plug-in audio amplifiers are now available from *Gates Radio Co.*, Quincy, Ill.

The Model PRE-1 preamp, Model PGM-1 program amplifier, Model MON-1 monitoring amplifier, and Model PWR-3 regulated power supply can be combined in any assembly. All units are identical in size except the



PRE-1 which is half-size. Four program amplifiers can be used in the space formerly occupied by a single unit.

RADIO CONTROL UNITS

Vernon C. MucNabb Co., 909 West-field Blvd., Indianapolis 20, Ind. is offering a 27.255 kc. Citizens band receiver and transmitter for radio control operations.

The receiver, which weighs 4 ounces and measures $2\frac{1}{2}$ " x $1\frac{3}{4}$ " x $2\frac{1}{4}$ ", gives a 5:1 plate current change to operate the Sigma 4F adjustable relay.

The hand-held transmitter, weighing 4 pounds and measuring 3" x 4" x 9", uses two 3V4 tubes. A three-section plug-in antenna is employed.

BASIC AMPLIFIER

A basic amplifier for the average home system is being marketed by Precision Electronics, 9101 King Ave., Franklin Park, Ill. as its Model 100 BA

Power output is 10 watts with 20

RCP is FIRST again with this . . . LOO-ALL TV Set and Tube Tester (Includes VT Voltmeter and Reactivator)



Model 808 ALL IN ONE UNIT!

- A TUBE TESTER: All the features of the famous 323 Dynoptimum free point tube tester—protected against obsolescence—tests all modern standard, miniature, noval base and subminiature tubes. Easily read on 4 ½" meter.
- A CATHODE RAY TUBE TESTER: Will check all magnetic deflection type Television Picture tubes. Locates and isolates all shorts or leaks.
- A REACTIVATOR: Revives and Reactivates many otherwise Dim or Bad Television Picture tubes.
 Can also be used on other tubes.
- ◆ A VT VOLTMETER (AC-DC): This really outstanding 17 Range instrument is a VT Voltmeter for AC os well as DC. Balanced bridge type pushpull circuit. Draws negligible current due to high impedance of 25 megohms. Accuracy ± 3% DC, ± 5% AC. Discriminator alignment scale with zero center. AC & DC volts 0 to 5-25-100-250-1000: db-20 to 16,-6 to 30, 6 to 42, 14 to 50, 26 to 62.
- ♠ AN OHMMETER: Reods all Resistances 0.2 ohms to 1000 megohms on 5 ranges. Use this Instrument also to check condensors for leakage and shorts.

Housed in handsome hand-rubbed oak carrying case with test leads, isolation probe, batteries, etc. Size 12 $\frac{1}{2}$ x 12 $\frac{3}{4}$ x 4 $\frac{3}{4}$; weight 12 $\frac{1}{2}$ lbs.

MODEL 808—complete, 199.95 ready to operate. In Model 808. Extends Ronge of VTVM to 30,000 volts.

MODEL No. HVMP-1.....\$8.9

For the "GREATEST VALUE PER DOLLAR IN TV-RADID TEST EQUIPMENT" send for the new, colorfut, fully illustrated 1953 RCP catalog. Complete details on Model 808 and other instruments in this top-quality line are

MAIL COUPON NOW FOR

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	RADI	0 CI	TY P	ROD	UCTS	co.	Inc.	
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colorful quality		ated Cat ent line.	featuri	ng th	e top

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CITY.....STATE.....



watts peak. Distortion at 10 watts is 1% harmonic and 2% intermodulation. Frequency response at 3 watts is \pm .5 db, 20 to 50,000 cps. Frequency response at 10 watts \pm 1 db, 30 to 20,-000 cps.

POWER AMPLIFIER

Brociner Electronics Lab., 1546 Second Ave., N.Y. 28, N.Y. has developed the Model UL-1 power amplifier which is an "ultra-linear" modification of the Williamson circuit.

Frequency response is from 10 to 200,000 cycles within 1 db. Power output is 20 watts from 30 to 20,000 cycles and 12 watts from 15 to 50.000 cycles. A power take-off socket sup-



plies filtered plate voltage and heater power for use with preamps. The distortion is 2% intermodulation at 20 watts and less than .1% at 1 watt. Hum and noise level is 80 db below 20 watts. The amplifier uses two 12AU7's, two 6BG6G's, and one 5V4G tube.

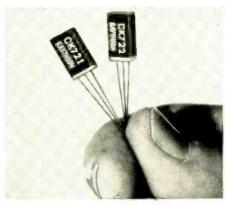
FOUR-WATT RESISTOR

International Resistance Co., 401 N. Broad St., Philadelphia 8, has added a new power resistor, type PW4, rated at four watts, to its line.

The new type is available in resistances from 1 to 8200 ohms in \pm 5% and ± 10% tolerances. It is 1%" long by 21/64" dia. It can be used in television circuits requiring 2 to 3 watts actual dissipation at high ambient temperature since the unit is completely insulated with an inorganic core material molded in a high temperature plastic which will not support combustion.

TRANSISTORS AVAILABLE

Raytheon Mfg. Co., 55 Chapel, Newton 58. Mass. now has two p-n-p ger-



manium junction transitors available the types CK721 and CK722.

The CK722 is available in production quantities but the CK721 will be limited in quantity until April. Both units have a 22 db noise factor at 1000 cycles. Power gain of the CK721 is 38 and the CK722 is 30 db. Leads may be soldered or welded or cut for insertion in subminiature sockets.

Technical specifications are available from the Technical Information Service of the company or the company's sales offices in N.Y., Chicago, and Los Angeles.

ALKALINE DRY BATTERY
A new alkaline "B" radio battery has been developed by RCA which is 25 per-cent smaller than present comparable types yet offers double the playing capacity.

Designed specifically for use in "personal portables" the 671/2 volt battery (VS216) utilizes the alkaline-cell principle formerly incorporated only in wet-type batteries.

The company has redesigned its "A" battery to provide balanced life operation with the new "B" battery. The new "A" unit (VS236) is twice the length of the standard cells but has a life capacity nearly four times greater. Two of these batteries will balance the life of the new alkaline "B" battery in "personal portable" applications.

UNIQUE BATTERY CAP

Industrial Research Inc., 4016 N.W. 29th St., Miami 42, Fla. is producing a new storage battery cap which preserves the water in batteries, prevents corrosion, and warns of overcharge or impending battery failure.

The "Hydrocap" contains a catalyst



which converts the battery's escaping hydrogen and oxygen gases back into water. Full details on these new units are available on request.

BINAURAL ARM

Livingston Electronic Corp. of Livingston, N.J. has developed a binaural transcription arm which plays either conventional or binaural recordings, uses conventional cartridges, costs less than two separate arms, and is especially designed for easy adjustment.

The unit provides independent action for each cartridge and has negligible tracking error.

CITIZENS RADIO GEAR

Motorola, Inc. of Chicago has received FCC approval on its Model T44A mobile receiver and L44A base station equipment for operation in the 460-470 mc. Citizens band.

The receiver circuit includes the (Continued on page 124)

RADIO & TELEVISION NEWS

CARRYING CHARGES!!

USE CONVENIENT TIME PAYMENT ORDER BLANK BELOW

Superior's New

Handsome round cornered molded bakelite case 31/6" molded bakelite case 31/8" x 57/8" x 21/4" complete with all test leads and instruc-

MOST COMPLETE AND COMPACT MULTI-SERVICE INSTRUMENT EVER DESIGNED

- Measures: * Voltage * Capacity * Current
- * Decibels Resistance * Inductance
- * Reactance

*Reactance

*Reactance

*Reactance

*Reactance

*Reactance

*Specifications: D.C. Volts: 0-7.5/75/150/

750/1500 Volts. A.C. Volts: 0.15/150/
300/1500/3000 Volts. Resistance: 0-10.000/100.000 ohms. 0-10 Megohms. D.C.

Current: 0-7.5/75 Ma. 0-7.5 amps. Capacity: 001 Mrd.—2 Mrd. 1 Mrd.—
20 Mrd. Electrolytic Leakage: Reads
quality of electrolytics at 150 Volt
test potential. Decibels: —10 Db to
+18 Db. + 10 Db. to + 38 Db. +
38 Db. to + 58 Db. Reactance: 15
ohms—25 K ohms 15 K ohms—2.5
Megohms. Inductance: 5 Henry—50
Henries 30 Henries—10 K Henries.

Plus Good-Bad scale for checking
the quality of electrolytic condensers.

Superior's New Model 670-A



The Model 670-A comes housed in a rugged, prackle-finished steef calinet complete with test leads and operating Instructions, Size 614"x91/2"

A COMBINATION VOLT-OHM MIL-LIAMMETER PLUS CAPACITY RE-ACTANCE INDUCTANCE AND DEC-**IBEL MEASUREMENTS**

SPECIFICATIONS: D.C. VOLTS: 0 to 7.5/15/75/160/750/1.500/

7,500 Volts.
A.C. VOLTS: 0 to 15/30,150/300/1,500/3,000 Volts
OUTPUT VOLTS: 0 to 15/30,150/300/1,500/

D.C. CURRENT: 0 to 1.5/15/150/ Ma. 0 to

1.5/15 Amperes
RESISTANCE: 0 to 1,000/100.000 Ohms 0 to 10 Megohms
CAPACITY: .001 to 1 Mfd. 1 to 50 Mfd. Quality test for electrolytics)
REACTANCE: 50 to 2.500 Ohms, 2.500 Ohms to 2.5 Megohms
INDUCTANCE: .15 to 7 Henries 7 to 7.000

28⁴⁰

DECIBELS: —6 to +18 +14 +38+34 to +58
ADDED FEATURE:
The Model 670-A includes a special GOOD-BAD scale for checking the quality of electrolytic condensers of a test patential of 150 Volts.

Superior's Model 660-A-A NEW A.C. OPERATED



Provides Complete Coverage for A.M.—F.M. and TV Alignment

• Generates Radio Frequencies from 100 Kilocycles to 60 Megacycles on fundamentals and from 60 Megacycles to 220 Megacycles on powerful harmonics. • Accuracy and stability are assured by the use of permeability trimmed III.Q colls. • R. F. available separately or modulated by the internal audio oscillator. • Built in 400 cycle sine wave audio oscillator used to modulate the R. F. signal also available separately for audio testing of receivers, ampiliers, hard of hearing alds, etc. • R. F. Oscillator Circuit; A high transconductance heptode is used as nR. F. oscillator, mixer and ampilifer. Modulation is effected by electron coupling in the mixer section thus isolating the oscillator from load changes and affording high stability. • A. F. Oscillator Circuit; A high transconductance heptode connected as a high-transconductance heptode content high transconductan Generates Radio Frequencies from 100

Superior's New Model TV-11



Operates on 105-130 Volt 5 60 Cycles A.C. Hand-rubbed oak cabinet complete with portable cover

lises the new self-cleaning Lever Action Switches for Individual ele-ment testing. Because all elements are numbered according to pin numare numbered according to pin number in the RMA base numbering system, the user can Instantly identify which element is under test. Tubes having tapped filaments and tubes with filaments terminating in more than one pin are truly tested with the Model TV-11 as any of the pins may be placed in the neutral position when necessary. • Uses no combination type sockets. Instead individual sockets are used for each type of tube. Thus it is impossible to damage a tube by inserting it in the wrong socket. • Free-moving built-in roll chart provides complete built-in roll chart provides complete data for all tubes. • Phono jack on front panel for plugging in either phones or external amplifier detects microphonic tubes or noise due to faulty elements and loose external connections

Superior's New

THROWS AN ACTUAL BAR PATTERN ON ANY TV RECEIVER SCREEN!!



TV Bar Generator comes com. \$3995 tal sweep signal for oldetailed operating instructionsOnly NET

Connects direct to antenna post. No connection inside receiver.

Features.-Can be used when no stations are on the air. · Provides linear patterns to adjust vertical and horizontal linearity . Provides vertical and horizontal sweep signals . Provides signal for testing

TIME PAYMENT PLAN NEW ORDER BLANK

MOSS ELECTRONIC DISTRIBUTING CO., INC.
Dept. B-49, 38 Murray Street, New York 7, N. Y. Please send me the units checked below. I an enclosing the down payment with order and agree to have the monthly balance as shown. It is understood there will be no carrying, interest or any other charges, provided I send my monthly nay- ments when due. It is further understood that should I fail to finke payment when due, the full unpaid halance shall become immediately due and payable.
JUNIOR SUPER METER. Total Price \$21.40 \$5,40 down payment, Balance \$4.00 monthly for 4 months.
MODEL TV-11 Total Price \$47.50 \$11.50 down payment. Balance \$6.00 monthly for 6 months.
MODEL 670-A
TELEVISION BAR GENERATOR. Total Price \$39.95 \$9.95 down payment. Balance \$5.00 monthly for 6 months.
MODEL 660-A Total Price \$42.95
□ I enclose \$ as down bayment.
Ship C.O.D. for the down payment.
Signature
Name
Address
Zone State

POLICY PROFIT MEANS GREATER



DELUXE MODEL

STOCK NO. RA-69

HI-FI DELUXE MODEL

STOCK NO. RA-113
Equipped with "Turnover" artridge and dual needle, hee side for 30 Mg and 45 PM discs and other side or 78 RPM discs. Both ides equipped with predious metal long-lasting list. Rectular retail price 52.50. Sppg. wt. 15

52.50. Shpg. wt. 15 ba. Single. each \$21.99 n lots of 3, ach, only.

GIANT 3-SPEED RECORD CHANGER SALE!

3-SPEED GENERAL INSTRUMENT

AUTOMATIC RECORD CHANGER STOCK NO. RA-69 Equipped with single needle, with precious per talliong-lasting tip. By the speed records, speed records, side, side, speed records, side, side,

Automatically Changes All Sizes-7", 10" and 12"

All Speeds—331/3, 45 and 78 RPM

All the finest features are incorporated in these General Instrument Record Changers, Records Slide Gently flown the center shindle. There is no wobble, no scrape, no slap. No chance of ilamaging your records. The newly-designed controls are 80 simple, they exhiain themselves. No instructions needed. All moving parts in every General Instrument Changer are factory adjusted thus insuring years of trouble-free performance.

anjosed thus insuring years of frount-free performance.

These Changers are Precision-built by craftsmen who have had years of experience. Every Changer is brand new—In original factory-sealed cartons—and guaranteed 100% by Olson and the manufacturer. Here is one of Olson's mout sonsational bargains. Believe us—you can't go wrong.

Changer can be connected to any radic or ampliner. Equipped with clever "touch-plate"—a slight press and you can't go to the connected to any radic or ampliner. On the proof of the connected to the parts. Here's a Changer you'll be proud to demonstrate to your friends. You can sell plenty of them too. Operates on 115 Volts AC, 00 cycle. Base \$2x 12"x12"b", 3½" hotoy plate and 3½" below. Take your choice of either model.

COMPLETE 3-SPEED RECORD CHANGER AMPLIFIER KIT

Easily Assemble Your Own Automatic Record Player

Stock No AS-71 FOR ONLY

	Regular ist Price
3-Speed Changer	. \$47.50
Ambiliner (Wired)	. 7.50
Set of 3 Tubes	4.55
5" Heavy Buty Speaker	4.00
Output Transformer	. 1.75
Mounting Base (Pre-Drilled).	. 8.50
Mounting Hardware	55

STOCK NO.
W-115
SOO Ft. Spool
Single,
Ea. \$7,95
Lots of 2
Spools

LOWER LOSS 300 OHM

SLOTTED SUPER SPACE LINE

This slotted 300 ohm TV line is made to standard specifications in such a manner as to provide maximum air spacing while maintaining the demander of the standard specific with the specific or the specific property of the





You Get Everything You Need to Easily Assemble Your Own 3-Speed Automatic Record Player. Kil In-cludes:

GENERAL INSTRUMENT IMPERIAL DELUXE CHANGER (Model RA-69 — as described to left).

PM HEAVY-DUTY SPEAKER AND OUTPUT TRANSFORMER. 3-TUBE AMPLIFIER COMPLETE WITH TUBES

MOUNTING BASE-WITH HARD-WARE & INSTRUCTIONS

DON'T THROW AWAY

OLD PICTURE TUBES

BOOST BRILLIANCE

WITH THIS TV TUBE BOOSTER ompletely automatic asy to install—no tools ecded. Just plug into old leture tube that is starting to dim and watch the lg change. Works on any une—10 to 30 ft in all C parallel circuits. Adda

HIGH GAIN STANDARD COIL TV BOOSTER

- ★ Latest Model ★ Brand New ★ Reg. List Price \$30.00

\$52.50.

Latest Model & Brand New
Reg. List Price \$30,00
While they last. Model No. B-51. \$ 1095
Est connect one of these Standard TV Just connect one of these Standard TV

Bossters to your receiver and get with the standard transpler includers and less small transpler includers and less small transpler includers and less small transpler includes the standard transpler includes the sets. An amazing deal-you can cash In-sive sets. An amazing deal-you can cash In-sive money — Order Today. Tunes all 12 claimates. Uses a 64k3 tube and a selentum rectifier. Complete. Oberates on 115 V. AC. Shgs. wt. 6 lbs.



12" Magnavox Speaker and Baffle Close-Out



Stock No.

A5-66
Get both for only.

5795
In lots of 4 sets.

Shift, wt. 12 libs.

Shift, wt. 12 libs.

Shift at a more sets and install them in restaurants, auditoriums. halls.



\$ 69

DELUXE COUNTER

BIG INSULATED
RESISTOR KIT
OLSON SPECIAL PRICE
Contains a carefully selected assortment of 100
Sinadard Risk even of the code.
Sinadard Risk even of the code.
Included are 70-16 watt. 20-1 watt and 10-2 w at t resistors.
Handssmely packed in a durable pilohim is a g
I e gu i ar List Price We're letting these go at a fifth of Actual Cost -88.50. Keep an accument of 100 in surfact ed resistors. Standard BMA color code. Included are 70— transactions, traffic, production, etc. Just touch stock No. a lever and it counts. X-298. Shpg. wt. 1 lb.



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OLSON ELECTRIFYING

499

BARGAIN! THE NEW WONDER OF ELECTRONIC CONTROL CAN BE YOURS FOR PRACTICALLY NOTHING THYRATRON REMOTE CONTROL

SERVICEMEN-HOBBYISTS-HAMS EXPERIMENTERS-RADIO SCHOOLS

EXPERIMENTERS—RADIO SCHOOLS

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Remote Control of your own at a fraction of its regular price! This mighty handful only 53a "85a" "Su" of miracle perform hundreds of practical. accurating feats of remie common of the second of t

POWER CORD makes it easy to connect to 115 V AC line. Consists of 12 rt. heavy rubber covered wire with rubber molded plugs. STOCK NO. W-116, ea., 49c.

Can easily and quickly be modified for Electronic Remote Control of: Transmitters: Turn Radio and TV on and off: Open and off: Open and off: Open and cost off from your carrier boors from your carriers. Schematic Dingram Included at No Extra Cost.

You get the complete outfit, including cabinet, 3 tubes (681.7, 68N7 and GL-5662) and wiring diagram.

STOCK NO. RA-111

RA-111 Single, each, \$5.99 Lots of 3, each

what you get: Valuable parts and thes galore that you can so easily use in any other radio, amplifier, etc.—or for experimenting.

• SSL7 and 6SN7
• 175 Ohm Var, Control • 240,000 Ohm—1/2
• 603 Ohm Calibration
• 604 Ohm Calibration
• 1 Mid, #200 Volts
• 2600 Ohm—1/2 Watt
• Wirewound
• 33 Ohm—1/2 Watt
• Wirewound
• 33 Ohm—1/2 Watt
• Wirewound
• 15,000 Ohm—1



STOCK NO. AS-67

COMBINATION DEAL!

12" CO-AXIAL SPEAKER FOR \$3995 WITH TUBES COMPLETELY WIRED

COMPLETE WITH

Order this matched outful today. You get the 10-Watt HI-Fi Ambilifier PLUS the 12" Co-Axial Speaker both as described below. Can be built into any cabinet of blookcase—giving you a complete Amplifier System of which you can be proud. Ships, wt. 25 lbs.
Amplifier is completely assembled and ready to play. Built-in PRE-AMP for G.E. amid similar types of magnetic pickulis. 4 inputs: 1 crystal phono. 1 magnetic phono. 1 radio. 1 mike. 4 Controls: 1 Bass. 1 Trebet. 1 Volume. 1 Phono-radio Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Output impecances: 4, 8, 16 ohms. Peak power output 17 Page. Switch. Switch. 15 ohms. 15 page. 15

2" x 61½" x 51½"

r is our new 1953 Co-axial Model, Guaranteed to outperform any speaker price class. Equipped with two "high concentration". Alrice 5 magnets high frequency diffuser. The 12" section delivers the bass while the 3 tweeter speaker section delivers the trebe tones. Together they give all the concentration of the concentration of

TECH-MASTER New Williamson-Type Amplifier Kit

Stock No. \$4895 COMPLETE KIT, ONLY 48 with Tubes

Full 15 Wotts—Ultra Linear • Includes
Altec Lansing Peerless Audio Transformer
Complete Kit of exact transformers, condensers, re-Complete Kit of exact transformers, condensers, re-alstors, sockets, tithes, bardware, punched chassis-veery part you, need-sa well as a full detailed wir-court for high idelity reproduction. Out top quality cuit for high idelity reproduction. Out top quality harts are included-specially wound ALTEC LAN-SING Peerless Transformers, for instance, are em-sistent factors.

SING Peerless Transformers, for Instance, are employed. Easy to assemble.

SPECIFICATIONS: Output Imbedance—4-8-16 ohms: Inhut Impedance—fligh for crystal pickups, tuners, pre-amps, etc., Response—8 cps to 80,600 cps to 5 these 2—18N7, 2—368t, 1—3v46;: 105-4-123V, 50-60 cycles 120 W. Size—9°x12"x 61½. Shpg. wt. 27 lbs.

TECH-MASTER 4 CHANNEL PRE-



Williamson Amplifier

\$ 1955 with Tubes williamson Amplifier

4 input channels and
selector switch forcrystal and refuctance
pick-urs, tape or wire
recorder, etc. 3 postitlon equalizer switch permits selection of
turnover and resident rebide boost and attack outlet permits main amplifier, etc., to
lee controlled by master switch. Complete
with preprinted punched chassis, all combonenis, tubes, cabinet and detailed instructions. Easy to assemble.

SPECIFICATIONS: 4 Input channels—1

SPECIFICATIONS: 4 Input channels—1 Low level-high gain, 3 III-Impedance. Tube Complement (1-12AX7, 1-12AU7). Size—103, '44" x 4". Shpg. wt. 4 lbs.

USE HANDY ORDER BLANK ON NEXT PAGE ▶



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MAILYOUR ORDER TODAY—OLSON WILL RUSH IT RIGHT AWAY!

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RA-112

SUPER BARGAIN!

OLSON

NO MORE WHEN THESE ARE GONE!



SPECIAL SALE! WILCOX-GAY RECORDIO TAPE RECORDER

2 Full Hours of Recording or Playback—Automatic—Foolproof Push-Button Controls • 2-Speeds •

Records . Plays Back . Erases

Records • Plays Back • Erases

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BRAND NEW

REGULAR

\$149.95

ONLY.

Automalically records from FM or AM radio, hionograph, TV or mike, Plays back through powerful fulli-line and plays and the record in the plays and the pl



RECORDING TAPE—FAMOUS MFR'S CLOSEOUT!

PLASTIC BASE

Stock No. X-249. Single eas, \$2.19 Lots of 10 cach...

Get the buy of your life. Save up to 64% on high quality RECORDING TAFE. A large maintacturer had to sell his action of the sell his high sell his high series of the sell his high series of the sell his high series of the sell his high sell h



ROLA 12" PM SPEAKER STOCK NO. S-174 \$ 495 single, each, \$5.95

Lots of 3

With Motching Output
Tronsformer for 6V6
Rola-a great name in Hi-Fidelityhas built these fine 12° Alnico 5
PM Speakers. Olson ellinched a deal
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usual wholesale price. Every Speaker
tures include a unique voice coil construction which maintains constant
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New design cone delivers all free
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former for 6V6 tube included. Look
at Olson's Low-Low Price! Shpg, wt.
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A MIRACLE in RESISTORS



KIT OF 130 NATIONAL RESISTORS 10% TOLERANCE

COMPLETE KIT \$366 Stack TO OF EACH SIZES ONLY No. AS-68 YOU GET 13 SIZES

A\$-68

Less than 3c each. You get 10 each of the following 13 popular values. OHMS: 10,000, 15,000, 22,000, 27,000, 47,000, 58,000, 100,000, 270,001, 330,000, 470,000. Miggs: 1,47, and 6,8. The degree of precision astoliuds experts. National lessistorial stoliuds experts. National lessistorial formation of the stories o



FREE! OLSON'S BIG NEW BARGAIN CATALOG

Get Olson's LOWER-than-wholesale prices from this famous book. STANDARD BRANDS-FRESH STOCK. IMMEDIATE DELIVERY. Catalog is two colors-40 full pages of unbelievable hargains. A new catalog malled Bi-Monthly-with new low bargains, A new catalog marter in anothry—with new low bargains each mailing. Simply note on order blank or write today for your free copy from: OLSON RADIO WAREHOUSE, 275 E. MARKET ST., AKRON 8, OHIO.

WANTED! \$500,000.00

WORTH OF Radio and TV Parta, Speakers, Transformers, Tubes, Picture Tubes, Condenkers, Resistors, Switches, Wire, Knobs, Colis, Phono Cartriliges, etc. ALSO Partally assembled or complete Radio, Amplifier and Television Chassis, ALSO Test Equipment, Record Players, Automatic Changers, Motors, Microphones, Tone Arms, Meters, Cable, Cablietts, Grille Cloth, Wire or Taylor.

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PHONE: JEfferson 9191 = 275 E. Market St., Akron 8, Ohio

CLEVELAND, OHIO

February, 1953

OLSON STORES TO SERVE YOU IN: CHICAGO, ILLINOIS

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these cities visit our Bargain Stores where
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OLSON HAS OVER 150,000 SATISFIED CUSTOMERS

COMPLETE: With Tubes, Loop An-tenna Es-cutcheon, Knobs, Etc. 12-TUBE AM-FM RADIO CHASSIS

BRAND NEW LATEST 1953 MODEL ESPEY

COMPLETE WITH

" MAGNAVOX SPEAKER

LOOK HOW YOU SAVE

12" Magnavox Speaker. .\$ 20.00 12 Tube AM-FM Chassis. 130.00

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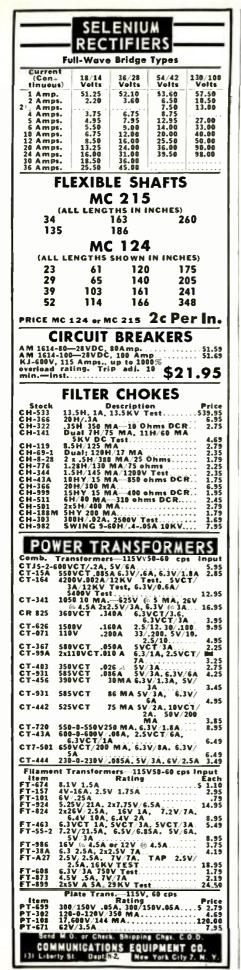
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Within the Industry

(Continued from page 26)

ALLEN H. CENTER, formerly public relations director for the Parker Pen Company, has joined the staff of Motorola, Inc. as public relations director . . . EUGENE M. KEYS has been elected to the post of executive vice-president, director of sales, and to the board of directors of the Edwin I. Guthman & Co., Inc. . . . EDWARD M. SHERIDAN has joined I.D.E.A., Inc. as industrial sales manager. He was formerly associated with RCA Victor Engineering Products Division for 10 years and was manager of the Product Analysis Section of the New Products Division prior to taking his new post . . . CLARK KEL-LEY is the new assistant service manager of Sparton Radio-Television of Jackson, Michigan . . . R. J. McCLUS-KER has been named assistant sales manager of the Westinghouse Television-Radio Division. He succeeds J. W. HITCHCOCK who resigned recently . . . Hycon Mfg. Company has appointed RAYMOND F. CRISP to the post of manager of technical services. He was formerly chief electronics engineer for the firm . . . ROLAND J. SHERWOOD, vice-president in charge of sales for the Hallicrafters Company, has resigned his post to organize his own business in an unrelated field . . . LEONARD F. CRAMER, assistant general manager of the Crosley Division, has been elected a vice-president of Arco. In his new post he will be in complete charge of Crosley's TV and radio activities . . . Raytheon Television and Radio Corporation has promoted JAMES R. BUTLER to the post of merchandising manager for the firm. He was formerly sales promotion manager . . . WIL-LIS E. CLEAVES has been named general sales manager of the Bendix Radio Communications Division of Bendix Aviation Corporation. He succeeds AR-NOLD ROSENBERG who has resigned . . . GAIUS WIKE is the new general sales manager of Utah Radio Products Co., Inc. of Huntington, Indiana. He succeeds FRED TOWER who has been promoted to division manager and vicepresident of the Caswell-Runyan Division of the firm . . . T. J. NEWCOMB, who has been with Westinghouse for more than 20 years, has been appointed manager of the company's Television-Radio Division with headquarters at Sunbury, Pa. . . . The promotion of HARRISON JOHNSTON to the position of general sales manager has been announced by the Ampex Electric Corporation of Redwood City, California . . . EDWARD P. ROBINSON has been named plant manager for the Espey Manufacturing Co., Inc. of New York. He has been with the firm since 1947 R. K. GILBERT has been appointed operation manager of the Chicago plants of Standard Coil Products Co., Inc. He was formerly associated with Philco Corporation for 16 years, serving in several important production capaciradio and television broadcasting sales fields, has been appointed assistant sales manager for JFD Manufacturing Company, Inc. MIKE MEYERS is the new chief field engineer for Radio Merchandise Sales, Inc.

JOHN B. OTTMAN, former advertising manager of Stewart-Warner's Electric



Division, has been appointed television-radio sales promotion manager for Admiral Corporation.

A native of New York City, Mr. Ottman is a graduate of Yale and the Har-

vard Graduate School of Business Administration. He served in the U.S. Air Force for three and a half years and joined *Stewart-Warner* in 1947.

NEDA will hold its 1953 convention and conference September 14, 15, and 16 at the Chase Hotel in St. Louis, Missouri, according to word received from the association's headquarters.

A departure from past meetings, this year's convention will eliminate booths for conference purposes and provide instead three large rooms on the first floor of the hotel for conferences. Each manufacturer will be allotted a table and several chairs for use in greeting and talking to distributors.

There will be no business or social functions of any kind during conference hours. Entertainment for each of the three evenings will be provided by each of the three groups attending; "The Reps," participating manufacturers, and NEDA.

Educational programs are scheduled for 10:00 to 11:30 a.m. each morning of the convention. Conference hours will be 1 p. m. to 6 p. m.

A.T. & T.'s Long Lines Department has announced the recent completion of two new links in its expanding telephone-television network.

The company has now connected Roanoke, Virginia into the nationwide television network.

The company also opened a new radio-relay link between Kansas City and Dallas. The new facility will provide 96 television circuits as well as one Kansas City-Dallas TV channel.

Network service is now available to 112 television stations in 69 cities in the U.S., as of December 15, 1952.

CAPT. HENRY J. ROUND, 1952 Armstrong Medal winner, recently received his award from the hands of John Bose, president of the Radio Club of America at the club's 43rd annual banquet.

The award was made in recognition of Capt. Round's pioneering work in radio. especially in the fields of radio direction and position finding and the high amplification of short-wave signals. Capt. Round is a native of England.

-30-

ties . . . MORT LESLIE, a veteran in the

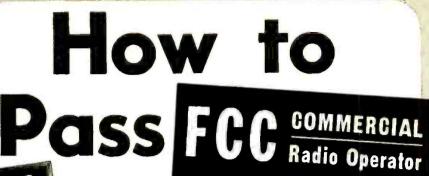
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Employers make

JOB OFFERS Like These to Our Graduates Every Month

Letter from Chief Engineer, Broadcast Station, North Carolina, "Need men with radio-telephone 1st class licenses, no experience necessary. Will learn more than at average station for we are equipped with Diesel Electric power, transmitting and studio equipment."

Telegram from Chief Engineer, Broadcast Station, Wyoming. "Please send latest list available first class operators. Have November 10th opening for two combo men."

These are just a few examples of the jab affers that come to our office periodically. Some licensed radiomen filled each of these jobs . . . it might have been you!

HERE'S PROOF FCC LICENSES Are OFTEN SE-CURED IN A FEW HOURS OF STUDY WITH OUR COACHING at HOME in SPARE TIME

Name and Address	License	Lesson
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22101/2 Wilshire St., Bakersfield, Calif.		
Clifford E. Vogt	1st Phone	20
Box 1016, Dania, Fla.	1st Phone	38
Francis X. Foerch 38 Beucler Pl., Bergenfield, N. J.	1st r none	30
S/Sgt. Ben H. Davis	1st Phone	28
317 North Roosevelt, Lebanon, III.	2nd Phone	23
110 West 11th St., Escondido, Calif.		

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Charles E. Loomis, 4516 Genessee Ave., Dayton 6, Ohio.

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"I have had half a dozen or so offers since I mailed some fifty of the two hundred employment applications your school forwarded me. I accepted a position with the Civil Aeronautics Administration as Malntenance Technician. Thank you very much for the fine cooperation and help your organization has given me in finding a job in the radio field."

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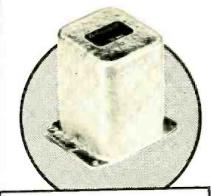
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February, 1953

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TV Sound System (Continued from page 55)

output transformer secondary. The volume control on the receiver can be used to vary the output of the amplifier. This method of connecting the receiver to the amplifier has many advantages over simply running a line to the high impedance input of an amplifier from, say, the hot side of the receiver's volume control. For one thing, there is little chance of hum pickup due to long high impedance lines, also there is no attenuation of the higher frequencies due to long runs of shielded wire which bypass the higher frequencies to ground.

For high impedance inputs, the grid of the 6SN7 is connected to an internal volume control and the cathode resistor R_2 is bypassed with a 25 μ fd. condenser, C_1 . The high impedance input is useful when it is desired to connect a record player attachment with a crystal pickup.

The speaker system used with this amplifier is shown in Fig. 3. It consists of an 8-inch, wide-range speaker mounted in a bass reflex enclosure. An 8-inch speaker was found to be a good compromise between the larger speakers, which require large enclosures, and smaller speakers which are not capable of adequate bass reproduction. A wide range 8-inch speaker, when properly baffled, is cap-

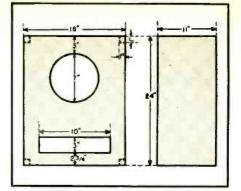


Fig. 3. Construction details for building the associated speaker enclosure. Cabinet should be constructed of %" plywood with corners braced with 1" x 1" blocks of wood.

able of excellent bass response, and the cone is small and rigid enough to reproduce the higher frequencies. The speaker system used by the writer showed remarkably smooth response throughout the audio range. Fig. 3 shows the dimensions of the bass reflex enclosure. The back, one side, and the top of the enclosure should be lined with suitable insulating material such as *Celotex* or rock wool. It should be rigidly constructed, the joints should be screwed and glued, and the back cover should be very tightly secured to the enclosure.

It is the writer's belief that anyone who constructs this amplifier-speaker combination will find it as useful and enjoyable as he did.

ELIMINATING BARKHAUSEN EFFECT

FROM the Service Department of Scott Radio Labs, Inc. of Chicago comes some useful tips on the causes and remedies of Barkhausen lines in the picture.

"Barkhausen lines are vertical black lines which run the full length of the screen. The lines usually are most prominent and occur more often in the left half of the CR tube screen when facing the front of the receiver. The lines shift and differ in intensity with each channel.

"Barkhausen ean occur in any re-eciver using a 6BQ6, 6CD6, 6BC6, or other similar horizontal output tubes used in modern television receivers. In such tubes an r.f. oscillation is set up between the screen and the plate due to rapid plate potential changes and emanates from the horizontal output tube as an r.f. signal. Physical characteristics of the tube determine the frequency of this oscillation to some degree. Some of the frequencies generated in the horizontal output tube fall within the TV spectrum and if allowed to enter the r.f. section of the receiver, they will appear visually as outlined above

"The built-in antenna will pick up this radiated signal, and whether or not the built-in antenna is used, it can feed or radiate the signal to the r.f. unit. In receivers where the built-in antenna is not used, it would be best to remove the antenna from the cabinet. The aquadag coating on the outside of the picture tube will also act as a radiator of this r.f. signal if not properly grounded. "In many receivers, the power cord terminates near the high voltage power box, and the power cord can pick up this signal and transmit it to the antenna leads, particularly where the antenna leads come from an outside antenna and then are allowed to be coiled on the floor in close association with the power lead. Often rearranging of the receiver line cord with reference to the incoming antenna leads will climinate Barkhausen oscillation.

"Within the receiver, moving of the piece of twin-lead from the tuner to the termination point at the rear of the chassis will often eliminate Barkhausen lines. Since horizontal output tubes radiate at different frequencies, the change of the horizontal output tube may either remove Barkhausen lines entirely or transfer them to a channel which is not in use. Also it would be advisable to try different damper tubes. In extremely difficult cases it may be necessary to attach a magnet to the horizontal output tube. Quite often an ion trap is slipped over the top of the horizontal output tube to eliminate Barkhausen radiation. Another possibility for the climination of Barkhausen is slight readjustment of the horizontal drive control. Check all tube shields on the tuner to make certain that they are properly grounded.

"Problems of Barkhausen climination are normally problems of installation and each set will show different characteristics and on each receiver lines will appear on different channels and in a different position on the CR sereen."



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183GT95	3LF41.19	6AV5GT89	6F 5 GT 59c	6SJ7GT. 54C	707	128 A7 69	SAYSGT 89	6C D6G 1.49	715 B
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1076 / 46	3Q5GT89	6A X 4	6F8G1.15	6SN7GT69	767	12 BF6 59C	6 B G 6 G 1.49	6V3 1.29	866 A / 1616
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IL A6	5W4 50r	6B A6	6J8G1.15	6T7G 1.15	717	12 J5GT	.54 14F8 1.	30 36	80
1L C5	5W4GT 33"	6BA7 690	6K5GT	6T8	7 K7 1.07	12K7GT /	19BG6G1.	19 37	94 674
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	6A8GT	6BG6G1.49	6L7	6W4GT	7w71.07	12SH7GT	69 25W4GT	69 452569	11726
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245 79	6AL5 COn		6SC7	7A8	12AT789	14A7	.89 35 W.4	45 7017	2051
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283 89	6AR5 74	6CR6 69	6SF5GT 59	786	12AV6	14B8 U	JU 1 35 Z4	9 1 / LA	I V 13/



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Model ARC-101-100 is a two stage
super high gain booster for the
most difficult reception areas.
Model ARC-101-75 a single stage
booster designed to give uniform
response on all channels. One knob control.

DEALERS-SERVICEMEN-MAKE MORE MONEY-GET ACQUAINTED with McGEE

28 WATT \$15000 LIST PORTABLE P. A. ON SALE \$6995 3-SPEED PHONO TOP-TWO 12-INCH SPEAKERS 7-TUBES PUSH PULL 6L6'S HEAVY LEATHERETTE

COVERED PLYWOOD PORTABLE CASES CRYSTAL MIKE \$8.95 EXTRA

CRYSTAL MIKE S8.95 EXTRA

STOCK No. AP-2RX. Portailse 28 wait public address system. You get a 7-tube heavy duty push-bull (1.6 anphiller with limits for 2 mikes either crystal or dynamic with separate mixing volume control high fidelity, while ranke frequency response. The heavy duty output transformer has taps for 4, 8, 18, 125, 25n and 500 ofm speaker connections. Two heavy duty 3 randle tone control high fidelity, while ranke frequency response. The heavy duty 12 fine intinto V P.M. speakers, and 500 ofm speaker connections. Two heavy duty 12 fine intinto V P.M. speakers can be a simple state of the speaker connections. Two heavy duty 12 fine intinto V P.M. speakers can as a simple speaker connection of the speaker connection of the

eNtra.

Floor type mike stand inslead of deak stand \$4.95 extra.

(SEE OFFERING TO THE RIGHT FOR WALL SPEAKERS INSTEAD OF THE PORTABLE SPEAKERS, P.A. system is offered with two of the 25 watt weatherproof trumpet and delvers No. MA-33 shown below: in place of the two portable speakers with buffles. Specify that you want MA-33 trumpets with your amplifier and add \$35.00 to the cost. Stock No. MA-28XX.

Not price \$104.95.

28-WATT AMPLIFIER WITH 12-INCH WALL SPEAKERS

shown to the left is also offered with out the port-able speakers



phono top with two 12 incl sheakers. 569.95. Extra 1 wall speakers 511.95. Mode Electro Voice mike 58.95 Floor stand 54.95 extra.

3 STATION INTERCOM MASTER \$16.95

3 STATION INTERCOME MASTER

SUB STATION \$3,95

3-station intercome master housed in chrome intered metal continued to the continued of the con





INTERCOM SUB STATIONS \$3.95

Chrome plated, with call back switch for a 3-wire intercommaster. Size 71½ "xt" x5" sloping front. 5" Alnico V PM spkr. Intercom dealers buy at less than present production c o s t x. Limited



BRUSH CRYSTAL EAR PHONE \$5.49

With Control

Simply clip on to the speaker voice coil of any radio or TV set or to an audio amplifier. No solderlist necessary, Listing and the speaker voice of the speaker voi



5-TUBE RADIO

WITH BRUSH EARPHONE PLUS REGULAR SPEAKER

Top quality lable model radio with Brush crystal earphane for private listening as well as the regular nearly duty 5" speaker. Beautiful cabinet available in lovory or walnut is constructed so that it has no open back, givelet with 128A7, 128N7, 128N7, 5016, and 33.75 rectifier tuie. Illuminated slide rule dial, linuar crystal caribone has 20 feet of cable and separate control back so that the volume can be resultated to still the Inspirate control back so that the volume can be resultated to still the Inspirate control back so that the volume can be resultated to still the Inspirate control back on the property of the private with a superior of the private with a superior control back of the private with such crystal carbinone. Stock No. 110-BH3, shipping weight 8 lbs. Sale price 521.95 in walnut finish. 50c extra for ivery cabinet.



CROSLEY RADIO

Charc. \$29.95

5 tube superhet radio (2.40 to 1600 ke Braid-cast) using 128A7.

128K7, 128Q7, 504L

129K7, 128Q7, 504L

139 tubes! Automatic changer for up to 8 45 RPM records (67% only). Brand new in original factory carlons. Only 100 to sell at the terrific low price of \$29.95. Shipped Express only. Shipping weight 23 las. Mahogany cahinet 13 x 16 x 81 x 18 k. Mahogany cahinet 13 x 16 x 81 x 18 k. Mahogany cahinet 13 x 16 x 81 x 18 k. Mahogany cahinet 13 x 16 x 81 x 18 k. Mahogany cahinet 13 x 16 x 81 x 18 k. Mahogany cahinet 13 x 16 x 81 x 18 k. Model No. 10-14 v. M. \$29.95.

OUTDOOR SPEAKERS — WALL BAFFLES — 50-WATT BOOSTER AMPLIFIER



25-Watt Weather-Proof Out-Door Speaker

\$28°5

8" PM AND LEATHER-ETTE BAFFLE, \$4.95 LOTS OF 10, \$4.75



The fluest Leatherette Baffle we have ever offered. New self-supporting plastic grill haterial, baffle is covered tan with material, baffle is covered tan with materials. Baffle is overed tan with materials of the peaker with 3.2 ohm volce cull. Stock No. 818. Steaker and liaffle, \$4.95 ct.; lots of 10. \$4.75.

8. Baffle only. Stock No. Nv-8. \$2.29 ct.; 10 \$6 \$19.55.



50-WATT BOOSTER AMP.

2-Mike Pre-Amp \$12.95 Extra. Not a Kit, but a Manufactured Amp.

50-WATT BOOSTER A

Onnect to your present amplifer as a boster of the booster of the present amplifer with the Pk-2X Pre-ample to shift the pk-2X Pre-ample the pk-2X

3-SPEED CHANGERS—FM-AM CHASSIS

ORDER FOR USE WITH ANY P.A. SYSTEM OFFERED ON McGEE'S 2 PAGES OF ADVERTISING 25-WATT HORN 100% weatherproof, horn in spun aluminum, offered to you at a considerable savings. Shippling weight 20 lbs. Net price 528.95.

IT'S McGEE FOR COAXIAL SPEAKERS

McGEE'S \$62.50 LIST 15" COAXIAL SPEAKER, \$21.95



This is the finest 13" coaxial SPEAKER, \$21.95
21 OZ. ALNIGO V MAGNET—5" TWEETER

This is the finest 13" coaxial PM speaker value that we have ever offered New 1952 production, of a famous manufacturer of fine speakers, New 1952 production, of a famous manufacturer of fine speakers, New 1952 production, of a famous manufacturer of fine speakers, New 1952 production, of a famous manufacturer of fine speakers, or speake

music lover's amplifier. Stock No. P15-CR, shipping weight 13 lbs. Net price 521.95. 12" JENSEN PM, \$15.95



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G.I. 3-SPEED CHANGER WITH G.E. \$2295 VARIABLE RELUCTANCE TURN-ABOUT CARTRIDGE

Another tremendous McGee Scoop: Brand new General Instrument 3-speed automatic record changers. Complete with RPE-050 G.E. very consistent of the Complete with RPE-050 G.E. very consistent of the Complete with RPE-050 G.E. very consistent with the Republic State of the Complete State of the Republic State of the Complete State of the Republic State of the Complete State of the Republic State o

ESPEY 12-TUBE FM-AM CHASSIS, \$59.95

- BUILT-IN PRE-AMP FOR G.E. VARIABLE RELUCTANCE PICK-UP
- * WIDE RANGE AUDIO
- WHY NOT ORDER WITH A COAX-IAL SPEAKER AND A RECORD CHANGER? SEE OUR SPECIAL OF-FERING

McGee's new 1953 model 12-tube FM-AM chassis, Latest design with phono inputs for all types of record players, crystal or G.E. variable reflectance, Receives standard broad-cast 550 to 1700 kc and FM 88 to 108 mc or for the first standard broad-cast 550 to 1700 kc and FM 88 to 108 mc or for first standard broad-cast and 300 ohm line type for for first standard broad-cast and 300 ohm line type FM antenna may be stapled in cabinet. Attractive lighted slide rule dial, Chassis size, 131 g x 9" high and 9" deep, Complete with tubes: 618 6, 618 6, 618 61, 12 A 77, 881 f. 31 g x 9", 6307, 6307, 12 A 77, 2 Fd Vigf and 5 Vigf rectifier. Shipping welche 20 his, Stock No. 7c-X Espey 12-tube FM-AM chassis, Sale price, \$59.95, less speaker. Output matches voice coil of our 12" or 15" chavital speakers.



ESPEY DEAL (1), \$99,95

Exper 7.0 chassis complete with 12" conxial PM speaker CU-14Y and VM-950 G.E. 3-speed changer equipped with a G.E. turnabout variable reluctance cartridge. A better home music system than ordinarily available. E. 8.9 c.With 15" conxial PM speaker P15-CR instead of CU-14Y, 510-00 extra.

ESPEY DEAL (2), \$118.95

EARLY UTAL (2), 318.95

EARRY 7-C chassis complete with 12" coaxial PM apeaker CU-14Y and the English Garrard 3-speed changer equipmed with a G.E. variable retuctance best home music system. Expey Deal 22. Sale price \$118.95. With 15" coaxial PM apeaker P13-CR instead of CU-14Y, \$10.00 extra.

ESPEY DEAL (3) \$138.95

Espey 7-C chassis complete with THIREE 12" constal PM speakers CU-14Y these three 12" coaxial papakers give a cone area equal to an 18" speaker and a Garrard 3-s p c e denanger with G.E. variable reluctance turnabout cartridge, Espey Deal 2-3, Sale price \$138.95.

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Prices F.O.B. K.C. Send 25% Deposit with Order, Balance Sent C.O.D. With Parcel Post Orders, Include Portage

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GENUINE STANDARD COIL T.V. BOOSTER Not Surplus. But Right From the Factory

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Latest Model B-51 Standard Coll Television Booster. McGee
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net. 8"k4\" x4\" y h Made for 110 voit. 6" cycle AC operation. S
Model B-51. Sale price. \$11.95 cach, or my 2 for only \$22.00.



\$11.95

sound. Has extremely for control switch for irk brown plastic cabi-shipping weight 5 lbs.

McMURDO SILVER BOOSTER \$10.95

Sensational value. Continuously variable inductance type tuner, frum channel 2. including the FM hand, through channel 13. This booster is self powered for 110 with xAC operation. Incorporates a 6.36 tube, input for 300 ohm TV line and 310 ohm output to the TV set. Single knot brings. Attractive plastic case, McMurdo-Silver Super Sonle TV-FM booster. Stock No. 611-618. Shipping weight 5 lbs. McGec's terrific sale price, \$10.95 cach, two for \$20.00.



CASCODE ASTATIC S19.10

New Astatic "Seanafar" TV booster with Improvements to match the newer model Treecivers. Minimum noise with maximum gain, Halanced esseaded circuit with a Tana and 12ATT. Insulational metal and 12ATT, Manugany initiated metal with with the control of the contro

DB-520 REGENCY \$19.10

20 INCH CONVERSION KIT \$29.95



YOU GET-20HP4-20" PICTURE TUBE **20-INCH PLASTIC MASK** 14 K.V. FLYBACK AND 70° YOKE

Our 20° conversion kit includes a 6-month guaranteed 201P4, 20° rectangular blackface picture tube, plus a 14,000 volt G.E. huilt high voltage flyback transformer, plus a matched 70° cosine yoke, plus a 20° rectangular gold trimmed plexiglas mask und suggested diagram. The picture tube is the latest electro-static focus type that requires no focus coil. Shipped via express or truck only. Ship, weight, 40 lbs. Stock No. 20-TP, net price, \$29.95.

Our 14" conversion kit includes an RCA 14CP4, 14" rectangular blackface tube, plus a 14,000 volt G.E. built flysack, plus a 70 cosine Yoke, plus a 14" plexiflas gold trimmed mask, Offered at the very line price of only \$19.95. Suggrested diagram furnished. Ship, weight, 20 lbs. Vla express or truck only. Stock No. RC-14X, net brice. \$19.95.

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Our 17" conversion kit includes a fi-month our art to the plus a g. f., bullt 14,000 with the hock, plus a matched 71" cusine yoke, plus a gold trimmed 17" plesiglas mask, and suggested diagram. The 171114 is the largest electro-static focus unde that resultes no focus cell. Shiphoet via express or truck only, Stock No. 17-TP4. Net brice, \$24.95.

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g Flylands and 3 belicetion Yokes for 59.95. Yok and 1-55° yoke, and 3 horizontal flylack ransformers. 2 General Electric 14.000 Your terainte core 70°, and 1 carly model philico. The flylack ransformers and 1 carly model philico. The flylack ransformers of the flylack No. 331 K. ship, weight, 5 lbs. Radio News Special, only \$9.95.

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liere is a terrific TV harts deal for those
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plus a standard 4-wire vertical output transformer. Plus : 70° coulse deflection yake
(no tubes included). It's worth \$20.00. Our
special pilec only \$12.95.

4 General Electric Diodes for \$1.95 Reg. \$7.20 Nct



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2-1N48, 1-1N52 and 1-1N63) only \$1.95
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RCA 201E1 T.V. TUNER \$7.95

Terrific buy on this RCA tuner. We have a limited quantity of the famous original 201E1. 13 channel completely wired and tested TV front end tuners. Ready to connect to your TV video 1.P. strip. Offered at a sacrifice. Price was \$44.00. Now only \$7.95 each, with tubes. Each tuner in good condition but has been repaired. Stock No. RCA-13P. TV front end tuner. Convertor coll type for separate sound as used in the famous 630 chassis. Complete with 3-636 tubes. \$7.95. Specify shaft length desired, either 2" or 4".

RCA 201E-1 T.V. TUNER
Same as pictured above only new-with tubes. Stock No. 2201. Sale Price. \$11.95.

3-TUBE SARKES-TARZIAN T.V. TUNER

This popular Sarkes-Tarzian Type 3 tuner is widely used. 13 channel rotary type switch with individually tuned colls. Price is comblete with diagram and three tubes: 6C4 oac. 6BH6 R.F. and 6AG5 mixer. Regular factory cost is twice our price. Each tuner is wired ready to hook up to a video and sound to receive the control of the contro



RCA PRINTED CIRCUIT T.V. TUNER \$14.95

RCA Printed Circuit T.V. Tuner with 6.16 and 6CB6 tubes. Similar mechanically to the standard coll (saine knobs Btt. Snap-in channel segments. Has 61½" shaft. Used on lafe Hallerafters T.V. sets. Stock No. RC-812. 12 Channel Tuner with Tubes. New. \$14.95. Knobs. 59c.



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For Emerson 650D ETC. Has 2¼" insulated shaft and tubes 6BC5—
niaments in series—shunted to .6 amps. Stock No. SC-947E. Sale Price, \$12.95. Knobs. 59c.

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Originally Intended for an Admiral 14° TV combination. Made of walnut veneer, 32° wide, 33.5%° high and 20° deep, Offered at less than the factory produce of the control o

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Beautiful these quality wainut or Mahogany
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AND AMPLIFIER KITS AT McGEE COMPLETE RADIO, TELEVISION 10-TUBE RADIO KIT \$29.95

3-WAY PORTABLE KIT \$1595



A NEW '52 MODEL

A NEW '52 MODEL

New 1952 Model 3-way

Personal portable radio

k it. Operates on 110

Puls 11/2 voit self-contained batterles.

Leatherette covered of the 16 of 87 kg. A

conventional 2-gang superhet circuit with

456 KC fron core 19's. Incorporates the

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Indicate drassia. La, approved circuit with

matched parts. After V PM speaker. A

factory quality kit. Stock No. PN-4T. ship
ping weight 7 lbs. The complete kit. Less

batterles. \$15.95. 071/2 v B, \$1.59; 11/2 v A, 39c extra.

Build Your Own 5795 arrie

Phono-Mike
Broadcaster
Kit Model DE-6R. With
this simple kit with the strength of the strength

8-Tube Hi-Fi Amplifier Kit \$29.95



10-Watt Hi-Fi Amplifier Kit \$14.95



10 tube 2.68K7.



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17, 20" T.V. Kit \$59.95 Less Tubes



6-TUBE 2-BAND KIT \$14.95



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Model RS-5. A 5 tube AC-DC straight broaderst kit, housed in the same cabinet as MEG-2 above. Complete with tubes. Ship-bing weight 10 lbs., Net \$12.95.

AC POWERED BROADCAST TUNER KIT \$12.95

A self-powered. 3-gang superhet tuter kit with R.F. stage. This complete kit is furnished with a diagram, photos and tubes. 6BAG R.F., 6BEG oscillator



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PRICES SLASHED! SAVE BIG MONEY ON CRT-TV TUBES

All tubes in Penn Tube Cartons. Code dated of current date.

Standard R.M.A. Guarantee.

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ALL OTHER TYPES AVAILABLE

70° DEFLECT. YOKES \$195

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PENN TUBE COMPANY

Radio and Television Tubes 3547 MONTROSE CHICAGO 18, ILLINOIS

"Ultra-Linear" Amplifier

(Continued from page 45)

20 eps to 20 ke, within much less than .1 db. Maximum phase shift over this band is about 3 degrees.

The very wide frequency band and low phase shift permit excellent transient response as attested by the square wave oscillograms of Fig. 7. The slight ringing visible on the high frequency square waves could be removed by introducing roll-off in the circuit above 100 kc. This expedient, however, would lessen the steep rise and round the upper left-hand corner. The designer always has to compromise between damping of the square wave and loss of high frequency response. In this circuit, the Williamson principle of maximum bandpass was preserved, and the resulting square wave is still better damped than that of most other high quality equipment.

Those who have actually tested amplifiers with square waves on scopes capable of showing details of the performance without distortion, will appreciate the extremely short rise time and rectangular corners of these oscillograms.

The transient response of the circuit undoubtedly makes a substantial contribution to its listening quality.

Listening Tests

Many AB listening tests have been made comparing the "ultra-linear" Williamson with the triode Williamson and with other circuits. A variety of speakers and speaker systems have been utilized in these tests, and many different program sources have been included. Results were almost invariably the same—the "ultra-linear" circuit was accepted as the most realistic. On bass passages, drum rolls, and musical climaxes, the ability of the circuit to handle large power without distortion and with no tendency to transient instability shows up to advantage

At the high-frenquency end of the spectrum, the low phase shift maintains the correct harmonic structure of complex transients; and the percussive sounds of triangles, cymbals, tambourines, and other instruments come through with a naturalness and crystal clarity which is audibly evident to the untrained ear. String instruments have the natural "gutty" quality; and with a high grade speaker, it is possible to differentiate between the metal "E" string of the violin and the gut "A" string even

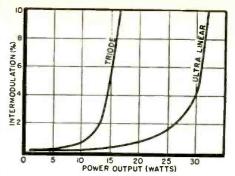


Fig. 4. Intermodulation distortion for triode and "ultra-linear" operation at 40 and 2000 cps mixed in a 4 to 1 ratio.

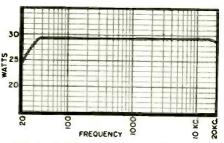


Fig. 5. Undistorted power vs. frequency.

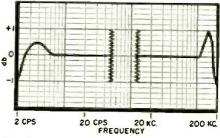


Fig. 6. Frequency response of the amplifier.

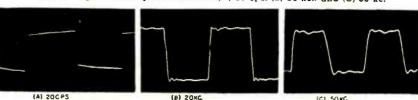
though a tone of the same frequency may be played on either.

The scratch of phonograph records is less noticeable and less irritating on the "ultra-linear" Williamson than on other amplifiers. Scratch and noise have a high transient energy content and tend to intermodulate with high frequency signals if the amplifier cannot handle considerable power at the high-frequency end of the musical spectrum.

The low intermodulation content of the amplifier is evident in the crisp definition of the music. There is no blurring, no shrieking. The slip of the violin bow against the bridge, the breathing of the singer, the cough in the audience; all are audible while the music plays. The various instruments are distinguishable individually rather than as a conglomeration of sound.

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Fig. 7. Square-wave performance at (A) 20 cps. (B) 20 kc., and (C) 50 kc.





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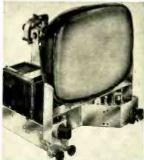


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pability of the "ultra-linear" Williamson shows up to audible advantage. The newest LP records, tape, and live FM cover very broad dynamic ranges, and it takes power to do them justice. The ten-watt amplifier cannot reproduce the climaxes of today's program sources, as is evidenced by comparison with a higher power unit such as the "ultra-linear" Williamson. New developments in program sources are forcing new ideas in amplifiers.

For some applications, even higher powers may be required. Just as can be done with the triode Williamson, the "ultra-linear" circuit can be operated in push-pull parallel, and the performance specifications can be maintained within a 60-watt rating. Experimental work is also being carried out with high power transmitting tubes to investigate the feasibility of using the same circuit arrangement in amplifiers of more than 100-watt capacity

Thus the "ultra-linear" Williamson circuit offers a distinct improvement over the original. It also offers the possibility of still further extension into the higher power ranges.

Many articles have appeared which describe amplifiers in terms of "best we ever heard." Such descriptions do not furnish a basis for the reader to judge the quality of the circuit. In this article the authors have attempted to provide the theoretical justification for an improved amplifier circuit. Theory and specifications cannot substitute for the listening tests which, in the end, are the only ones which count. The dubious reader, therefore, will wait until he hears it before accepting the "ultra-linear" Williamson as the best around. However, when he does hear it, he will find that, to coin a phrase, "hearing is believing."

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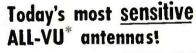
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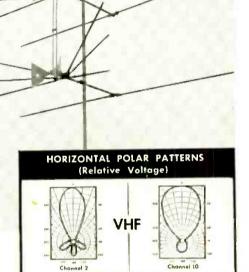
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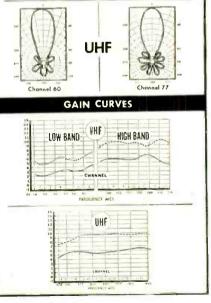


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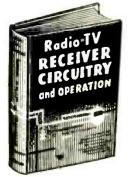
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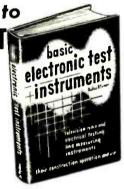
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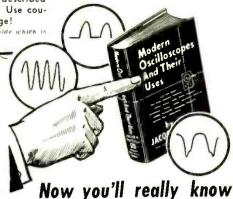
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RADIO-TV Service Industry News

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PRODUCTION for the defense program is supposed to reach its plateau, or peak, in the electronics industry during the months just ahead. It is expected, with the slackening of the demand for critical materials for military needs, expanding supplies of raw materials available for normal channels will rapidly stimulate the development and production of products for civilian use. The allocation and procurement of supplies for the defense program has preceded production by many months so it can be assumed that the flow of material into normal channels of trade will be noticeable even while production for defense stays at a high level.

An Expanding Industry

The electronics industry has been straining at the leash for a long time and the slackening of the pressure for war goods will be followed immediately by the rapid expansion of the industry in several directions. The applications of electronic devices to new tasks mean more complex circuitry with the result that maintenance is demanding a higher degree of training and competence on the part of personnel employed in that phase of the work. It is well worth careful study of what lies in the immediate future to appraise what the up-coming developments may mean to independent service as a business activity.

When television first burst upon the scene in 1947 it found the independent service forces of that day poorly prepared to cope with the new problems it presented. Almost every radio service operator in business at that time jumped into the "bonanza" of contract service for installing and servicing TV receivers. Most of the men who had had good radio service business expanded their activities to handle the sale of TV sets. In the intervening years many of these men have built substantial radio and appliance retail businesses with TV installation and service as a profit producing department.

Very few of the former radio service operators survived as TV service contractors. During the summer of 1951 alone the mortality rate in in-

dependent TV service businesses was close to 20%. In other words, about one out of every five independent service businesses ceased to exist during the six-month period in 1951 when the business of TV servicing hit rock bottom. We have heard of only a few TV service businesses that did not operate at a loss during the two summer months of that year.

Facts of Service Business Operation

The TV service business has been experiencing a small scale "boom" that started with the national political conventions last July. However, only a very small percentage of the independent service businesses have been able, during this period, to build up adequate cash reserves to tide them over the slack periods that are sure to come. This factor will bring about another period of high mortality when the cycle dips again to low business levels for a few months.

In traveling about the country on lecture tours your editors talk to many parts distributors about the caliber of service businesses they have in their trade areas. One of the most common remarks we hear is crystalized in this statement:

"Bill Jones (a neutral name we have selected) could have the leading and most profitable business in this area. He is a good technician; he gets along well with his customers and he tries to maintain a good credit standing.

"But the trouble with Bill is his business is under-capitalized. The result is he hasn't been able to expand enough to handle the volume of business necessary during good times to build adequate reserves to tide him over bad times. So when business gets bad Bill goes into debt to keep going. When business improves it takes him months to pull himself out of debt. He isn't building a business. He merely has a job working for himself in which he is not building any future security for himself or his family."

Then they will point to some other service business in which the owner is not an especially good technician but he is a good enough business man to keep a large enough volume of business coming in so that he can

hire competent men to handle the technical end of his business. He is able to give his attention to sales promotions that keep a steady volume of business coming in, to a regular and careful study of costs, and the planning of work routines and all of the other elements that are involved in running the business so it will produce a profit as well as a good income for the owner. That is the kind of business, they say, that will survive the long pull.

Classifications of Service Work

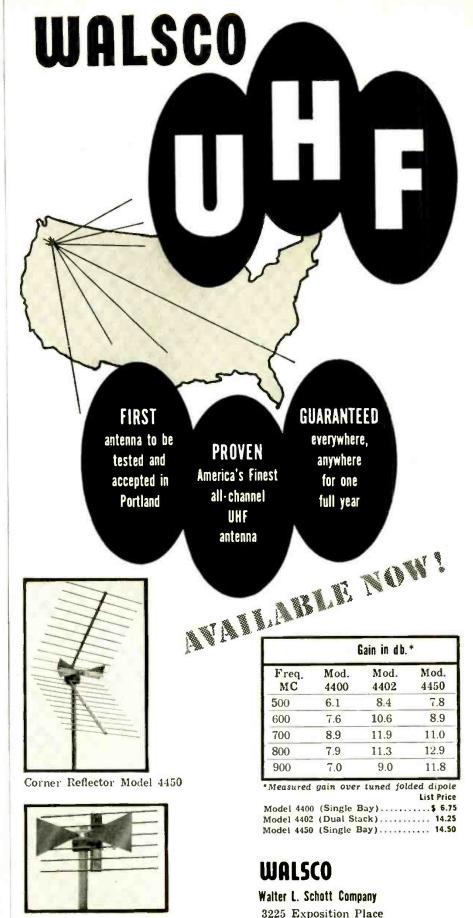
The many millions of AM radios that are either in use or sitting inoperative in closets, constitute a pretty good market for service in themselves. In TV areas, AM radio servicing has been taken over pretty much by TV service companies and the small shops that handle some minor TV service. As a rule, very little service sales attention is being given to the large number of AM radios that are in need of service. The AM radio repair jobs that come into shops are usually "emergency" jobs. The one that gets repaired is probably the last of several AM radios to finally quit working in that home. Chances are if the service operator who got the repair job would make the effort he could get two or three other AM radios to repair out of the home where the "emergency" job

Recently we mentioned this to a parts distributor who immediately cited what a service operator had told him the day before. This service operator delivered a TV set which he had repaired to the customer's home. As the customer paid him she said, "Will you take our four regular radios to your shop and repair them, too?" These "four regular radios" were a console and three table models—all inoperative.

There has been very little aggressive effort on the part of the service industry to get some of the available business on automatic changer replacements and on record player repairs. In many TV areas set owners are taking a new interest in recorded music. Lots of people who still have single-speed changers in their AM console cabinets that they like as furniture pieces, do not know that they can buy 3-speed changers that would fit into their console cabinets. While it would take some "personal selling" to do it, any radio or TV service operator who needs to increase his volume of business could do it with a campaign on replacing single-speed changers with 3-speed units.

The phono crystal cartridge and needle replacements have been sorely neglected, too. Perhaps it is because technically trained people think only in terms of technical proficiency required of an electronic device and not about how to sell their services to the people who own those devices.

The average person is prone to procrastinate in having things repaired.



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Vacuum cleaners stand idle in closets because the housewife puts off getting a new bag to replace the one worn out. Faucets drip because the old man forgets to get new washers until the old ones finally give way completely and the water pours out in a steady stream. Automatic record players gather cobwebs because the needle is worn out or the tripping mechanism gets out of whack,

One case in particular that recently came to our attention is typical of user indolence in having equipment repaired. This family had four AM radios; one in the kitchen, a console in the living room, and table models in each of two bedrooms. When the kitchen radio went out the housewife set it aside with a firm resolve to have it fixed right away and, in the meantime, she put one of the bedroom radios in the kitchen. The bedroom radio went on the fritz so it was set aside to be repaired, the family depending on the radios in the kitchen and living room for their radio listening. Then the substitute set in the kitchen went out, so they relied on the living room radio. Finally the last of their radios started to "act up" so the husband resurrected the first kitchen radio, took it to a radio shop and had it repaired. At last report they were doing all of their radio listening over the repaired kitchen radio. The radio service operator who repaired this set could have had three others to repair if he had been either curious or alert when he dealt with this customer

The TV service technicians who have called at this home to service the television set have never inquired about their AM radios, record changers, or hattery radios. Yet an itinerant grinder picks up about ten dollars each year on his regular annual calls at this home, for sharpening all of the knives and scissors on the place.

TV Servicing

The tremendous dollar volume of business that will continue to flow from TV service and replacements eventually will result in the development of basic types of business operations to handle it economically and profitably. Most TV service businesses are haphazard operations as husinesses that are hopelessly swamped when business is good and desolate when it is bad. The TV service contract was so badly abused by some customers' impossible demands for service and by the misguided, mishandling of funds by many service businesses that its usefulness as a medium to level off service revenue to insure year-round operation was destroyed.

Right now the TV service business generally is very good. Yet many service operators are badly under-pricing their labor. Many service operators who are handling a lot of money from their service activities are confusing the volume of dollars they are handling as "earnings". They are not



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CARTER Type B-420 SUPER DYNAMOTOR

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400 mfd @ 450 volts. equiva-lent to 400 watts seconds. All brand new. but removed from quantity at this sheelal price. STECIAL. \$5.95

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PHILCO Pri. 115v. 50-60 cy. Sec. 650v c.t. @ mils. 6.5v @ 4.5 amps: 6.3v @ .3 amps: 5v amps. Balf-shell mig. Shpg. wt. 9 lbs. itelleced to

RCA Pri. 113v. 50-60 cy. Sec. 750v c.t. @ 225 mils: 6.3v @ 8 amps: 6.3v @ 1.2 amps; 5v @ 3 amps. Half-shell mtg. Shrg. wt. 13 lbs. Reduced to \$5.99

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RCA 12" SPEAKER Ideal for replacement or new set use. 6.8 ohm voice coil. \$3.85 SPECIAL \$11.00 ROLA 8" SPEAKER

RULA 0 STEARLE (Sentine 18 of 18 of

ROLA 5" SPEAKER

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Complete with output transformer.
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4 For	4.75
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amortizing their test equipment, trucks, or any of the capital equipment that is wearing out. Most of them have no system of books whatsoever. Some of them insist they are making a lot of money on service at three dollars per call!

The "TSA News" (Detroit) recently carried an article by C. T. Wycoff which included an interesting breakdown of the cost of a service call:

"Many people think of television service calls at \$5.00 per call for half an hour or less, robbery, not realizing the costs involved.

"Let's break down the cost of a call. In a large city the maximum calls that a technician can complete in one day is seven calls in eight hours; the average mileage required per call is eight miles. 7 calls in 8 hours is one and 18 hours per call.

int & nours per carr.	
1 and 1/8 hours at \$2.00 per	
hour (low for professional	
labor)	\$2.25
8 miles at 9 cents per mile	
(replacement costs of car) .	.72
Supervision and management	
(someone has to run the	
business)	.83
Clerical and bookkeeping	.83
Overhead, rent, light, heat,	
& miscellaneous	.41

Total cost

"These figures are those of a typical service organization and do not figure in the costs of social security, workman compensation, call backs, or jobs guaranteed, etc."

Many service technicians believe that city or state licensing would answer the problems of independent service business operation. Actually, any form of licensing will eventually drive the small operator out of business. Where reports, inspections, and the payment of fees to political elements become a requirement for a man to operate a business, the red tape that develops demands so much time and attention that it becomes impossible to operate in a small way. Larger business units take over and through their volume of business they are able to afford the specialized help necessary to look after the non-productive phases of the business.

In most areas where licensing bills have been proposed the excuse is that "gyp" service technicians are gouging the public and giving inferior service. Yet in those same areas you will find successful TV service businesses that are being operated at a profit and have a high rate of customer satisfaction with the services they are giving and the prices they are charging. These businesses do not sell cheap service. They sell quality service. They are managed by men who realize that TV owners cannot truly appraise the value of good service. It is the responsibility and obligation of the servicing company to tell them about good service and what it rightfully costs. So they carry on regular customer relations programs as a part of every service call.

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FREQUENCY MODULATION PHONOGRAPH PICKUP SYSTEM



REALISM without "NOISE



- - **Extended Record and Stylus Life**
- **Negligible Distortion**
- Negligible Needle Talk
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- No Hum From Motor Field
- Triple Play Single Stylus Model Plays ALL Records

NEW! Weathers Reproducer Arm for the W-2 FM Capacitance (For Standard W-2 **Pickup** Cartridge Only) W-216 Arm and W-202 Cartridge

Protect your investment in new records with the one gram stylus pressure of the Weathers cartridge and arm. You will be amazed at the reduction in stylus wear. A new standard in record reproduction which must be heard to be fully appreciated.
The low mass of the Weathers stylus follows every groove undulation perfectly without distorting the groove wall.

- 5 CYCLES PER SECOND

Set for any 16" transcription turntable

Typical frequency response curve produced with Cook Series 10 Test Record, (Response over 500 cycles compensated to obtain constant velocity characteristic.) Terminals provide compensation based on AES Standard Playback Curve or constant-amplitude response, as preferred

SIMPLE INSTALLATION COMPONENTS

Each cartridge, or cartridge and arm set, includes a Weathers oscillator with pickup eable receptacle and power cable for one 6AT6 tube. Power cable may be connected to user's amplifier (receptacle supplied) or to Weathers W-22 Power Supply, sold separately. The new W-21A oscillator is factory-adjusted with the cartridge and pickup cable in each set and does not ordinarily require further adjustment, even after tube replacement.



CARTRIDGE FOR STANDARD RECORD PLAYERS

The W-202-C Universal Cartridge Set is available for installation in modern record players, manual and automatic, and in standard makes of transcription arms. Stylus pressure may be adjusted to 3 grams or less when installed in a Webster automatic changer or RCA-45 record player. W-202-C Universal Cartridge Set is electrically identical with the W-202 and W-212 Standard Set (used only with the Weathers arm), but the stylus compliance is slightly reduced.

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ENTER BOTH RADIO AND TELEVISION 12 months or one-third of the B. S. degree course (Electronics major)—also brings you the Radio Technician's certificate. An added 6-month course qualifies you for the Radio-TV Technician's certificate. Recent develop-Recent developments open unlimited opportunities for TV technicians and engineers.

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Conditioning: A	cating. Refrigeration, Ai echanical Engineering, B. 8 tory; Television Service,
Name.	Age
Name	Age
	Zone State

Any service technician who feels that licensing would answer any of his problems would do well to talk to any one-store drug store owner. Just ask him to tell you how many licenses he must carry and what they entail in record keeping alone. It will provide part of the answer why large drug chains are gradually pushing the small, one-man drug store out of busi-

Cheap Service or Good Service?

Recently in looking over a community newspaper we noticed the classified section carried three ads offering TV service. One ad listed TV service calls at \$3.00 and gave only the phone number; the second ad listed TV service calls at \$4.00 and gave only the phone number; the third ad offered TV service calls at \$4.50, included the name and address of the advertiser and a brief, professionally-phrased statement about the technical qualifications of the business.

After considerable checking we found the \$3.00 service calls were offered by a man who worked in a factory and handled TV service calls nights and on week-ends; the second was a radio technician who was trying to get some TV service business; and the third was a highly competent TV service company with an almost perfect record of customer satisfaction. The first two were equipped to handle only the simplest forms of TV service work, such as the replacement of receiving type tubes. The TV service company was equipped and manned to handle any type of installation or

On the basis of the information we were able to gather, the third company, advertising calls at \$4.50 with company identity included in the ad, is getting about three times as many calls from its ad as the first two combined. It again bears out the statement that TV set owners want to feel that they get full value for the money they pay out for TV service but they do not want cheap service. They want competent, reliable service.

Industrial Electronics

Most electronic devices for industrial applications are either custombuilt for the particular operation they perform or are adapted to suit the individual requirements of an installation. Because of those factors the sale of industrial electronics equipment is usually made on the basis of recommendations and specs developed from an engineering study of the function the equipment is to accomplish. Since most of this equipment has been going into large plants, they usually set up their own maintenance departments to install and service it.

However, the easing of the defense program will probably be closely followed by an expansion of the development of electronic control devices for use in smaller plants. This will open a new market for competent independent service.

Make Your Dollar Go Farther!

The father of our country made a dollar go a long way, but your dollar will go a longer way when you get a Walter Ashe "Surprise" Trade-In.

IS THAT
RIGHT,
OLE TIMER?

IT'S THE TRUTH.

JUNIOR. IT'S PROVEN

EVERY DAY AT

WALTER ASHE BY

THE CONSTANTLY

GROWING AMOUNT

OF REPEAT BUSINESS





JOHNSON VIKING II TRANSMITTER KIT. Complete with tubes. Shpg. wt. 85 lbs. Only \$279.50 JOHNSON VIKING II Wired and tested. Only \$336.50 There's no doubt about it—you're money ahead when you take advantage of the one and only "Surprise" Trade-In Allowance on your used (factory-built) test and communication equipment. For fast action, use the convenient coupon to tell us what you have to trade and to indicate your choice in new equipment. Get your trade-in deal working today!



NEW COLLINS 75A-3
RECEIVER. Complete with
tubes and 3 kc Mechanical Filter. Less speaker.
Only \$530.00.

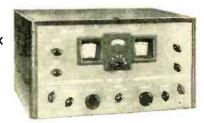
NATIONAL HRO-60T Less spkr. Shpg. wt. 90 lbs. Only \$483.50



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HALLICRAFTERS SX-71 Less speaker. Shpg. wt. 51 lbs. Only \$224.50 HAMMARLUND HQ-129X Less speaker. Shpg. wt. 74 lbs. Only \$239.50



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Manufacturers of electronics equipment for industrial and commercial applications have indicated they would prefer to deal with a single organization that could insure adequate maintenance and servicing facilities in all parts of the country rather than to have to ferret out competent organizations on an individual basis.

In order to provide these manufacturers with a national servicing "package" of independent servicing companies a group of major service businesses recently formed the National Industrial Electronics Service Affiliates, as incorporated organization whose aim it is to tie together in a cooperative program the leading service companies in every town, city, and hamlet across the nation.

It is the objective of NIESA to provide manufacturers with a service that will include the preparation of the necessary operating, installation, maintenance, and servicing information that its affiliates will need to efficiently handle the manufacturer's products

Major service companies who are interested in receiving detailed information on NIESA may write to the Service News Editor, RADIO & TELE-VISION NEWS, 366 Madison Ave., New York 17, N. Y.

Industrial Television

While u.h.f. TV and the new v.h.f. stations that are building in areas not previously served by local or nearby telecasting stations will bring an increased volume of business to many service shops in those areas, the next big "national" boost the independent service industry will get will come from industrial or "closed circuit" television.

The needed elements to get wired television underway on a large scale are now available. There is a comparatively low-priced camera tube built into a compact, easy-to-use camera. Such cameras are now in production. Extensive advertising and sales promotion campaigns will soon be "breaking" that will create a widening interest in this newest phase

The Dage TV camera, now in pro-

duction, is a compact, completely selfcontained unit about the size of a large brief case. It develops a 525-line picture with interlaced scanning so it will work into any standard television receiver. It is simple to adjust and operate. An installation consists of running a cable from the camera to the receiver or receivers to be used.

The Dage camera is to be sold through regular parts distributing channels and it is planned to leave the installation and servicing in the hands of competent independent servicing companies. It is presumed, of course, that progressive TV service companies will arrange for some of their technical personnel to study TV camera cir-

Many service technicians are now studying TV camera circuitry through a ten-lesson course prepared by the Television Technicians Lecture Bureau. The pulse generator, constructed as a part of the course for use with the TTLB camera, is a very useful servicing tool in itself.

The TTLB course includes complete construction details for a camera. All parts for this inexpensive unit are available from parts distributor. Information on the TTLB course may be obtained by writing to the Service News Editor, RADIO & TELEVISION News, 366 Madison Ave., New York 17, N. Y.

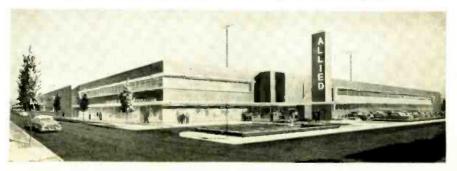
WESTERN SHOW DATES

HE Board of Directors of the Western Electronic Show and Convention (WESCON) has set the 1953 conclave for August 19 through 21 at San Francisco's Municipal Auditorium.

In 1952, a total of 15,092 individuals attended WESCON in Long Beach, California and plans for 1953 envision a substantial increase, not only in general attendance, but also in the 1952 figure of 2692 persons who registered for the technical sessions and the 199 ex-hibitors who displayed products and services in 224 booths.

WESCON, as an operating organization, is jointly sponsored by the West Coast Electronic Manufacturer's Assn. and the Seventh Region of the Institute of Radio Engineers. NEDA and the California Chapter of "The Represen-tatives" have pledged their cooperation.

Allied Radio Corporation, one of the leading national distributors of electronic parts and equipment, is building a new \$2,000,000 home at Washington Blvd, and Western Avenue in Chicago. The new location will give the firm 150,000 square feet of floor area in which to handle an anticipated 25.000 items. A system of conveyor belts, chutes, and electronic controls will move orders and merchandise quickly from one section to another. The building is expected to be ready by summer.



Mac's Service Shop (Continued from page 64)

versed from a positive to a negative. He moved the dial a little farther, and the picture returned to normal but the sound was blotted out.

"As you can see," Mac continued, "the grid-dip oscillator is a powerful little signal generator that covers, with the coils that come with it, a range of 2 to 250 megacycles. I have wound additional coils that allow me to go down to 350 kilocycles for use in radio servicing. The one I am plugging in now covers most of the broadcast band. Note when I flip this little switch on the back of the instrument the grid current falls to zero, for I am cutting off the plate voltage; but also notice when I bring the inductance close to the oscillator coil of this little a.c.-d.c. set and tune the instrument to the frequency at which the set oscillator is working, I get a reading on the meter. The grid of the 6AF4 is now acting as the plate of a diode and is rectifying the voltage induced into the plug-in inductance. That gives a means of determining the frequency of any oscillator or other circuit handling a substantial amount of r.f. power. Furthermore, by noting the amount of coupling and the reading of the meter, I can get a rough idea of the amount of r.f. energy present in the circuit being investigated.

'And now," Mac continued as he plugged a pair of phones into the jack of the GDO and switched its plate power back on, "there remains but one more basic function of the grid-dipper to demonstrate. Listen in here while I tune the signal generator across the frequency at which the oscillator is working. Hear that heterodyne? Now we are using the instrument as an oscillating detector, and it provides us with still another method of determining the frequency of an unknown signal when that signal is too weak to give a reading on the rectifying-diode

"These coils you wound have three connections on them. Why?"

"The Colpitts circuit employing a split-stator tuning condenser as the sole 'capacity-voltage-divider' for providing feedback does not work well at low frequencies, especially when the tuning condenser approaches the allout position. I simply wound my coils in two equal portions and brought out the center tap and grounded it through an extra pin-jack on the frame of the tuning condenser. In effect, this changes the oscillator from a Colpitts to a Hartley; and then the low-frequency, home-made coils work just as well as the ones that come with the instrument. Now that technicians are buying the grid-dippers, I am sure that soon low frequency coils will be sold with them as standard equipment."

Barney picked up a little air-wound coil with a pair of alligator clips fas**UHF-VHF** Signal Testing is QUICK, EASY with...

> THE NEW HEAVY DUTY

EREC-TOWER

TEST SIGNALS UP TO 80 FT.

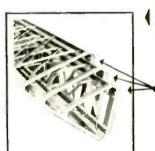
EREC-TOWER - and only EREC-TOWER - goes up a full 80 feet. You test signal strength anywhere along the way up . . . determine just exactly how high the permanent antenna must be!

ERECT PERMANENT TV TOWERS

Use the EREC-TOWER as a gin pole to raise permanent antenna towers. With an EREC-TOWER, for example, two men can erect a 100-foot Alprodco Tower in less than two hours. You save time, money, labor on every job!

DEMONSTRATE TV SETS

EREC-TOWER helps you demonstrate sets quickly, anywhere. Here's the ideal way to show razor-sharp pictures to your fringe area prospects . . . right in their own homes. EREC-TOWER is a real sales closer!



RETUEN BUILT

FREC. TOWER is constructed of lifetime aircraft aluminum. Each leg and track (see opposite illustration) is extruded in one solid 24-foot length . . , will not buckle, crack, stick or rust.

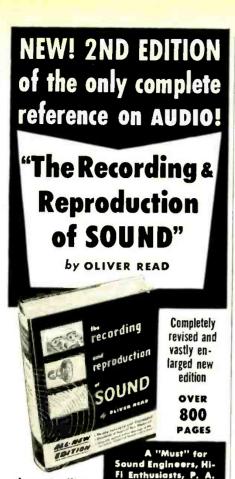
HEAVY EXTRUDED ONE-PIECE ALUMINUM TRACKS

> **Net Price** (For Tower) \$233.50

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FREE! WRITE TODAY for full information and literature on the Alprodco EREC-TOWER as well as Alprodco Aluminum TV-FM-AM Towers.

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A Partial List of Authoritative Chapters:

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Now you can have all the right answers to any subject in the field of Audio. Learn how to select and get the most out of recording equipment. Tells you how to select the proper amplifier for given applications, how to test amplifier performance, how to eliminate hum. Explains microphone, speaker and pickup principles and selection factors. Shows how to utilize inverse feed-back, expanders and compressors. Covers hundreds of subjects-a vast wealth of reliable information found in no other single volume. If you work in the field of Audio, this book belongs in your library. Order your copy today!

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tened to the ends. "Did this come with

it?" he asked.

"No. that is a Barker & Williamson #3006 'Miniductor' with the ends unwound until they both take off from the same supporting bar, leaving a full sixteen turns between those ends. I use it to determine the capacity of unknown mica or ceramic condensers. When any condenser of from 2 or 3 $\mu\mu$ fd. to .005 μ fd. is clipped across that coil, the resonant frequency falls within the range of the five lowest-frequency inductances furnished with the instrument. I simply find this frequency with the dipper and then refer to this graph I made in which resonant frequency is plotted against capacity, and I know the value of the condenser. This is the old mustard for identifying condensers when you are not sure of the color code or when one of the colored dots cannot be identified.'

"This is rather funny-looking graph

"It is double logarithmic paper with two vertical cycles and four horizontal cycles. The vertical cycles from the bottom up read 1 to 10 and 10 to 100 megacycles. The horizontal cycles from left to right indicate 1 to 10, 10 to 100, 100 to 1000, and 1000 to 10,000 μμfd. The resonant frequency of the coil and a small-tolerance 100 µµfd. silver mica condenser was carefully measured with the grid-dipper and plotted on the graph. I know that as long as I use the same inductance and vary the capacity, the resonant frequency doubles every time I divide the capacity by four and is halved every time I multiply the capacity by four; so this gives me any number of other points on the graph. On this kind of paper, these points all lie in a straight line; so all you have to do is determine a couple of points a goodly distance apart and draw a straight line through them. Were our coil a pure inductance, this line would be accurate throughout its length; but because of the distributed capacity of the coil, there is a small error at the lowcapacity end. To correct this I measured several Ceramicons of low capacity and high accuracy and curved the upper left-hand end of my line to pass through these plotted points. are many other ways of determining capacity with a GDO. some producing greater accuracy; but this method is the easiest and most practical for the needs of the technician."

"Can you measure inductance with the gadget?"

"Why not? All you have to do is place a known condenser across the coil you're measuring and find the resonant frequency with the dipper. Then you refer to a resonance chart to learn what inductance will produce resonance at that frequency with that

While he was talking Mac clipped a twenty-ohm resistor in series with the coil and condenser lying on the bench. Then he placed a clip across the resistor so that it was shorted out. "See how sharp the dip is with the

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POSSNER ELECTRONICS (formerly Electronics Sales Co.)

DEPT. R-1 5279 West Pico Blvd. . Los Angeres 19, Calif. resistor out of the circuit," he said to Barney. "Then notice how it broadens out when I cut the resistance in. This difference in dipping action is really an indication of the 'Q' of the tuned circuit. A sharp dip means a high 'Q'; a weak dip, a low 'Q'. Since high resistance or shorted turns in a coil lower the 'Q' of a circuit in which it is used, the dipper can often be used to detect such a coil defect. The manual that comes with the meter tells you how to find the numerical value of 'Q'; but for our purposes, the rough indication of the sharpness of dip is sufficient."

"It's too bad," Barney sighed, "you can't use it to spot intermittents."

"But you can!" Mac exclaimed. "Look on page 108 of the August, 1952, issue of RADIO & TELEVISION NEWS, and you will find an article by Lewis Hughes explaining how the GDO can be used to spot intermittent condensers without removing them from the circuit or turning off the

"That thing's got more uses than chlorophyll," Barney muttered.

"Let's talk about using it in every-day radio service," Mac suggested. "Take the case of a receiver in which the r.f. stage will not track with the oscillator. The GDO can be used to check the tuning range of both the r.f. and oscillator circuits and will immediately reveal which one is not covering the span it should. In the same way, without ever plugging the set in, we can trim the turns of a new 'universal' loop antenna until it and the tuning condenser track perfectly with the dial markings. 'Loopstick' antennas can be adjusted just as easily and

"The instrument also makes an excellent portable signal generator that can be carried in the shopcoat pocket. With it tuned to the proper frequencies, you can quickly tell if a signal will pass through a set from the antenna, the grid of the mixer, or the grid of an i.f. stage. All you have to do is hold the inductance close to the point where you want to insert the signal. This makes for very speedy troubleshooting. We have already shown how the diode-rectifying action of the GDO can be used to determine if the oscillator is working.

"Remember that set we had a while back that gave us such a hard time because of parasitic oscillations? If we had had the dipper, we could have used the oscillating detector to locate the frequency of the parasitic, and then we could have switched off the receiver and used the instrument as a grid-dip oscillator to locate the circuit components yielding resonance at that frequency. Incidentally, as an oscillating detector, the dipper can trace a signal through the i.f. stages, too; and in an emergency, you can even use it as a signal generator to align those i.f.'s"

"The frequency settings could not be too accurate with plug-in coils and that small dial," Barney objected.



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"You're right: a GDO is not intended to be a precision frequency instrument in itself. However, by letting a harmonic fall on a known broadcast station, or other known signal, such as WWV's transmissions, you can set the grid dip oscillator very closely. Ordinarily, though, the markings on the dial of the GDO are plenty accurate for most purposes.

'But now let's talk about how the instrument can be used in TV service. You have already seen how it can produce a signal on either the sound or picture frequency of any TV channel, but it will also produce any frequency found in the i.f. channels of either separate sound and picture sets or those of the intercarrier type. I don't need to tell you how such a compact little signal generator as this can be used to isolate trouble in a TV set by simply injecting the proper signal at different parts of the circuit. All you have to do is just hold the inductance of the GDO close to the point where you want to introduce the signal. For example, in the case of a dead oscillator, if the GDO is tuned to the proper oscillator frequency and held close to the mixer tube, a picture can be obtained.

"A very important function of the grid dip meter is to check the frequency of traps and stagger-tuned transformers before any attempt at alignment is made. This can be done in a matter of seconds before the set is turned on and will often save much useless work. It is important that the transformers be set to approximately their correct frequency before alignment with a scope is started-especially if there is reason to believe the original settings may have been changed. Otherwise it is often possible to produce a curve similar to the correct one with the individual transformers set away off their specified frequencies, but the curve will not have the proper amplitude because the mistuned transformers will not have the 'Q' for which they were de-

"Still another important use for the GDO," Mac went on, "is as an auxiliary 'exploring' marker to be used to determine characteristics of a curve while the regular marker is left fixed at an important point. By positioning the GDO just right with regard to the set, a marker of the desired size can be obtained. If you want a precision marker, a crystal can be plugged into the coil socket, using an adapter, and the oscillator will function at the fundamental frequency of the crystal and produce strong harmonics. The tuning condenser setting serves as a broad control of the amplitude of oscillation and permits the frequency to be varied over a few cycles. I have used ham crystals for the 160, 80, 40, and 20 meter bands in this fashion and all oscillate strongly. A surplus tank-transmitter crystal with a fundamental of about 510 kc. would not work, however.

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uses of such a versatile gadget now," Mac broke off; "but I'll tell you what I'm gonna do: for every new use for the GDO you come up with, I'll give you a couple of bucks. Said use, however, must be one in which the dipper does a job quicker or better than an instrument normally used for the purpose, or it must be one in which the portability of the grid dip meter is an important item. How does that sound?"

"Like money in the bank!" Barney said enthusiastically. "Come with Papa, Mister Grid Dip Oscillator; we're going to bankrupt this tight-fisted Scotchman!"

C.W. TRANSMITTER

By GLENN W. DYE

THIS true pocket portable can be built up from scratch or from one of the surplus BC-746B tuning units, some of which are sold with one 80-meter crystal. The basic unit supplies the chassis, tuning condenser, a usable crystal socket, and tie lugs. A 7-pin miniature socket and the small parts listed in the circuit diagram must be added, along with a small coil form and coil form socket, though a fixed-mounted coil can be used.

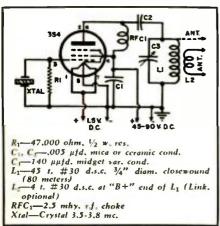
A home-made, U-shaped chassis about 4"x1'4"x1" can be bent from a strip of scrap metal 1'4" wide. The tuning condenser can be the familiar APC type or anything similar.

The best above-chassis parts lineup, for simplest and most efficient below-chassis wiring, is crystal-tube-condenser-coil. If a BC-746B is used, its crystal socket should be moved to the end of the chassis and the tube socket installed in its place.

With a 67-volt supply, the plate-screen current of the 3S4 tube will be 12 to 15 ma, in the operating condition. A flashlight cell can power the filament. Keying is done in the "B—" lead from the battery. The antenna (about 135 feet of small magnet wire will do) can be connected to the plate pin of the coil socket (see diagram) and the ground to "B—", or the optional link coil may be used.

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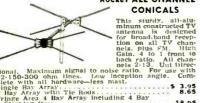
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Manufacturers' Literature

Readers are asked to write di-rectly to the manufacturer for the literature. By mentioning RADIO & TELEVISION NEWS, the issue and page, and enclosing the proper amount, when indi-cated, delay will be prevented.

PARTS BULLETIN

Greylock Electronics Supply Co., 115 Liberty Street, New York 6, New York has released an 8-page television and radio technician's bulletin which lists a number of timely buys in television and radio tubes and parts.

The company is also accepting requests for its 1953 catalogue which will be available shortly. The complete catalogue will contain 68 pages of offerings.

PARTS DIRECTORY

The Tube Department, RCA Victor Division, Radio Corporation of America has recently issued a comprehensive, 142-page "Service Parts Directory" containing schematic diagnostic parts lists, and top and bottom chassis views for the seventy-one 1950 and 1951 RCA Victor television receivers.

Designed for the convenience of television service dealers and technicians, the directory speeds and facilitates the selection of service parts.

The directory's pages are 11 x 17 inches in size and so arranged that the parts lists and top and bottom chassis views for a particular model face the corresponding schematic diagram. Service parts are listed by symbol number. This arrangement facilia tates the location of the stock number of any part shown on the schematic.

The TV receivers in the directory are indexed by model name, model number, and chassis number. The r.f. tuner chassis number appears on each schematic. The model name, and model and chassis numbers are listed on the right-hand page margins to help locate information quickly.

The directory (SP-1014) is now available from RCA tube and parts distributors.

FACILITIES BROCHURE

The products of Raytheon Manufacturing Company, Waltham, Massachusetts, are shown in the illustrated, three-color catalogue recently published by the electronics firm.

A brief history of the company and a photo layout of its various plants are followed by detailed descriptions of the products of each of the company's four divisions: receiving tube, power tube, equipment, and radiotelevision. A page is devoted to an outline of the concern's research activities.

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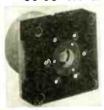
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Western Electric Western Electric Speaker units, for horn or baffleboard mtg. Shock and blast proof diaphragm, will handle up to 60 watts. Response to 7.000 cbs. favoring high fred. Impedance 13 ohms. Dim: 6"x 6"x 44" deep. Throat opening—1%" dia. Anico 5 sug wt. 6

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Precise Signal Generator and Heterodyne Meter, with crystal calibrator for check points every 1.000 KC. Range .125 to 20.0 MC. Complete with tubes, crystal. Excellent Condition units. BUT NON-MATCHING Calibration Books. Follow the Instruction Manual for "Adjustments." and you can make the instrument and calibration book jibe. We could do it and charge you \$95.00 per unit, but we think you would prefer to do it yourself and save \$30.00.

BC-221 Freq. Meter, as Described. EACH.......\$65.00

MISCELLANEOUS SPECIALS

The following items are for Exporters, Governmental Agencles, and Industrial Companies. Wholesale Only All material Is in stock and available for Immediate delivery. Descriptive literature and prices available upon request.

MARINE

TCS X'mttr-Receivers for Ship or Shore.
TAJ 500 Watts Output, 175-550 KC. New Equipment, with Spires, Motor Generator (AC and bC available) Starter, Tubes, Complete.
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Spares.

GO-9 100/125 W. IF/HF Ship or Aircraft Transmitter. Al or A2 Emission. All New with Spares.

150-AY Mackay IF Ship X mttrs.

8707 RMCA Ship Radio Compass.

MISCELLANEOUS

DZ-2 Direction Finders.
GP-7 Aircraft Transmitters.
ZB-3 ILAS Eqpt.
SCR-283 RCVG and X'mttng Eqpt. Complete.
RT.3/ARN-1 Altimeter.
RADIOSONDES ANAMQ-1A to D. New.

SCR-610 Crystals, in sets (120 channels) or individually. TESTED. Write for PRICES.

EXTRA!

PE-104 POWER SUPPLIES for Receiver of SCR-284, NEW, with Spare Vibrator, Export-Packed. Large Quantity Available. WRITE Packed. Large FOR PRICES.

GROUND AND AIR COMMUNICATIONS

TDQ VHF 100-156 MC 50W. AM X'mttr for 110 V 50:60 C. AC.
BC.797 VHF 110-126 MC, 50W. AM Output or 110

50.60 C. AC.

BC.797 WHF 110-126 MC. 50W. AM Output or 110 V. 50/60 C. AC.

SCR-284 Ground Portable AM, Trans-Recr Eqpt. for Field Communications.

SCR-512 VHF, 4-Channel, 100-156 MC Trans-Rer Eqpt. for Plane or Ground Communications.

SCR-511, Walky-Talky, 3-6 MC. Crystal Controlled Trans-Recr. with Plug-In Units for Fred, Changing.

96-200A, 2 KW Wilcox X mttr, 125-525 KC, 3 Cabinets: RF Unit, Modulator, Rectifier: A1, A2

Cabinets: RF Unit, Modulator, Rectiner: A1, A2 and A3 Emission.

10 KW GE FM RF AMPLIFIERS, Type BF-3-A, 88-108 MC, Complete with RF Power Supply (separate unit), New Eapt. For increasing power FM and Television stations. Write for descriptive sheets and prices.

2 GREAT BOOKS By Milton S. Kiver IF YOU SERVICE TV -YOU NEED THEM! "TV Servicing Short-Cuts Based on Actual Case Histories" shows you how to

solve commonly recurring troubles

> the book that really teaches fast, expert service techniques

This book describes a series of actual TV service case histories, each presenting a specific problem

about a specific receiver.

The symptoms of the trouble are described and then followed by a trouble are described and then followed by a step-by-step explanation of how the service technician localized and tracked down the defect. Finally, there is a detailed discussion of how this particular trouble can be tracked down and solved in any TV set. The discussions which follow each case history are invaluable—they explain how to apply the proper time-saving servicing techniques to any TV receiver. Here, in one volume, is the successful experience of experts—to make your service work easier, quicker, more profyour service work easier, quicker, more profitable. Over 100 pages, 5½ x 8½", illustrated. Pays for itself on a single service job.

ORDER TK-1. Only.

"HOW TO UNDERSTAND AND USE TV TEST INSTRUMENTS"



shows you how to get the most from your test instruments

Provides basic explanations of how each test instrument operates; describes functions of each con-

functions of each control and shows their proper adjustment to place the instrument in operation. Covers: Vacuum Tube Voltmeters, AM Signal Generators, Sweep Signal Generators, Oscilloscopes, Video Signal Generators, Field Intensity Meters, Voltage Calibrators. Describes each in detail; explains functions: tells proper use in actual servicing: Caltbrators. Describes each in detail; explains functions; tells proper use in actual servicing; shows how to avoid improper indications. Because this book gives you a clear, complete understanding of your test instruments, you get more out of them, save time, and add to your earning power. Over 175 pages, 8½ x 11", illustrated.

Order from your Parts write direct to Howard 2203 East 46th Street,	W. Sams & Co., Inc.
My (check) (money ord enclosed, Send the foll TK-1 (\$1,50)	
Name	[] IN-1 (\$5.00)
Address	
CityZone	State

The catalogue also lists the addresses of the principal sales offices of the company throughout the United States.

INTERCOM DISPLAY

Vocaline Company of America, Inc., 300 Vocaline Building, Old Saybrook, Conn., has released a new counter display featuring its portable intercom.

In the form of an eye-catching arrow, the display "points" to a "Vocatron" intercom on which it stands. In this way the display takes no more counter space than the compact intercom itself.

The sales message is concise and "quick reading" and urges passers-by to "ask for a no-obligation demonstra-

The company will provide complete details on how the new display may be obtained.

PHONO NEEDLE CHART

Jensen Industries, Inc., 329 South Wood Street, Chicago 12, Illinois, has issued a new replacement phonograph needle wall chart which incorporates several exclusive features.

Designed to simplify the work of the record dealer and the service technician, this guide also aids retailer inventory control and shows authorized needle substitutions.

A total of 78 different replacement needles are silhouetted on the chart. each with its Jensen "Durosmium" or sapphire equivalent. Representing the requirements of the 16 leading cartridge manufacturers, it shows all the existing cartridge numbers in quick, easy-to-read style.

The chart also features a "best seller list" which indicates the relative turnover of each needle and, in effect, tells the dealer which of the many needles in the line he should stock heavily.

Copies of this 8" x 22" chart, which is printed in two colors, are now available from the company's distributors or by writing the company direct,

DU MONT SCOPE

Allen B. Du Mont Laboratories, Inc., 1500 Main Avenue, Clifton, New Jersey, has recently issued a 12-page catalogue covering its Type 304-A oscilloscope.

The publication outlines the features of the new instrument, instructions on calibrating the unit, data on the various controls, specifications, and other pertinent information.

The catalogue is lavishly illustrated with actual photographs of the unit and scope patterns obtained at specified settings of the controls.

CENTRALAB PRODUCTS

Centralab, A Division of Globe-Union Inc., 900 East Keefe Avenue, Milwaukee 1, Wisconsin, lists 470 new items in its new industrial and distributor stock catalogue, No. 28.

The book has been expanded from 28 to 32 pages and covers the company's five product divisions: variable resistors, ceramic condensers, rotary and lever switches, printed electronic circuits, and steatite insulators.

The fully-illustrated and indexed catalogue is available free of charge from any Centralab distributor or by writing the company direct.

NEWARK'S 1953 CATALOGUE

Newark Electric Co., 223 W. Madison St., Chicago 6, Ill., has issued its 1953 catalogue, No. 55.

This 194-page listing covers components, equipment, manuals, etc. for industry, lahoratory use, high-fidelity applications, and for radio and TV. This complete manual carries a comprehensive index for ready reference.

HUDSON CATALOGUE

Hudson Radio & Television Corp., 48 W. 48th St., N.Y.C. has just issued its catalogue H-53 comprising 194 pages of parts and equipment listings.

Of particular interest to purchasing agents is the inclusion of the latest JAN cross-reference guide. The catalogue is fully indexed to facilitate locating specific parts.

AUDIO CATALOGUE

Terminal Radio Corp., 85 Cortlandt St., New York 7, N. Y. has just published a 132-page audio equipment catalogue which contains fifty pages devoted to high-fidelity home music system components and seventy-six pages covering p.a., institutional, recording and broadcasting equipment as well as audio test instruments and similar specialized equipment.

The new catalogue is available without charge to interested persons or firms on request.

1953 POCKET BOOK

The Tube Dept. of RCA has completely revised and expanded the 1953 edition of its yearly pocket reference and calendar notebook to provide even more technical data on its kinescopes. receiving and transmitting tubes, electronic components, test equipment, radio and industrial batteries, and miniature lamps, than before.

A section on troubleshooting hints, prepared by John Meagher, is included along with 16 pages of full color maps, a 58-page diary, and a memo, address, and telephone number section.

THORDARSON CATALOGUES

Thordarson-Meissner, Mt. Carmel, Ill. has issued three new catalogues of interest to the industry.

The #400-K catalogue lists replacements types of power, filament, and audio transformers for the service industry as well as standard types. A special section is devoted to TV replacement transformers. The second catalogue is a TV replacement guide for the service industry. It provides complete information on over 2500 TV models. Manufacturers parts numbers and the company's replacement types are listed for power and filament transformers, filter chokes, audio, vertical, and horizontal output transformers, focus coils, booster transformers, and deflection yokes.

The #53-A general catalogue gives specifications on the Meissner line of AM-FM tuners, receivers, and amplifiers and includes a section on receiver and amplifier kits. The company's new novice transmitter kit and hi-fidelity 10 watt amplifier are listed for the first time.

TV REPLACEMENT GUIDE

Standard Transformer Corp., 3580 Elston Ave., Chicago 18, Ill. has issued a simplified television transformer catalogue and replacement guide which lists replacement information on over 4400 TV models and chassis.

All the technician has to do is look up the manufacturer's part number, listed in numerical order by type of transformer, then the Stancor replacement will be found listed next to it.

U.H.F. ANTENNA DATA

The LaPointe-Plascomold Corp., Rockville, Conn. is now offering an 8page catalogue, entitled "UHF Antenna Systems--How, What and Where for Every UHF Area", to interested persons

The brochure includes valuable u.h.f. data of interest to the installation technician. It is now available at all "Vee-D-X" jobbers on request.

PRINTED CIRCUITS

Erie Resistor Corp. of Erie, Pa. has issued a new bulletin on its complete line of five types of electronic printed circuits, each in a range of capacities: diode filters, triode plate couplers, vertical integrators, pentode plate couplers, and audio output circuits.

MERIT CATALOGUES

Merit Coil & Transformer Corp., 4425 N. Clark St., Chicago 40, Ill. has issued two replacement guides, one a 36-page book covering practical recommendations for replacements in over 6000 TV models and chassis and the other an 8-page catalogue covering transformers, i.f. and r.f. coils for auto radios.

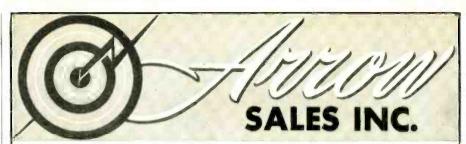
The auto radio guide is available from jobbers as Form No. 3 while the TV handbook is designated as No. 405. The company will also furnish copies on request.

TAPE RECORDER DATA

The Pentron Corporation, 221 E. Cullerton Street. Chicago 16, Illinois, now has available several brochures describing its line of magnetic tape recorders and recorder accessories.

The first pamphlet is a six-page folder which describes the company's multi-speed portable tape recorder unit. The booklet points out applications for the unit and gives concise data on performance and operation.

The second booklet covers accessories for tape recording, including tape player-amplifier, mike mixer, radio tuner, foot pedal, phonograph, tape player-preamp, speaker in baffle, recording tape, telephone pickup, waterproof oover, accessory cords, and a tape carrying case.



AN/APS-4

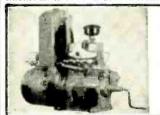
Airborne radar. New. .P.U.R AN/APS-6

Airborne radar set. New.

AN/APR-4

RECEIVER & TUNING UNIT.P.U.R. AN/APS-3

AIRBORNE RADAR SET. Now Complete P. U. R.



POWER UNIT PU-41/G

Power Unit PU-41/G (Köhler Model IM21A) is an electric generating Power Unit PU-41/G (Köhler Model IM21A) is an electric generating set consisting of a 4-cylinder, 4-cycle valve-in-head, fluid cooled, manual starting (crank) assoline engine directly connected to an a-c generator of the revolving armature type. Engine is rated 4.25 horsepower at 1.200 r.p.m. and consumes approx. 0.45 gallon of fuel per flour at rated load. Generator is rated at 1.5 kilowatts, 60 cycles, single phase, 110 V, 13.6 ampures at 100% power factor. Length: 45"; width: 16"; height 36". Weight (crated) 880 lbs. New in cratical law constitution of the control of original box with spare parts...

(G) Monthly Specials!

RT-34/APS-13 420 MC. TRANSCRIVER with stages of 30 MC. IF amplifier strip. Less & A tubes & R.F. section. With dynamotor. \$9.95

2 TRANSMITTERS
BC-457 (4-5.3 MC) and BC-458 (5-3.7 MC).
Command transmitters, Subment just in, Limited chandity, Less tubes and xtals, Good cond.
EACH \$4.95 PER SET. \$9.50

AN/ARC-5

R-28/ARC-5 RECEIVER 100-156 MC. \$49.50

With tubes. Like New 12-13/ARC-5 TRANSMITTER 100-156 MC. With tubes. Like New 15-14 Like New 15-15 MC. With tubes Like New 15-15 MC. With tubes Like New 15-15 MC. With tubes Like New 15-15 MC.

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For prospectors, miners, oil companie \$59.50 WHILE THEY LAST!

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	Used	New	Used	New
	ANTENNA RELAY. Less cond.\$1.95 With cond. TRANSMITTER CONTROL ROX	\$ 3.95 1.50	BC-453 With tubes	\$0.95
	3-RECEIVER REMOTE	2.95	FT-234 MOUNTING RACK for single	3.50
	MECHANICAL DRIVE SHAFT.	2.95	FT.226 MOUNTING RACK for 2 Com-	3.95
	2-POSITION RECEIVER CONTROL BOX	2.95	FT-221 MOUNTING PLATE for FT-220 FT-220 MOUNTING BACK for 3 re-	1.50
BC-459 BC-455	6-9 MC RECEIVER. With tubes 9.95 Less tubes 7.95	14.95	FT-225 MOUNTING PLATE for BC-456	2.25
BC-454			Complete set of 4 tubes for transmitter	4.50 1.95

RADAR TEST EQUIPMENT

TS-3, TS-12, TS-13, TS-15, TS-33, TS-34, TS-35, TS-36, TS-45APM3,

ARC-4 TRANSCEIVER

140-144 Mc. Complete with control box, rubes, 12/24 VDC dynamotor with schematic. This is a special reduction for this month only. \$32.50

TUBES! NEW! ORIGINAL BOXES!
Limited Quantities Available
250TL... Ea. \$11.50 250T11... Ea. \$14.50

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11-tube UHF tunable receiver with \$17.95\$3.50

Miscellaneous 5

HS-18 HEADSET. HS-23 HEADSET. 8.000 ohms NEW
1-26 CHEST TYPE MIKE. New
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20 lbs. of good, useable radio parts

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BC.605 INTERPHONE AMPLIFIER. With dual mike limit circuit. NEW.

RM-13 COMPLETE REMOTE CONTROL BOX. For 3 septement transcrivers. With TS-13 handset, decided output meter and ET-8 ringer unit. 110 V.

FL-8 RANGE FILTER. COM. 1.95

UNES! TUBES!

TUBES! TUBES! TUBES! 16JP4 ..\$19.95 16AP4 ..24.95 16DP4 ..19.95 304TH ... 58,95 304TL ... 8.95 830-B ... 2.75 IN-4A L R TUNING METER. Used. \$3.95
FL-5 RANGE FILTER \$1.25
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BC-1033 75 MC MARKER BEACON RECEIVER. COMPLEX WITH THE PROPERTY OF THE PROPERTY

MP-22 MOBILE ANTENNA. MOUNTING RACK. Complete with hardware. New ... \$ 3.95 Antt. Ded 1.70 ST TUNING METER. NEW 2.50 NEWS 1.70 ST TUNING METER. NEW 2.50 NEWS 1.70 ST TUNING METER. NEW 2.50 NEC 1.23 75 MC. MARKER BEACON RECEIVER. Complete with tunes. mig. rick. NEW 10.95 TU-25 TUNING UNIT. (3.5-5-2 MC.) For BC-223 Xmir. Used 2.95

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BC-624 VHF RECEIVER. Freq. range 100-156 MC. Less tubes & crystals. with conversion \$19.95 dope. Used, good cond. BC-625 VHF TRANSHITTER. Freq. range 100-156 MC. Less tubes & crystals. with con-\$12.95 version dope. Used. sond condition. \$12.95 \$29.95

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Popular Double-IF Model SX-71

A double superheterodyne circuit receiver at modest cost. Built-in narrow band FM reception. Temperature compensated, voltage regulated. | 5 position band selector for 538-1650 kc, 1600-4800 kc, 4.6-13.5 mc, 12.5-35 mc, 46-56 mc. 1



All-Wave Receiver Model \$X-62

Covers 540 kc to 109 mc-including AM, FM, and SW broadcasts. Six bands: 540-1620 kc, 1620 kc-4.9mc, 4.9 mc-15 mc, 15-32 mc, 27-56 mc (AM-FM), 54-109 mc (AM-FM). Only \$289.50. Other popular Hallicrafters models: S-76, 11 tubes plus voltage regulator and rectifier. \$169.50; \$-408, \$99.95; \$-72, \$109.95; Only \$199.50

Butler 2. Missouri

DISTRIBUTORS OF SHORT WAVE RECEIVERS"

THE ORIGINAL

ULTRA-LINEAR

WILLIAMSON AMPLIFIER



Model UL-1 Power Amplifier,

20 watts, Ultra-Linear Williamson-type Circuit.

AVAILABLE SEPARATELY Completely independent, self-powered, remote control unit. Incorporates the famous Model A-100 Phonograph Preamplifier-Equalizer and the Model CA-2 Control Amplifier.



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TV Receiver Sensitivity Measurements made Simple with

Portable

...a "must" in fringe areas



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anufacturersi

Consult your Job-

ber or write for further information

TV service Checks receiver from antenna terminals to picture tube

> Microvolt scale is divided into 3 sections as a guide for the servicemen

* Sensitivity testing is accepted by servicemen as the best method of determining the, cause of bad pictures

SERVICE INSTRUMENTS COMPANY 422 South Dearborn Street, Chicago 5, Illinois

The third brochure is a small folder briefly describing the portable tape recorder and its accessories and is designed as an envelope stuffer or mailing piece.

Details on any or all of these brochures are available from the com-



U.H.F. Antennas

(Continued from page 58)

again provide a 300-ohm termination at (L-L).

The close positioning of B-B, D-D, and E-E form an array possessing a very low "Q". This low "Q", in effect, represents a dipole of a large electrical diameter which, in turn, accounts for the broad (all v.h.f. channel) frequency characteristics of the entire array.

So much for the v.h.f. sections of the composite array of Fig. 9. To this is added the tilted dipole in front of rod F-F for reception of signals over the u.h.f. band. F-F, as we have said,

acts as its reflector.

Now, to prevent interaction between v.h.f. and u.h.f. sections, another printed circuit filter is added to the array. The low-frequency electrical equivalent of this filter is shown in Fig. 8A, while its physical appearance is indicated in Fig. 8B. The transmission line to the set is connected across points P-P. The u.h.f. antenna is then connected to one end of this filter and the v.h.f. section to the other. The various resonant circuits comprising this filter are shown, together with their resonant frequencies. Isolation, now, is achieved in the following manner. The u.h.f. signals leaving the u.h.f. array see short circuits in the 195 mc. and 70 mc. resonant circuits because the u.h.f. signals can pass through the condensers of these sections. On the other hand, u.h.f. signals see high impedances in the 680 mc. tuned circuits. Therefore, there is no tendency for any u.h.f. signal picked up by the v.h.f. antenna to reach points P-P. Any u.h.f. voltages reaching the transmission line must thus come from the u.h.f. antenna.

Considering v.h.f. signals, those coming from the v.h.f. section will encounter little opposition from the 680 me. resonant filters and therefore v.h.f. signals will reach points P-P undiminished. However, v.h.f. signals picked up by the u.h.f. array will be largely lost across either the 70 mc. tuned circuits (for low v.h.f. band signals) or the 195 mc. filters (for high v.h.f. band signals). Very few of the v.h.f. signals from this source will reach points P-P.

The antenna is designed to operate with any 300-ohm balanced line and at present this means either the 300ohm flat twin-lead or the 300-ohm tubular. There are, however, other lowloss lines being developed to provide better u.h.f. operation than the lines now available.

(To be continued)

RADIO & TELEVISION NEWS

Signal Distribution

(Continued from page 47)

plifier can overcome some of the difficult problems of signal levels on the system. With individual channel amplifiers it is possible to adjust the level of each station in relation to a uniform signal distribution amplitude and establish an optimum signal-tonoise ratio for each station. In a difficult local-fringe reception area the strong signals can be held down to a level that will just prevent overload by high amplitude levels. Fringe signals are amplified as much as possible to bring them near what is considered to be the desirable distribution amplitude.

Possible combinations of these basic units in practical distribution systems are illustrated in the block diagrams of Fig. 3. The first shows a simple system that can be used for a small apartment building or a store demonstration arrangement in a strong signal area. In this basic arrangement the amplifiers are for matching and isolation. Some losses occur, so it is really only satisfactory with strong signals and a limited number of outlets. Notice that the larger distribution outlet amplifier can feed individual receiver groups as well as a line running to smaller distribution ampli-

A fringe or weak signal installation would require the addition of a wideband amplifier or a channel-strip amplifier group to bring up the signal levels. Such an arrangement can also be used in a strong signal area for supplying the signal to a larger group of receivers. When the signal level declines to a specified minimum level another amplifier is inserted to reestablish signal distribution levels for continuance of the line. Each amplifier point recovers the losses encountered in the previous section of the distribution system so signal division can be continued.

Still another distribution plan is shown in Fig. 3 and can be used to supply hotels and apartment houses or groups of dwellings. Line lengths must be evaluated (db loss-per-hundred-feet) and made no longer than is required so signals can be amplified to the prescribed level of 10.000 microvolts by the next amplifier of the chain.

Distribution Problems

In a difficult multi-outlet area such as that north and east of Philadelphia, a distribution mixer with individual channel amplifiers is a necessity if New York and Philadelphia reception is desired. In this area there are very strong local signals and weak fringe signals (some 60-80 miles to New York). There are many stations to be received (10 stations maximum) and strong adjacent channel interference must be overcome. Practically all reception difficulties exist that would tax

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PLATT BREAKS ALL PRICES! TEST EQUIPMENT SALE

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No doubt about it, you haven't seen buys like these in many a month! Why don't you check them yourself? All merchandise is on display at PLATT'S New Branch Bargain Store. And you'll find many more items not listed here. First come, first served! (Send Mail Orders to Main Store.)

NATIONALLY FAMOUS VTVM

\$34.95



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TOP BRAND SIGNAL GENERATOR Model 320

Freq. Coverage on fundamen-tals: 1.70 KC to 1210 KC. 1.3 to 102 mega on 7 callbrated harmonics. Completely wired \$24.95

SPECIAL!

Radio City Products Model 449 VOLTOHMMETER

AC-DC output; 1000 V, ohmage up to 2 megs. In metal case with zero adjusting knot us front to 2 mers. In metal case were adjusting knot in the metal Ready for use. ONLY MITTED NUMBER LEFT— SPECIAL! \$14.95







APPROVED Model A-200 SIGNAL GENERATOR

Freq. Range: 100 KC to 75 megs in 8 signal harmonics. AC operated. Excellent for TV & FM alignment. This special buy cannot last long—so prense herry so that you aren't disap \$21.95

BRAND NEW SPEAKER SALE!



SPECIALS!

A full line of Recording Tabe, Crystals, Pickurs, Phum Motors, and the New G.S. Reluctance Cartridge are available at Platt's Branch Store, It will buy you to come in and browse around a bit!

BC-221 Frequency Meter

21 Frequency
alue! QUANTITY IS LIMITED
set come, first served. They
t like new, with original callcharts. Hange 125-20,000
the crystal check points in all
Complete with \$129.50
and tubes. \$199.50 rough and tubes 5189.50
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Tower Supply Meters are factory tested, checked for frequency alignment and GUARANTEED.

MN-26 INSTALLATION



MN-26c RECEIVER—Remote control commercial type navigational. Indicommercial type navigational indi-cates direction of any desired trans-mitting station. 3 bands—frequency range 150KC to 1500KC; has 12 6V type tubes. Brand New—\$39.95 Original Cost \$600.00...\$39.95

ARMY TEST UNIT 1-236



Meter is contained in a metal box Meter is contained in a metal 50.85 14.8 long x 334.7 wide x 314.7 deep. Comes complete with test leads and instruction book. Can be used for testing between AC and DC measuring resistances of circuits, checking fuses and test-

ing capacitors. SPECIAL \$4.19

MINIMUM ORDER \$2.00

Immediate Delivery — Send 25% deposit on C.D.D. orders. All shipments F.D.B., N.Y.C. (N.Y.C. residents add sales tax to your remittance.)

BRAND NEW! TUBES TUBES

182269c 182353,75 282249c 2C2609c	100R 49c 114B 29c 215A 09c 221A 29c 304TH \$5.95	861 19c 951 13c 1616 49c 1625 29c 1626 19c
2C26A09c 3B2219 3C2498c 3D839c 7C439c	316A29c 388A59c 471A\$1.19 532A\$1.19	1629
10Y 19c 12K8Y 39c 15R 39c 39/44 29c	722A99c 801A19c 82639c 84129c 84317c	E114849c RK3499c VR9214c VT12715c

ELECTRIC MEGAPHONE SYSTEM



For Rural Areas, Hotels, Commercial Steamers, Ball Parks, Etc.

U. S. NAVY Type PAE-1 Electric Mckal-hone equent is designed for voice reinforcement in much same manner as, but to a greater designe than the same manner as but to a greater designe than the same part of the same part of the metal to the same part of the metal to the same part of the metal part of signal to the reproducer section. Charging charging the self-contained storage battery able amplifier. BRAND NEW-A TIFMENDO DEMONSTRATION GIVEN AT EITHER OF PLATT'S STORES. \$149.50



SCR-274N COMMAND and ARC-5





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	BC-453—190 to 550 KC	29.95	\$13.95	549.95 24.95 19.95
	TRANSMITTERS		,,,,,,,	
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	ADDITIONAL EQUIPMENT			
	BC-456 Modulator	1.49	2.95 1.95	5.95 2.75
	BC-450 Control Box (3 Receiver) BC-451 Control Box (Transmitter) BC-442 Relay Unit (ANT)			2.39
	Plugs: PL-147, 148, 151, 152, 153, 154, 156—EACH Flexible Shafting with gear to fit		1.25	3.00
	receivers			2.69
	3 Receiver Rack	1.79	2.29	2.98
	2 Transmitter Rack Single Transmitter Rack	1.69	2.39	3.97 3.97
ŀ	DM-32 Dynamotor for Command Set		3.95	5,95
l	DM-33 Dynamotor for Command Set.		2.95	3.95
	Mounts for 2 Trans. Rack, 3 Rec. Rack Modulator, & Antenna Relay Unit	4,	1.95	

HEADSETS

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tlon	plug, use	ert. mite	COLIGI1.	2 79	E)	- 41
HS-23	high Imte	edance. I	BRAND			10
NE	V with en	r pads		5.95	711	
HS-33	low Imper	dance. F	BRAND		الاست	
NE	with e	ar pads.	. cord		_	
and	Pl.54 plu	Ig				5.39
HS-30	BRAND .	NEW-W	estern	Electric.		5.95
CD-30	7A Cords.	6 ft. N	EW			.89
EL-167	J hisch im	npedance	. Inch:	des two	re-	
coil	ing units	-1				3.9



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the performance of a multi-outlet installation. Consequently, we can consider this as an ideal testing area.

In this section the individual channel amplifier and mixer combination affords greater versatility. Individual amplifiers tune to specific channels and amplifier tune to specific channels and amplification. Strong signals that require amplification. Strong signals are not amplified (and for some installations must be attenuated) and, therefore, are not permitted to reach overload levels. Here is a definite aid in overcoming adjacent channel interference. A wide-band amplifier would only accent adjacent channel spillover and intermodulation because of over-amplification of strong local signals.

In a typical installation. Fig. 1, a Blonder-Tongue MA4-1-M was used. This unit will accommodate four individual channel amplifiers. The most consistent New York channels are 2, 4, and 5 and individual amplifiers were used for these channels. A Channel 10 amplifier occupied the fourth position because it is the weakest local channel.

Two antenna arrangements were employed, each performing satisfactorily. In the first plan, Fig. 4A, a compromise low-hand yagi was used to receive New York Channels 2. 4, and 5 and a separate conical type for local channels. The yagi was applied to the Channel, 2, 4, and 5 amplifiers; the conical to the Channel 10 amplifier and the wide-band antenna input of the mixer. The strong local Channels 3 and 6 signals entered the mixer at this point and consequent attenuation reduces their levels to safe interference limits. The mixer output feeds the distribution system. Weak signals have been strengthened; strong ones, retarded. Thus, from this point conventional wide-band amplifiers can be used to maintain distribution signal levels. In areas where there are fewer stations, a separate and peaked antenna could be used for each weak station and, it is apparent, the individual channel amplifiers afford maximum antenna versatility.

The same plan can be used for a two-receiver home installation. Just a single "Directronic" antenna was used to supply the signal to the four channel amplifier (2, 4, 5, and 10), Fig. 4B. The wide-band antenna input of the mixer was not used. Instead, by properly connecting a jumper on the mixer, the wide-band antenna input circuit can be used as a second output and two receivers in the house were supplied with all signals and no interaction. It is important to realize that the Channel 3 and 6 signals entered the mixer at a useful level via the Channel 2, 4, and 5 amplifiers.

The advantages of the second plan insofar as a dwelling is concerned are single simple antenna installation and two-receiver feed without any additional equipment. Disadvantages are that "Directronic" switching is required as the switch must be set properly for either New York or Philadel-



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phia reception. Also, New York signals do not receive the benefit of the full antenna gain obtained with a

yagi-type antenna.

To amplify more than four channels, a second mixer amplifier can be connected in series with the first mixer, Fig. 4C. For this area it was expedient to insert Channel 7, 9, 11, and 13 amplifiers into the second mixer. These are the most inconsistent stations because of erratic signal levels which vary widely due to weather conditions. Daytime reception is not possible in most of the area. Evening signals vary from very poor to quite good. However the second mixer furnishes fairly good reception of these stations in the evening.

For a single dwelling installation two antennas are advisable in order to make full use of the high-band signals when levels rise—a "Directronic" can be used for Mixer #1 (as discussed previously) and a modified stacked yagi for the New York highband channels to be introduced via the second mixer. In a multi-outlet system serving a number of families, the most practical plan is to use a lowband yagi for Channels 2, 4, and 5; a stacked high-band yagi for Channels 7, 9, 11, and 13; and a conventional

conical for local reception. In summary, the examples given demonstrate the versatility of the channel amplifier-mixer combination in reducing the problem of distribution in areas where there are numerous stations with great variations in signal level.

CODE PRACTICE

By DR. T. H. LIPSCOMB, W4RTI

WSC and WSL send out nightly (at 2318 EST) weather, baseball scores, political information, and human interest news at a rate of approximately twenty-

five words-per-minute.

I have recently recorded some of this material at seven and one-half inchesper-second on tape and play it back at just half this speed. This gives twelve and one-half words-per-minute of straight matter at a speed which is ideal for code practice required for the "Amateur Conditional" and "General Class' licenses.

This same material could equally well be recorded at 78 rpm on discs and played back at 33½ or 45 rpm.

The table below lists the times, calls, and frequency of broadcasts which are suitable for obtaining this code practice material.

Stations transmitting code signals.

(EST)	CALL	FREQ.	ORIGIN	SPEED
11:18 p.m.	WSC	125 6350 8430 11,175 12,675	N.J.	25
11:18 p.m.	WSL	5555 11,115	N.Y.	25
1:05 a.m.	KFS	6270 12,550	Calif.	25
3:10 a.m.	KPH	126 6370 8440 12,735	Calif.	25
12:00 noon	DZM	8670	Manila	25



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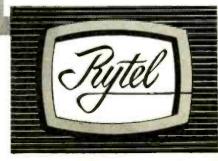
PLUS ECONOMY... simple, tough aluminum construction means low price, no maintenance, long life.

PLUS RUGGED CONSTRUCTION ... simplicity of design avoids fragile, expensive insulators, no chance of electrical or mechanical breakdown. Supported at current node (ground potential).

PLUS' APPEARANCE... no more monstrosities on the roof... just simple, attractive...perfect Double-O.

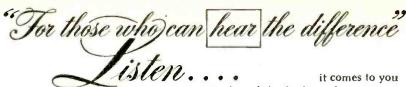
PLUS INSTALLATION... no more "servicemen's nightmares"... Double-O is a serviceman's dream...comes completely assembled, just a "U" clamp to tighten, no "adjustments"

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What's New in Radio (Continued from page 86)

company's "Sensicon" circuit with "Permakay" filter and employs 21 tubes (only 5 types, however, for economy in maintenance). The transmitter, which has a nominal power output of 20 watts, uses 9 tubes.

HIGH RATIO CONDENSER

Johanson Mfg. Corp., Boonton, N.J. is marketing a new concentric highratio condenser with a range of 1 µµfd. to 35 uufd

Designed for low minimum capacity. high "Q", applications, it has been used successfully in ten-channel transceivers. A friction spring locks the rotor to insure stability. Constructed of silver-plated brass and Pyrex glass. it operates well at the higher frequencies.

OVAL RESISTORS

Milwaukee Resistor Co., 700 W. Virginia, Milwaukee 4, Wis. is producing a new line of oval-type wirewound resistors to provide higher wattage ratings in small areas.

The resistors are currently available in 10 watt (3%" x 34") and 15 watt



(3/8" x 1") sizes. Spacers attached to ends of aluminum mounting strips permit easy stacking and better heat conduction.

HIGH-SPEED CONDENSER

A butterfly-type variable condenser capable of continuous operation at speeds as high as 3200 rpm is available from Hammarlund Mfg. Co., Inc., 460 W. 34th St., New York 1, N.Y.

Units are available with series effective capacity values ranging from 5.4 to 17 μμfd. nominal. Air gap between plates is .030" nominal. Outside dimensions of each silicone-treated steatite base are 1%" x 1%".

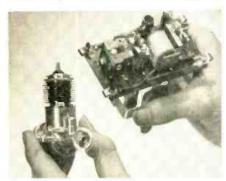
PORTABLE TAPE RECORDER

A battery-powered portable tape recorder with spring-wound motor, the "Broadcaster Model 610-SD", is now available from Amplifier Corp. of America, 398 Broadway, N.Y. 13, N.Y. Measuring only 11½" x 10" x 7½",

the unit weighs 15 lbs. with batteries. It operates at 71/2 inches-per-sec., furnishing 15 minutes of playing time on a 5" diameter, 600-foot reel of tape. A single-track head with double-gap is used. Recordings may be played back on any a.c.-operated studio unit at equivalent speed.

ENGINE FOR MODELS

Production is underway at the Herkimer Tool and Model Works, Inc., Herkimer, N. Y. on a new class A



engine designed for radio-controlled model plane operation.

The "OK Cub .14" weighs only 23/4 ounces but will carry sturdy radio equipment even in bumpy air. The company points out that the FCC now allows any model fan to fly his ship by radio control on the Citizens band (27.522 or 465 mc.) with approved equipment by just filing a registration form with the Commission.

"META-GUN"

A volt-ohmmeter in gun form has been introduced by Jersey City Technical Lab., 880 Bergen Ave., Jersey City 6, N.J. for radio and TV service work

It has a built-in light, a flexible probe for reaching test points, and a trigger range selector. All work can be performed with one hand. The Model



3A has 1000 ohms/volt sensitivity and the Model 3B 20,000 ohms/volt sensitivity. The gun measures 51/2" x8" x3", operates on four self-contained penlight cells, and weighs just 2 lbs.

MOBILE CONVERTERS

Radio Manufacturing Engineers, Peoria, Ill., a division of Electro-Voice has release three new mobile converters for hams.

The MC-55 is a five-band model covering the 10-11, 15, 20, 40, and 75 meter bands. The Model MC-53 is a threeband converter for 2, 6, and 10-11 meters. The Model MC-57 is a three-

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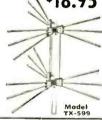
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All models have edge-lighted dials, side-knob tuning through a 25:1 worm gear drive, individual slug-type coils for each band, three-gang tuning, four tuned i.f. circuits, and an output frequency of 1550 kc.

Bulletin #169 covering all of the company's converters is available on request.

PENCIL SOLDERING IRON

A pencil-type soldering iron for precision applications has been introduced by The Lenk Mig. Co., 30-38 Cummington St., Boston 15. Mass.

Available in either 25 or 40 watt sizes, the new tool weighs 2 ounces, measures 71/2" over-all, and comes equipped with a 1/8" dia. tip. The handle is of plastic.

5-INCH SCOPE

Electronics Measurements Corp., 280 Lafayette St., N. Y. 12, N. Y. is offering a new 5" service scope, the Model 600.

The vertical amplifier has a wide ban I and can be used up to 5 mc. A two-step attenuator input is available. Synchronization is available on either positive or negative phase of input voltage through the vertical amplifier or from an external source.

RECTIFIER TESTER

Jackson Electrical Instrument Co., 18-46 S. Patterson Blvd., Dayton 2, Ohio has developed an instrument for testing all radio and television selenium rectifiers rated from 20 to 650 ma.

The Model 710 operates on 110 to 125 volts a.c. and has a variable indicated voltage range of 25 to 300 volts a.c. Use of the instrument is simple. After the load and voltage indicators are set and the line voltage adjusted, the test lead clips are placed on the rectifier terminals, the correct

meter range is selected, and test switch pressed. The "Good-Bad" dial shows the condition of the rectifier and indicates life expectancy.

TRANSISTOR SOCKETS

Transistor sockets are now available in limited quantity from Mycalex



Tube Socket Corp., 60 Clifton Blvd., Clifton, N.J.

Contacts can be supplied in brass or beryllium copper. The sockets, the "Myculex 410", are readily solderable and will not warp or crack when subjected to high soldering temperatures.

NEW ELECTROLYTICS
Aerovox Corp. of New Bedford, Mass, has introduced a new series of twist-prong base electrolytics for filtering in selenium rectifier circuits.

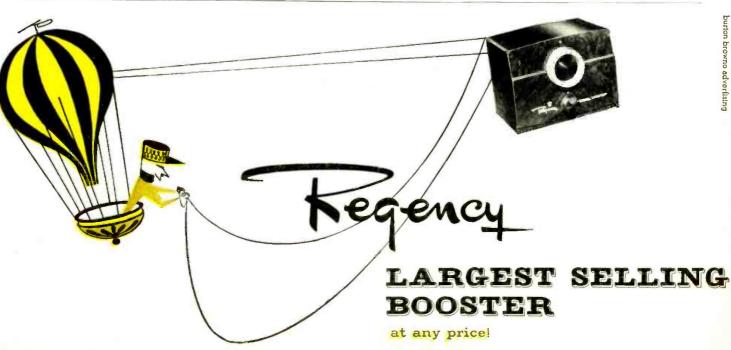
The Type AFHS series has been especially designed for this service with provision being made for handling the high ripple currents found in selenium rectifier circuits.

CONNECTOR KIT

Elco Sales Co. is now offering a "Varicon" miniature connector kit through its jobber outlets.

The new kit contains all parts needed to assemble the company's miniature connectors. Detailed instructions accompany each kit of components.





126

International Short-Wave

(Continued from page 65)

closedown. (Ridgeway, South Africa) Bruzil-The new Radio Cultura outlet, ZYR57, 9.745, Sao Paulo, can be heard best on Mon. when HCJB, Quito, Ecuador, is absent from that channel; noted with identification 2300. (Niblack, Ind.) Wants reports to Av. S. Joao 1285, Sao Paulo, Brazil. (Villela, Md.) The Brazilian which tested some time ago on 11.855 was an experimental transmitter, PRB4, Radio Club de Santos, Rua Jose Cabalero 60, Sao Paulo, Brazil. ZYR63. Radio Emissora de Piratininga, Praca do Patriarca 26, Sao Paulo. Brazil, operates on 6.025, 50 kw., 0400-2300. (Serrano, Brazil, via Radio Sweden)

Radio Nacional, Rio de Janeiro, is scheduled in Portuguese 0345-1500, 1800-2310 on 9.720; 1703-1937 on 15.295; Spanish at 1400-1420; by this time should also have a service in English. (WRH) ZYK3. 9.565, noted 1705 in Portuguese. (Tonsi, Wisc.) ZYR59, Sao Paulo, A Voz de Sertas, is noted on 3.338 at good level 1830-2100. (Ridgeway, South Africa) PRLA. 9.770, Rio de Janeiro, noted with English session 1700-1800 recently. (Sutton, Ohio)

British Honduras-Radio Belize on announced 4.950 can be heard occasionally in USA with weak to fair signal, much CWQRM and aircraft phone QRM, around 1830-1904A sign-off. Uses English. (West, Va., others)

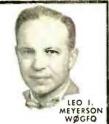
Bulgaria-Radio Sofia, 7.671, announces English for Europe now 1345-1400, 1600-1630 on this channel parallel with 6.070; for North America 2000-2030, 2300-2315 on 9.700 (is slightly lower). (Pearce, England) Noted on 9.700A with good level in the 2000-2030 period. (Lund, Iowa)

Canada - VE9AI, 9.540, Edmonton. Alba., noted at fair level 1845; at 1900 announces for medium-wave CJCA. (Brown, N.Y.) Calgary, 6.030. Alberta. has good signal around 1400; announces "The Voice of the Prairies"; power is listed 100 w. (Gaylord, Washington State) CBNX, 5.970, St. John's, Newfoundland, noted to 2235 sign-off: is in the clear after 2230 when HI4T signs off. (Machajewski. N.Y.)

Cape Verde Islands - CR4RA, 7.112. Praia, noted 1515 with call in Portuguese. (Pearce, England) And signing off 1700. (Saylor, Va.)

Ceylon Radio Ceylon sent these current schedules-Commercial Service 2045-0230, 15.120, 100 kw., English to India, Pakistan; 0730-0830, 15.120, 100 kw., Urdu, Hindi (VOA relay) to India, Pakistan; 0844-1145, 11.975, 100 kw., English to India. Pakistan; 2045-0230, 7.190, 7.5 kw., English to India, Pakistan; 0630-1145, 7.190, 7.5 kw., Hindi (0630-0830), English (0830-1145) to India, Pakistan; 0015-0130, 17.820, 7.5 kw., English to Africa; 0415-0615, 17.820, 7.5 kw., English to Southeast Asia: 0630-0845, 11.975, 7.5 kw., Hindi to

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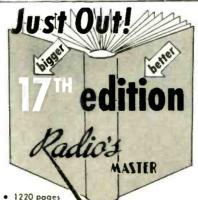
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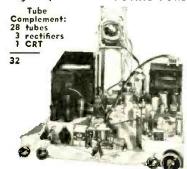
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Chile-CE920. 9.200A, Punta Arenas, has been at fair level recently to 2200A sign-off; slogan is "Radio Militar Austral." CE960, 9.593A, noted around 2000 at good level; announces "Radio La Americana." (Niblack, Ind.) Closes 0030. (Kary, Pa.)

CE1175. 11.73A, noted with powerful signal 2303. (Bellington, N.Y.) CE622, 6.220, Santiago, heard with news in Spanish 2130, then music. (Levy, N.Y.)

China - Radio Peking's 11.69AV channel has been noted with English 1730-1800 again lately. (Niblack, Ind., others) Noted in Britain with strong signal on 15.060AV with English session 0400; announced English broadcasts as 1730 on 6.100, 7.500, 9.040, 10.260, 15.060, 15.170, 0400 on 6.100, 10.260. 11.690, 15.060, and 0830 on 11.690, 15.060. (Pearce, England) Noted on 7.500 early mornings (EST) and evenings to around 2000. (Chatfield, N.Y.)

Schedule received by Scheiner, N.J., from Radio Peking, listed these Peking outlets for use in relay of Home Service — 6.100, 7.500. 9.040, 10.260, 15.170 at 1800-1830, 2100-2150, 2255-0145, 0425-0845, 0900-1300; listed Mukden, Manchuria, on 7.660; Shanghai on 5.985, 6.812; Wuhan on 6.645; Chungking on 6.154, 11.000; Sian on 6.400, 9.480. Rosenauer, Calif., notes slowspeed Chinese 1000 on 6.100, 7.500, 9.035A, 9.435 outlets.

Another Chinese channel noted is 6.05 heard lately after 0400 and as late as 1030 in parallel with 6.105A Peking; 15.060AV and 15.130A are heard in parallel often after 2000. (Balbi, Calf.) Radio Sian, 9.480, is heard at good strength opening 0600. (N.Z. DX Times)

Costa Rica-TIDCR, 9.62, has news in Spanish daily 2350-2400 sign-off, (Bellington, N.Y.)

Cuba - Tests in English around 0030-0130 (at least Sun., Mon., perhaps other days) to learn how well the medium-wave transmitter on 590 kc. is heard in USA, have been carried also on the 11.727A and 6.450 shortwave channels of COCY. (Guentzler, Ohio, others) Asks for reports to CMCY, P. O. Box 770, Havana, Cuba. (Levy, N.Y.)

Cyprus-ZJM6, 6.790, logged 1100-1130 with Arabic music; time signal 1115. (Wada, Japan) Noted parallel recently on 6.12A and 6.168A around 2345 in Arabic. (Bellington, N.Y.)

Dominican Republic - HI2A, Santiago, La Voz de la Reeleccion, opens 0700 with Dominican National An-



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them: is readable to 0745 when begins to fade out; during hours of darkness is usually snowed under by strong QRM. (Kary, Pa.) H18Z, 5.023A, is sometimes intelligible around 2000, but has bad CWQRM, Kary says.

Ecuador - HC1AC, 6.210A, noted with call 2216; nice level; announced "La Voz de La Democracia." (Niblack, Ind.) Excellent opening 0600 with news in Spanish. (Kary, Pa.) HC2BK, listed 4.710 but nearer 4.700A, Radio El Mundo, Guayaquil, is best after 2200 to 2300A sign-off; programs then are entirely musical, with many commercials in Spanish; HC4AS, 4.202, Bahia de Caraquez, is fair to poor daily, with bad CWQRM; has news in Spanish 1945-2000A; mentions "La Voz de las Caras." (Kary, Pa.) HCJB, 11.915, noted at good level 0015-0130. (Lieberman, N.Y.) And to 0300 at good level in Ill. (Gustafson)

Egypt—SUX, 7.866A, sometimes has strong signal 1400-1700; all-Arabic. (Chatfield, N.Y.) At least some days runs to 1800. (Brown, N.Y.)

El Salvador-YSAXA, 11.950, San Salvador. La Voz Panamericana, was audible recently from interception 0945 to past 1200, had sporting event. (Kary, Pa.) YSUA, now on 6.190A, noted to after 2030; should sign-off around 2400. (Stark, Texas)

Ethiopia-ETAA, Radio Addis Ababa, 15.047AV, noted recently 1320-1420 with English recordings of popular music and English announcements; poor level, heavy CWQRM. (Saylor, Va., others) Is heard often in Britain now from 1030A sign-on; some days has religious (missionary) programs in English around 1030-1100; has English news some days 1110A; format is irregular. (Pearce, England)

Finland-Helsinki, 15.190, noted with news 0700, parallel 9.555, 17.800. (Pearce, England) English should be repeated on these channels around 2200.

France-English from Paris is daily 0245, 6.145, 7.240; 1445, 11.970; Sundays only 0800-0900, 7.240. (ISWC, London) Noted on 6.200 at 0200-0300 with musical session, strong level; on 6.145 signing on 0300 with program in French weak. (Chatfield, N.Y.)

French Cameroons Douala sends on 7.287 at 1230-1500 (Sun. also 0500-0800) according to "Malmo DX-aren", Sweden. Not confirmed.

French Morocco-Radio Maroc, 15 Avenue du Congo. Rabat, sent schedule for CNR3, 6.006, 1 kw., as 0200-0330, 0600-1000, 1200-1800 (Sun. 0200-1800). (Kary, Pa.)

French West Africa-Radio Dakar, 9.560, noted opening with French march 0200. (Pearce, England) Current schedule is 11.896A weekdays 0130-0300, 0700-0900, 1400-1810, Sun. 0200-0900, 1300-1810; 9.562A, weekdays 0145-0315, 0730-0845, 1200-1730, Sun. 0430-0845, 1330-1730; news in French on 11.896A at 0230, 0800, 1500, 1800; on 9.562A at 0800, 1700. (WRH) Sometimes opens on 9.560A as early as 0130. (Radio Sweden)

Germany-By this time, the German

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1.5	HY	2.50	21.4	80 ohm.		C:	N N		D												3.7	5
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Short-Wave Overseas Service should be on the air. I hope to have details shortly.

Baden-Baden, 6.320, was noted fair a recent Sat. at 1830 with popular recordings; this extended schedule may be Sat. only. (Kary, Pa.)

Gold Coast-Acra, 4.915, tuned 1230 when had music; 1245 Gold Coast news, followed by weather forecast, then dance music to 1300 closedown with "God Save the Queen." (Pearce, England)

Greece-Radio Athens is now using 9.607 to North America on winter schedule of 2000-2100; English news around 2035. (Bellington, N.Y.) Noted on 7.300 with news in Greek 0215; on 15.345 with light music 0800; heard on 9.607 with news 1430, then news in French 1445. Larissa, 6.745, noted with call 1530, now signs off 1600 (formerly 1500). "Radio Amateur", London, reports a Greek Forces Station at Kozani operating around 7.940-7.950, heard at good level 1300.

Greenland OXI, 9.310A, Godthaab. on a recent Sun, had extended schedule to 2012 sign-off. (Stark, Texas) Normal sign-off is around 1850. (Niblack, Ind.; Kary, Pa.)

Guadeloupe - Basse-Terre, 7.445A, noted at fair level some days shortly before 0600 in French. (Kary, Pa.) May sign on 0530.

Guatemala-TG2, 6.620, logged 2015 in Spanish. (Tonsi, Wisc.) TGZA, 6.675AV, Zacapa, Radio Oriental, is audible to 0805A mornings and to 2210A sign-off evenings; has bad QRM. (Kary, Pa.)

Haiti - The "wandering" 4 V R W, Radio Haiti, has been varying lately around 10.070-10.092A. (Niblack, Ind., others) A badly distorted signal has been noted from a Haiti outlet on 6.230A to 2015 sign-off. (Stark, Texas) 4VEH, 9.685AV, Cap-Haitien, heard signing on 0630. (Chatfield, N.Y.) A letter from Radio Citadelle indicates that power of 4VWA, 6.235, is 150 w. (to be increased to 1 kw.); slogan is "Ici Radio Citadelle, Cap-Haitien, capitale touristique de la Republique d'Haiti." (Kary, Pa.) Is heard to after 0800 and past 1815; may sign off around 2015. (Stark, Texas) 4VPL, 5.902, Petionville, is audible from as early as 1830 to past 2000 with varied musical programs. (Kary, Pa.)

Honduras-HRP1, 6.35, El Eco de Honduras, San Pedro Sula, noted 1715-1730 at fair level in Spanish. (French, Mass.) Good level 2246-2323. (Patterson, Ga.) HRXW, Radio Comoyaguella, noted moved to 6.105 from 8.985A and 6.110; is best after 2200; signs off around 2300. (Stark, Texas, others) At times, HROW. Radio Monserrat, uses both 6.675 and 6.660: noted parallel one night recently past 2015. (Stark, Texas) Signs off around 2130. (Dexter, Iowa) HRLP, 6.410, Tegucigalpa, Radio America, is best prior to 1900 with recorded music and commercials in Spanish; after 1930, signal weakens rapidly. (Kary, Pa.)

Hong-Kong-ZBW3, 9.525, Victoria, noted at good level 0530. (Ballou,

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Calif.) Has been closing lately 1030; has BBC's Radio Newsreel (probably recorded) at 1000 now. (Ridgeway, South Africa)

Hungary-Budapest. 9.833, noted with English to North America 1700-1730, 1930-2000. (Lubell. N.Y.) Should be parallel on 7.222A and 6.240A.

India-AIR, 11.790, noted signing on 2030 with English identification; the 15.160 outlet noted closing down 0730 with English announcement. (Niblack, Ind.) Noted with European Service 1445-1545 now over 11.780, 9.565A, 7.120; asks for reports; heard signing on 1445 on 7.125 with French session, also audible over 5.960: with Indonesian program 1745-1800 on 7.125, 5.960A; with news 0300 on 17.705. 15.160, closing 0330. Bombay, 4.840, noted 1200 with native program, signed off 1230: Delhi, 4.940, strong in native 1200, closed 1330 at end of Persian session, Madras, 4.920, noted with news relay from Delhi 1030. (Pearce, England) Is strong level opening 0830 with news on 11.780. (Brown, N.Y.) Noted with news 0730 on 17.760. (Gillett, Australia)

Indo-China - Radio France-Asie, 9.754A, Saigon, still noted with English session to Europe 1734A-1800; announces next English for 1830 on 7.230; noted on 15.430 with news 0500, closing with "Knightsbridge March" 0513. (Pearce, England) Heard on 11.935 with bilingual (English-French) sessions from 0900. (Ridge-(Continued on page 132)

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RADIO COMPANY, INC. 103 W. 43rd St., N.Y. 36. N.Y. • LU 2-1500 way, South Africa) Radio Hue can be heard in Japan very well but with some hum around 0500-0800 on 7.205; closes 0800 with identification in French. Radio Dalat is at fair strength, sometimes QRM'd by Radio Moscow, on 7.265, closes 0630 daily except Sat. when runs to 0700; has French on Sat. 0630-0700. (Wada, Japanese Short-Waye Club)

Iraq—Radio Baghdad, 11.724A. noted 1145 with Arabic music: at 1200 clock chimes the hour, call, then news in Arabic. (Pearce, England) Should have English 1415-1500A closedown.

Italy — Rome, 9.575A, noted with news to North America 1930, good level. (Niblack, Ind.) Noted on 6.010 in Russian 2215-2245. (Lubell, N.Y.)

Jamaica—Due to requests of listeners. Radio Jamaica has announced it no longer changes from 4.950 to 3.360 at 1515 but remains on 4.950 to 2300 closedown; opens 0600. (Levy, N.Y., others) Station officials list this one as 5 kw., using omnidirectional antenna. (Baitzel, N.J.)

Japan—AFRS, Tokyo. noted parallel over JKL, 9.605, and JKI, 11.825, at 0100. (Stein, Calif.) Good signal over JKL, 4.860, at 0825, moderate fading. (Ballou, Calif.)

Mexico—A Mexican has been noted on 9.575 identifying as "La Hora (Continued on page 137)

Transistor Receiver

(Continued from page 37)

grounded base circuit. The value of R_2 should be chosen so that the collector current is about 1 milliampere. The collector current of the detector/amplifier transistor will depend on the strength of the received signal but will average about 200 microamperes with a strong signal.

Battery life with only one transistor will probably equal the shelf life of the battery. With two transistors, the life will depend on average hourly use but should be at least 100 hours for two penlight type cells.

If magnetic phones are used, they may be connected directly in the collector of either transistor. Low impedance phones or a speaker will require the use of a matching transformer. A load impedance of 2000 ohms in the output stage is correct for the voltage and current indicated.

Alignment is perfectly straightforward but should be done carefully in order to realize maximum sensitivity. Any good service oscillator or signals from broadcast stations may be used to accomplish the alignment. The collector current of the first transistor is a good indication of resonance. The parallel trimmers are used to line the set up on the high frequency end and the slugs on the low frequency end.

The output power of this receiver is about 1.5 milliwatts and is sufficient for adequate earphone volume. An efficient speaker can be connected to the output circuit and adequate volume will be obtained in a quiet location. However, the addition of a class B output stage to drive the loudspeaker is recommended.

The receiver, as originally huilt and as shown in the photos, included a CK705 germanium rectifier and several parts associated with this rectifier. The junction transistors were used as straight audio amplifiers. Tests proved that the diode was not essential and in fact provided no advantage, so the receiver has been modified to the circuit of Fig. 4.

BIBLIOGRAPHY

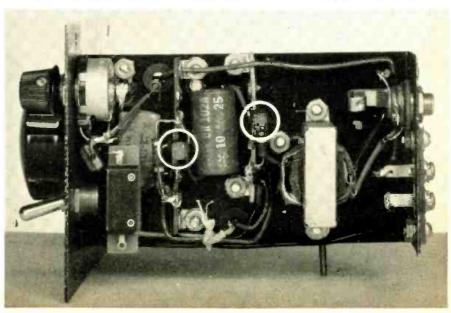
Doremus. John A.: "Point-Contact and Junction Transistors." Radio-Electronic Engineering Edition of RADIO & TELEVI-SION NEWS, April 1952.

Reich, Dr. Herbert J.; "Transistors and Transistor Circuits," Electrical Manufacturing, November, December 1952.

Proceedings of the IEE, Vol. 40, November 1952.



Under chassis view of the transistor receiver designed around the CK722 transistor.



Writing for Profit

(Continued from page 59)

ing time. In addition, there is the real satisfaction of doing creative work.

Articles prepared for the popular technical magazines must still meet reasonable standards of neatness and. to be easily salable, should be prepared with certain basic rules in mind. We will discuss these factors separately.

1, Choose Your Market: Before starting a technical article, decide how the article is to be slanted and to which magazine (s) the article is to be submitted. This will determine the style of presentation and, to some extent, the subject matter. Obtain copies of the magazine and carefully read the majority of articles published. In this way, you can obtain a better insight into the style preferred by that magazine, the types of articles desired, and the general level of writing.

It is a good idea to send an outline of the proposed article to the editor of the magazine before writing the article. If the editor is interested, the chances of selling the finished article are many times better. However, if the editor is not interested in the suggested article, he will often tell why, and may, at the same time, list the type of articles desired at that time.

Most of the technical magazines can be grouped into five general classifications, as follows:

Semi-Technical Magazines: In this group are the very popular "home mechanic" magazines. Articles for these magazines must be extremely simple, should include detailed sketches and photographs, and must be fairly short. Preferred are construction articles on phonographs, radios, amplifiers, "gadgets." and electronic toys.

Technical Magazines: In this group fall the majority of radio, television, and electronic magazines. Articles may range from semi-engineering in nature to simple construction. All phases of the electronic field are covered. However, construction articles, in general, are the most popular. Articles written for these magazines should not be over-simplified, but extensive theory and complex mathematical expressions should be avoided.

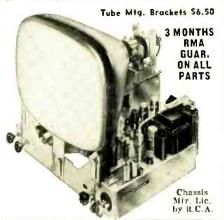
Specialized Technical Magazines: In this group fall a number of magazines designed to appeal to a specific group in the electronic field. There are audio magazines for the audio and high fidelity enthusiasts, service magazines for the radio-TV technician and service-dealer, and amateur magazines for the amateur radio operators or "hams."

Engineering Magazines: Magazines in this group are designed to appeal to practical engineers and, to some extent, to engineering executives. Preferred articles include descriptions of new circuits and specialized electronic equipment, production and management methods, practical design techniques, and new laboratory techniques. NEW 1953 630 FA-2*

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A reasonable amount of math may be included, but it must be remembered that the articles are slanted towards practical men, many of whom don't have time to "wade through" page after page of advanced mathematics.

Professional Journals: Articles or "papers" written for these magazines must be on a high academic level. Considerable math is permitted and often desired. Articles are generally concerned with new developments in fundamental research and, more specifically, with the derivation of new circuits and design methods.

2. Pick Your Subject: The prospective writer should pick a subject he knows well, but also one that will carry appeal to the readers of the chosen magazine. In general, commonplace subjects are to be avoided. While a top-notch author may be able to write and sell an article on "A Three-Tube Phonograph Amplifier," for example, the beginner will stand a better chance if he chooses a less common subject.

Above all, take care not to "borrow" from previously published material. To do so is not only poor taste, but may also be a criminal offense.

It is possible to write a number of articles on the same, or similar subjects, of course, but deliberate copying may cause legal action against the writer.

Timely subjects are especially good. but care must be taken that the material will not become "dated" in a few months. Often, an article may not be published until several months after acceptance. If the material cannot stand a few months' delay in publication without detracting from its interest, there is a good chance the article will not be accepted regardless of the quality or interest of the writ-

When writing for the general technical magazines, avoid subjects appealing only to very limited groups. To use an analogy, don't write articles appealing only to "one-armed paperhangers with red hair."

3. Preparing the Article: Once the possible market (magazine) and the subject have been chosen, the article itself may be written. Here, again. there are certain basic rules to follow.

Some authors work from an outline, preparing first a "rough draft," then second and third drafts and the fina! copy. Others prepare only a rough draft, followed by the final copy, thus permitting the first writing to serve both as outline and rough draft. The author generally prepares final copy directly, working from a preliminary outline.

However, until experience is gained in writing, it is suggested that both an outline and rough draft be prepared before starting the final article.

Avoid superfluous words. While some magazines pay on a "per word" basis, and others on a "space" basis. there is an increasing tendency to pay on the relative merits of the article

RADIO & TELEVISION NEWS

itself, regardless of length. Thus, a well-written 2500 word article on an interesting subject may result in a larger check than a longer and more wordy article on the same subject.

Articles must be typewritten and should be written on plain white 16 lb. or 20 lb. paper. Double-spacing and good margins are mandatory.

While an occasional error and correction in the body of the finished manuscript is permissible, if there are an excessive number of errors, the manuscript should be retyped.

When writing an article, good grammar is important, but letter-perfect grammar is not as important as an interesting and clear presentation of the written material. Thus, a stiff, cold, and very formally written article may stand less chance of acceptance than an easy-to-read and "straight-from-the-shoulder" style, even with an occasional minor grammatical error.

4. *Illustrations:* When writing an article, remember that the final published material should "look good" if the reader's interest is to be held. Page after page of the printed word may become boring.

Illustrations are especially important in the case of construction articles, where both sketches (schematic diagrams) and actual equipment photographs must be included.

In most cases, the magazines prefer to have any final drawings prepared by their own art staff in order to maintain a consistent style and quality. Therefore, schematic diagrams and other drawings may be submitted as pencil sketches. However, care should be taken in preparing the sketches so that the magazine artist or draftsman will have no difficulty in interpreting and redrawing the illustrations.

It is perfectly all right to use a straight-edge and compass to prepare the pencil sketches. An example of an acceptable diagram is given in Fig. 2.

Photographs must be suitable for direct reproduction. Small snapshots are definitely not acceptable to most magazines. Preferred are 7" x 9" or 8" x 10" glossy prints with good contrast. If possible, the photographs should be made by a commercial photographer and prints prepared "for reproduction."

Fig. 1 (right) shows a poor photograph of a small laboratory meter. It lacks contrast, is slightly out-of-focus, and is improperly lighted. Another shot, from the same angle and of the same instrument, is shown in Fig. 1 (left). Notice the superiority of the second photograph.

Avoid writing on or marking the photograph itself in any way. If it is necessary to identify parts or objects in the photograph, do so on a piece of tracing paper laid over the photo and secured to its back with rubber cement or Scotch tape.

5. Submitting The Article: Once the article is finished and "ready-to-go,"



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determine the number of words in the article, and give this information along with the number of illustrations and photographs and the author's full name and address on the title page (even if a pen name is used). Some magazines also like the author's name and the title of the article repeated on each succeeding page.

Mail the article in a manuscript type envelope-don't fold the article and send in a conventional envelope, even if the article is short. Articles should always be mailed flat. If photographs are included, chipboard or corrugated board stiffening should be included to minimize bending or folding.

If the material is a construction article, be sure to include a complete parts list. Any "special" parts should be indicated, along with the manufacturer's name and type number.

A self-addressed and stamped envelope should be included for the return of the manuscript should it not prove acceptable for use. If this is not done, the article may not be returned to the author if rejected.

If the article is rejected, don't be discouraged. It may only indicate that the magazine already has an article on hand covering the same subject. The article may still be submitted to other magazines and may be sold on the second try. Try and try again!

However, don't submit the same article to more than one magazine at the same time. Both publishers may accept the article, resulting in undue embarrassment all around.

Often, the editor of the magazine will send a letter of general criticism on the article. In such cases, revision of the article may turn otherwise wasted work into a salable effort. Accept the criticism in the same good spirit in which it is offered, and profit by the greater experience of the editor.

Good Luck! Probably every technician and engineer in the nation has, at one time or another, completed a piece of work which would be a suitable subject for a technical article. Use that subject, follow the general hints given, and write that technical article!

You will find two thrills awaiting you, and it's difficult to tell which is the greater-receiving that first check in the mail, or seeing your article in print.

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International Short-Wave

(Continued from page 132)

Nacional:" heard from interception 0745 past 0900. (Kary, Pa.) XESC, 15.205, noted 1700 with call in Spanish. (Baitzel, N.J.) XEBT, 9.625. noted around 1300-2100 in Spanish only. (Simpson, Kans.)

Monaco-Radio Monte Carlo noted on the new 7.350 channel (replacing 9.785) in parallel with 6.035 at 0200, strong level in French, commercials interspersed with music. (Pearce, England, others)

Mozambique-The Portuguese Service from Lourenco Marques is noted on 15.285A some days as early as 1515, good level; noted closing 1515 with "A Portuguesa." (Niblack, Ind.) Heard in Britain on this channel from 1045A opening. (Pearce) Lourenco Marques was noted on a channel of 4.825 recently at 1345; was found another day near 4.865 with news in Portuguese 1300, says Pearce.

Lourenco Marques is now on "summer" schedule in English 2300-0200, 11.742, 4.916; 0200-0800, 11.742, 9.766, 7.262; 0800-1200, 11.742, 4.916; 1200-1500. 9.766, 4.916, 3.490; still announces 11.761 but has been measured 11.742; Portuguese Service is 0000-0100, 9.804AV, 4.830; 0430-0630, 9.804-AV. 8.005, 7.216; 1100-1500, 4.830, 15.-285 (Ridgeway, South Africa)

Nicaragua-Granada, 7.850A, heard 1800 with strong signal in Spanish. (Chatfield, N.Y.) YNBH, 6.015. Radio Panamericana, was heard recently around 2215 with news in broken English, interspersed with short musical interludes and short Spanish announcements. (Stark, Texas)

North Korea-In answer to a query by your short-wave editor, Hahn Ki Syun of Radio Korea, Republic of Korca, says the Communist radio at Pyongyang, North Korea, is using frequencies of 970 kc., 1080 kc., 4.440, and 6.230 (varies). Rosenauer, Calif., says the latter channel now appears to be 6.275A, heard 0950 with speech in Korean, good level.

Northern Rhodesia - Lusaka, 4.826, noted 1300 with BBC news relay, signing off 1400 with "God Save the Queen." (Pearce, England)

Norway Oslo, 11.735, noted signing on to South America 1800. (Pearce, England) Heard on 15.175 in Norwegian at 1100. (Hoffman, N.Y.)

Pakistan-Radio Pakistan, 17.715A, noted with news 0330; to Indonesia on 15.270 and 17.835, 0630-0715. (Pearce, England) Latter transmission noted in New York. (Mast) Dacca, 4.807, heard in Britain 1110 with native program, fair level, CWQRM. (Catch) Noted on 9.647A from tuning 0750 to closedown 0815; no English; good signal. (Ferguson, N.C.)

Panama-HOJA. 9.645, Chitre, Radio Provincias, is fair from 0600 past 0700. (Kary, Pa.) HO50, 5.995.5, noted 0558 signing on with S7 signal. (Oskay, N.J.) HOLA, 9.505, Colon, on Satur-



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days has "late dance music" to 0200 (Sun.) (Villela, Md.)

Paraguay—The outlet on 6.270A is best before 2100. (Stark, Texas) Is ZPA1, Asuncion.

Peru—Radio America, OAX4W, 9.405A, was noted a recent Sun. at 2150 with American recordings and announcements in English; mentioned this as a request program; may be weekly feature. (Niblack, Ind.) Heard signing off 0050. (Sutton. Ohio) Radio Nacional del Peru is now using OAX4T, 9.550A, to 1800, then changes to OAX4Z, 6.082A. (Villela, Md.) Latter channel heard closing down 0030 with announcements in both Spanish, English. (Saylor, Va.)

Philippines—Radio Free Asia relay, 6.110. Manila, noted at good level with news 0920. (Balbi, Calif.) Far Eastern Broadcasting Co., 17.805A. Manila. a new channel. noted 0430 with identification in English, wiped out by Rome coming on air 0445; on 11.855 at 1030 with English identification, then "Bringing Christ to the Nations" in native dialects. (Pearce, England) DZH7, 9.73, noted 0750 at excellent level. DZH2, 9.64, Manila, heard at weak level 0452. (Ballou, Calif.) DZI4, 6.110. Manila, noted with weak signal 0613. (Oskay, N.J.)

Portugal—Lisbon, 6.374, noted 1900-2005. (Patterson, Ga.) CSA32, 11.995A, opens 1230 in Portuguese. (Baitzel, N.J.) Radio Sweden says a new transmitter at Coimbra is testing daily 1300-1500 on 7.020A.

Portuguese India — Radio Goa is scheduled 2100-1230 on 6.025, 9.610; has experimental transmissions on 3.425. (WRH) Heard on 9.610 in Hindi 0930; Portuguese 1000; English 1030; has guitar interval signal; closes 1230; good level in South Africa.

Reunion—St. Denis, 7.168, broadcasts 0900-1200 (Wed. to 1330, Sat. to 1400). (1SWC, London)

Sao Tome—CR5SB, 17.683A. is noted Sun. with strong signal 0700-0800, musical session with Portuguese announcements. (Ridgeway, South Africa)

Sarawak — Scheiner, N.J., has received this information direct from the Information Officer, Sarawak Information Service, Kuching, Sarawak: "The broadcasting station here does not yet exist. Our plans are made, our money voted, and the chief members of our staff engaged, but the station will not be completed and in operation before the end of 1953. In the beginning, it will be operated as a department of this office." Promised further information on developments.

Saudi-Arabia—Djeddah, 7.245, noted signing on around 2249 with 8-note signature tone, march, then Arabic music; signal is sometimes S8. (Brown, N.Y.) Noted parallel on 6.102A. (Stark, Texas; Bellington. N.Y.)

South Africa — SABC, 9.870, noted 1400-1500 with English program, fair level; QRM at times. (Chatfield, N.Y.) The African Service is radiated from a 5 kw. post office transmitter of the

radio telegraph station at Roberts Heights, 15 miles south of Pretoria; is beamed northerly 0330-0715 weekdays, 0330-0845 Sat. and Sun. on 15.230; 0900-1130 daily on 11.937, and 1145-1505 over 9.870; English on Tue., Thur., Sat.: Afrikaans, Sun., Mon., Wed., Fri. (Ridgeway, South Africa) Johannesburg is using 9.680 now for its new Southwest African transmission 2345-0130, 0315-0715, 0900-1405 (Sun. opens 0055). (N.Z. DX Times)

South Korea - Wada, Japan, confirms that Seoul's HLKA is using 9.555 in parallel with Pusan's HLKA on 9.735. The latter outlet is noted from as early as 0340 with Western classical music; commentary in Korean 0345, fair signal in Calif., reports Rosenauer. Measured recently 7.9342 by Ballou. Calif. Heard by Balbi, Calif.. from around 0450; cannot hear the Seoul 9.555 channel,

Spain-Radio Mediterraneo, 6.995A, Valencia, noted strong 1315 tune-in. Radio S.E.U., 7.088, Madrid, strong with call 1930, then popular music; La Voz de Falange, Madrid, noted on 7.380A at 1435, still on the air 1535. (Pearce, England) Malaga appears to vary in frequency, is now about 6.960, possibly slightly higher; some days becomes audible as early as 1445. (Kary, Pa.)

Sweden-Radio Sweden, 11.880, noted to North America with English 0700-0715, then in Swedish; heard with English on 9.535 at 2300. (Niblack, Ind.) Heard on 6.065 closing period to North America with English announcement

2000. (French, Mass.)

Switzerland-International Red Cross, 7.210, Geneva, recently was heard with test broadcasts in various languages, including English, at 0130-0230, 1630-1730. (Kary. Pa.; Pearce, England, others) Wants reports.

HER5, 11.865, noted 0945 with music, good level in N. Y. (Hoffman) Heard opening 1015A to Western North America on 9.535 at excellent level, parallel with (announced) 6.165, 7.21, 9.665, 11.865. (Bishop, Ohio)

Syria-Damascus, 11.913A, noted with news, in clear.

1720-1730 sign-off. (Black, Pa.)

Taiwan—BED7. 7.130A, noted at good level 0435 and again 0630. BED29, 6.095, is fair signal around 0630. (Ballou, Calif.) Taipeh is noted on 11.735 in Chinese dialects from around 0830 to 1145 when has bad QRM from Radio Nederland; from 0930, BED7, 7.130A. is in parallel. Is good level in English on 15.235 at 2300-2400 when goes into Chinese. (Ridgeway, South Africa) BEC32. 9.778V, noted 0500 with English program, children's session; BED26, 10.080, heard 0830 with Western music, then Chinese news. (Sanderson, Australia)

Tangier - Radio Africa has returned to 7.126 after a brief move to 7.193A; noted with call 1515. (Pearce, England, others) VOA, 7.215A, noted 0830-0922; news in Arabic 0900; had announcements in English.. (Maynard, Ky.)

Thailand—Bangkok, 7.105, strong 0914. (Ballou, Calif.) Strong signal on 6.24 and 15.625 from 0915 to closedown 1030 when gives call in English, then Thai. (Ridgeway, South Africa) Noted on 11.910A with chimes 0615, then news. (Sanderson, Australia)

Trans-Jordan-Ramallah has ceased broadcasts on shortwave. (WRH)

Trinidad-Radio Trinidad has news 0700 on 9.625. (West, Va.) Sent this schedule—on 9.625, 0430-1515; on 3.275, 1500-2200. (Levy, N. Y.)

Turkey—TAT, 9.515. heard with powerful signal to

North America in English 1815-1900. (Machajewski, N. Y.) Uganda The station projected for Uganda will use 7.5

kw.. to give complete coverage to this Central African eolony; will operate in vicinity of 4.000; will not be completed for about a year yet. (Radio Amateur, London)

Uruguay-CXA10, 11.90A, seems to have settled down on 11.895A right atop Radio Dakar. (Bellington, N. Y.) Noted with strong signal 1850. (Gerran, N. Y.) CXA3 heard on measured 6.0755 at 2125; signed off 2201; announced "CXA3, Integrante de la Radiodifusoras Ariel." (Rastorfer, N. Y.)

USI (Indonesia)—In response to an inquiry, officials of Radio Republik Indonesia, Djakarta, explained-Ambon does not operate on 11.089 or in that vicinity as reported by listeners some months ago, but transmits only on 4.865. A new transmitter of 50 kw. has been put into service with test transmissions on 9.868A (is heard on meas-

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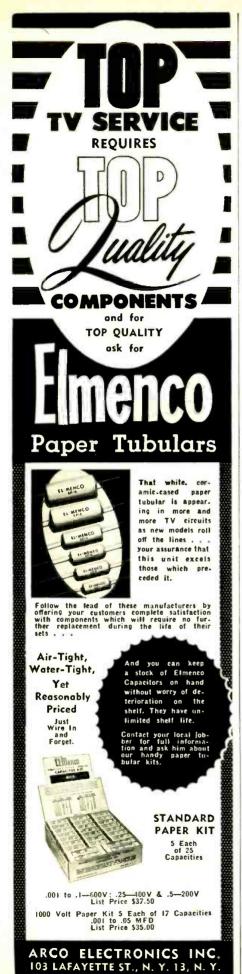
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ured 9.866 at 0430-1030 in parallel with 6.045, according to Balbi, Rosenauer, Calif., others). A service is planned for the whole of USA but when it will be inaugurated is yet unknown. PLB9 and PLQ2, reported heard some months ago, are not stations of Radio Republic Indonesia; officials said these might be amateur stations or stations used by the Post-Telegraph and Telephone Service as transmitters for telephone communications. (Scheiner, N.J.)

YDF6, 9.580. Djakarta, has been heard with "Voice of Indonesia" program in English for Europe 1400-1500, evidently replacing YDF7, 11.770. (Fairs, England, via URDXC) However, may be using both 9.580 and 11.770 at 1400 since Pearce, England, more recently heard this broadcast on the 11.770 outlet; announced three daily broadcasts in English-for 0600. 0930, 1400; announced use of 11.77, 15.15. Radio Sweden says Diakarta has been heard with an English test program on 11.935 at 0630-0725 signoff. Gillett, Australia, notes an Indonesian on 3.960A at 0600 with good level.

Vatican—HVJ, 11.685, noted recently with English 1315-1330. (Niblack, Ind.) Heard signing off on 9.55 at 1615 after 15-minute period in Russian. (Baitzel, N. J.) Noted on this channel with news 1000. (Balbi, Calif.)

Venezuela—Radio Barquisimeto verified reception of 9.510, call YVXJ, by hectograph form letter in Spanish; QRA is Avenida 20 No. 491 (or Apartado Postal 76); listed YVMQ, 4.940, 4 kw., and YVMR, 1490 kc., 3 kw. YVKT, 3.350. Caracas, has newscast in Spanish 1830-1900; one night recently had news in Italian 1900-1915, then news in Portuguese to 1930.

Western Samoa—From 2AP, Box 23, Apia, Western Samoa, Scheiner, N. J., has received word that this (mediumwave) station has two short-wave frequencies. one of which, 6.040, will test soon, but no date could be fixed; 2AP operates on 1420 kc.

Press Time Flashes

Radio Free Europe can be heard at excellent strength 1900 on 9.695 in foreign language. (Niblack, Ind.) Madrid. 15.625, noted with news in Spanish 1146. signing off 1155A. (Pearce, England) Leon, Spain, more recently has been heard on 7.590A concluding relay from Madrid 1625. (Kary, Pa.) A station heard in Arabic on 5.000 around 1340-1403 close (with short band anthem), is probably Al Kuwait, Kuwait, in the Persian Gulf. (Pearce, England)

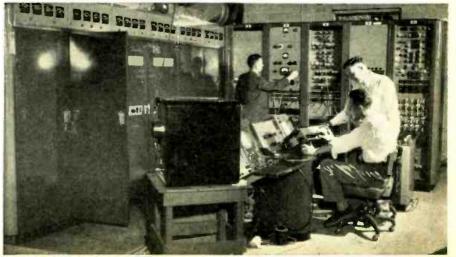
Pearce, England, says he has been unable to log EA8AB, Canary Islands, for some weeks now, although WRH reports it is currently operating on 7.295. Kary, Pa., recently noted this one on 7.305A with bad QRM to 1800 closedown; news in Spanish 1705. The Voice of America, New York 19, New York, has informed Kary, Pa., it is now set up to verify reports on reception of the relay base outlets overseas.

The station manager of mediumwave ZNS, Bahamas, has thanked Kary, Pa., for a report on reception of ZNS on 7.308A, but did not indicate if this is a fundamental operation or a spurious frequency. This one has been heard with weak signal here in West Virginia with BBC relay 1800, then local program from 1815 when gives the time in EST.

Radio Athens, 7.300, more recently has had news 0000. (Bellington, N. Y.)

Emisora Nuevo Mundo, 6.000, Bogota, Colombia, verified with attractive QSL card; listed HJKC, 830 kc., 10 kw.; HJKD, 6.100, 10 kw., and HJKF, 9.520, 10 kw. (Kary, Pa.) A station heard on 7.126A around 0830-0900 with native music is probably Hargeisa, British Somaliland. (Stark, Texas) Is scheduled 0815-0930 according to QSL

The transmitter room of Station KPTV. Portland. Oregon, the first u.h.f. station to go into operation in the country. The transmitter is the same as that used by RCA-NBC at its experimental station in Stratford, near Bridgeport. Conn. At the control desk is Russ Olsen, station's chief engineer. Looking on is Bill McAllister. NBC engineer who helped install the transmitter. Working at the panel in the far corner is Victor Bary, another National Broadcasting Co. engineer.



received. (Radio Sweden) At press time, Radio Jamaica appeared back on 3.360 from 4.950 to 2300 sign-off. (Saylor, Va.) Radio Brazzaville, 11.970, French Equatorial Africa, takes relay from Paris 1445 of English lesson ("The French Have a Word For It"); good strength in Britain. (O'Sullivan) Radio Journal do Commercio, Recife, Pernambuco, Brazil, sent schedule of 15.145, 455-1300; 11.825, 1100-2120; 9.565, 0455-1105, 1300-2120. (Boggs, Mo.) Zurich sunspot prediction for March is 21; for April, 20. (Ferguson, N. C.)

Radio Juventud de Sabadel is on a new channel of 7.312, audible from around 1400. (Buettner, Germany) Direct from Taipeh, Taiwan. comes this current schedule of "Voice of Free China"—2300-2400, 15.235, 11.735, English to USA 0530-1230, 7.130. 11.735, 6.095 (latter 1100-1230 only), to Japan, Korea, Malaya. Chinese Mainland; 1400-1600, BED4, 11.800 (reported "heard," however, on 11.920—K.R.B.) to Europe and the Near East with English 1420-1445. (Kary, Pa.)

The Ecuador station on measured 6.7873 announces as Radiodifusora Costa Azul, Portoviejo, Province of Manabi; noted 2026-0041; the measured 6.8298 outlet announces "Radio Equinoccial," Ibarra, Province of Imbabura. (Rastorfer, N. Y.)

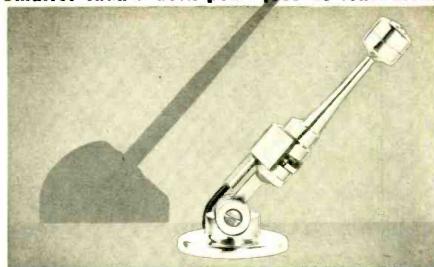
Here is the complete schedule of Radio Pakistan as received by Scheiner, N. J. Service for East and West Pakistan—Karachi, 2125-2300, 5.980; 0210-0230, 15.270; 0230-0430, 9.645; 0730-0810, 7.096.6; 0915-1045, 5.990; 0815-0900, 7.096.6; 2115-2300, 15.335; 0210-0230, 17.710; 0230-0430, 17.710; 0730-0750, 17.835; 0915-1045, 6.945, 9.630.

Zonal Service — Lahore, 2115-2330, 3.915; 0230-0310, 6.138; 0730-0930, 3.469; 0930-1300, 3.469. Dacca. 2000-2200, 4.807; 0100-0130, 7.150; 0600-0800, 4.807; 0815-1130, 3.325. External Services-Karachi, 1430-1515, 6.235, 7.010 in Turkish Service; 1515-1600, 6.235, 7.010, to United Kingdom; 2015-2100, 11.885, 15.335 to Southeast Asia; 2315-2400, 17.750. 15.335 to East and South Africa; 0445-0530, 9.645, 15.335 to South Asia; 0630-0715, 15.270, 17.835, Indonesian to Indonesia; 0830-0915, 9.630, 9.645 Burmese to Burma; 1100-1200, 6.235, 7.010. Afghan-Persian program; 1210-1230, 6.235, 7.010, General Overseas Service (slow-speed news in English); 1230-1315, 6.235. 7.010, Iranian Service; 1315-1415, 6.235. 7.010, Arabic program; power for Karachi was listed 50 kw., for Lahore, 300 w., for Dacca, 7.5 kw. To East and West Pakistan uses English, Urdu, Bengali, Sindhi, Kashmiri, Baluchi, Gurati, Pushto; Lahore uses English, Urdu, Punjabi; Dacca uses English, Urdu, Bengali.

Acknowledgment

Thanks for the fine reports. Just keep them coming to Kenneth R. Boord, 948 Stewartstown Road, Morgantown, West Virginia, USA. Good listening! K.R.B.

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14 mc. Rotary Beam

(Continued from page 68)

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$$Z_T = \vee Z_L \times Z_R$$

For example, if a 300-ohm transmission line were used with the 3-element array, then

$$Z_T = \sqrt{300 \times 10} = 54.8$$
 ohms.

In this case, 52-ohm coaxial cable could be used.

The actual physical length of the quarter-wave transformer is not ¼ wavelength, but is somewhat shorter due to the "velocity factor" of the particular cable used. Most manufacturers give this "velocity factor" in the data for their cable. Using this figure, the following equation may be used to calculate the actual physical length required for the transformer:

$$L = \frac{KV}{f}$$

where: L = length in feet of the transformer.

K = a constant, 246,

V = velocity factor of cable used for transformer.

f = resonant frequency of the array in megacycles.

The RG-11U cable used has a velocity factor of 0.65; the length of the transformer, therefore, was:

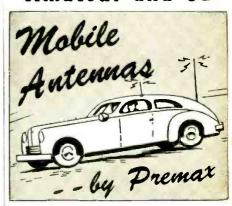
$$L = \frac{246 (0.65)}{14.25} = 11.2 \text{ feet}$$

A further improvement may be made by using a shielded cable such as "Twinax" for the transformer. With such a cable, a capacitive unbalance to ground does not occur when the transformer is run up inside the metal pipe shaft. The cable length within the shaft of the array should be kept to a minimum if conventional coaxial cable is used.

The standing-wave ratio of the transmission line is about 4:1. This is negligible for the 600-ohm line, but it must be remembered that the power carried by the quarter-wave transformer would then be quadrupled. It is important to select coaxial cable

PC	LYST	TYRE	NF -	
ROD -		or 48 "		hs
Dia. 12"	48"	Dia.	12"	484
1/8" \$.03	\$.12	3/4"	.80	3:20
3/16" .06	.24	1"	1.55	6.20
1/4" .10	.40	1-1/8"	2.00	B.00
5/16" .16	.64	1-1/4"	2.30	9.20
3/8" .21	.84	1-3/8"	3.00	12.00
7/16" .30	1.20	1-1/2"	3.30	13.20
1/2" .40	1.60	1-3/4"	4.50	18.00
5/8" ,57	2.28		5.90	23.60
SHEET-m	asking	paper	both s	sides.
Thickness	Si		Price	
1/16"	12" x		\$2.50	
3/32"	12" a		2,75	- 4
1/8"		12"	3.00	
3/16"	12" x	12"	3.75	
1/4"	12" x	12"	4.60	
1/16"	12"	24"	4.90 5.25	
1/8"	12"	24"	5.90	
3/16"	12" :	24"	7.25	
1/4"		24"	8.25	
1/32"	20" >	20"	7.75	
1/16"	24" x		9.50	
3/32"		24"	10.25	
3/16"	24"		14.00	
1/4"		24"	16.00	
5/16"	20" ;	20"	14.50	
3/8"	20" 1	20"	16.00	
3/8"	24" 1	24"	23.75	
1/2"		20"	21.50 31.88	
5/8"	20" 1		34.50	
1/4"	20"	20"	41.00	
1"	20"		55.50	
TUBING	_ 12	" or 48		gths,
O.D.	1.D.	12" lgth.	48" 1gt	h.
1/4"	1/8"	\$.07	\$.28	
5/16"	3/16"	.10	.40	
3/8"	1/4"	.13	.52	
1/2" 5/8"	3/8"	.18	.97	
3/4"	5/8"	.29	1,18	
1"	7/8"	.38	1.52	
1-1/2"	1-1/4"	1.13	4.5	
2"	1-3/4"	1.50	6.0	,
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for the transformer which will carry the power required. The approximate power in the cable may be determined by assuming a final class C amplifier efficiency of about 75 per-cent. In the array described, therefore, the power would be 600 x 0.75, or 450 watts. With a standing-wave ratio of 4:1, however, there would be 1800 watts of power being carried by the coaxial cable, as well as by the 600-ohm line.

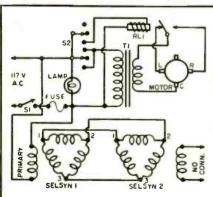
The fundamental reason for a mismatch which creates standing waves is that the transmission line is not terminated in a pure resistance. Mismatch may be caused by a radiator cut to the incorrect length, by nonsymmetrical transmission lines, by unbalance to ground along the line, or by an incorrectly tuned quarter wavelength transformer. If the radiator is cut accurately according to the equation given previously, and if the transmission line is mounted symmetrically and kept at least a few feet away from metallic objects, this loss due to mismatch may be neglected for all practical purposes.

The 600-ohm transmission line was connected to the 75-ohm, quarter-wave matching transformer by means of slip rings. A set of slip rings was mounted on the shaft of the array with brass brushes (1/8" diam. rod stock) connected to the 600-ohm line making contact with the rings. The 75-ohm coaxial cable which runs up the center of the shaft connects to the inner surface of the rings, thus making possible continuous rotation in either direction.

Electrical Controls

As mentioned previously, a propeller-pitch control unit is used to rotate the described 20-meter array, These rotator units come complete

Fig. 8. Wiring diagram of 14-mc, beam rotator and selsyn-indicator systems.



S.p.s.t., 125 volt, 10 amp. switch -D.p.d.t., 125 volt, 3 amp. switch ("center off")

Trans. 117 v. primary, 50-60 cycles, 10-

20 v. sec. @ 10-15 amps. RL,-S.p.d.t. relay, normally closed, 15 amp. contacts, 117 >. a.c. coil.

Lamp—117 v. pilot lamp (see text)

Motor*—Propeller-pitch type motor (see text)

Fuse—125 v., 5 amp. "Slo-Blo" type Selsyns (2)—117 v., 60-cycle type. Lower-voltage surplus types can be used (see text).

*Note: The motor will have four connection terminals. Consult the instruction sheet supplied with the motor to determine which three of the terminals to use for this application.

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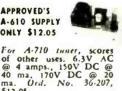
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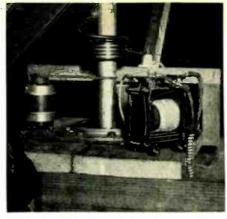


Fig. 9. Side view of the rotator mechanism. showing the indicator selsyn, the motor transformer, and the coaxial matching section entering the pipe shaft.

with motor and gear box and are ideal for this purpose. They are presently selling for about \$15.00 and are well worth it.

The simple electrical system employed with the rotator, as shown in Fig. 8, consists of a d.p.d.t. switch, normally open in the center position, a 10-to-20-volt, 15-ampere transformer, and a s.p.s.t. 110-volt a.c.-operated relay, normally closed, with contact points capable of making and breaking a 15-ampere circuit. BX cable was used for all the wiring shown in Fig. 8.

The transformer and relay were mounted as close to the motor as possible to provide for short leads in the motor circuit. The switch, S_1 , fuse, and lamp were mounted together near the beam-heading indicator shown in Fig. 6. The lamp is used to light the beam-heading indicator, which can be a compass card or great-circle map, so the lamp can be of any convenient size and brilliance. The switch S_2 was mounted at the operating position for convenience.

Selsyn #2 was mounted upright near the shaft of the array and coupled to the shaft by means of a rubber belt, as shown in Figs. 2 and 9. The pulley for the selsyn is a 1-inch length cut from the pipe shaft, thus providing a 1:1 ratio. Gears may be used to couple the shaft of the array to the selsyn, but this method is much more expensive and is not necessary. Although some error may be introduced due to slight differences in the circumferences of the shaft and the pulley and to slippage, this error can be kept to a minimum by rotating the beam backwards to return it to its final position of rest. To keep the array properly oriented, the beamdirection indicator should be marked with a small arrow to indicate the position of rest.

You will notice that the primary of only one of the two selsyns was connected to the a.c. line. The other was left "floating." Both primaries could have been connected, but it was unnecessary since no appreciable power was needed to drive the arrow on the indicator map or compass card. If both are connected some fussing with phas-

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ing may be required, although this amounts to reversing one set of primary leads. It does not matter which selsyn has its primary energized. It was convenient in this case to connect selsyn #1, at the indicator position, to the 117 v. line, as a handy outlet was already there.

The selsyns used in this system have 117-volt primaries. The low-voltage selsyns being sold on the surplus market may be substituted by using a suitable voltage-dropping arrangement, preferably a transformer.

Final Assembly

When the rotator was in place, and all the electrical wiring had been completed and tested, the final assembly of the beam was made. The array had previously heen assembled on the ground, balanced, and then disassembled. The following method was used to transfer the array to the rooftop and re-assemble it:

1. The 1½-inch pipe shaft was placed in the roof bushing, and the rotator platform was shifted until the threaded end of the shaft could be screwed into the flange at the rotator. The rotator platform was then fastened into position with wood screws.

2. The coaxial-cable matching transformer was inserted into the shaft, as

shown in Fig. 4.

3. The slip rings and selsyn belt were attached to the shaft from inside the attic, and the shaft was screwed into the rotator flange.

4. The boom was transferred from the ground to the roof peak by means of ropes, and was temporarily held in position.

5. The 11/2-inch pipe guy-wire support with all six guy wires attached was transferred to the roof, and the guy-wire pipe flange and boom were fastened in place on the shaft flange by means of four bolts, as shown in Fig. 4.

6. The radiator assembly, director assembly, and reflector assembly were transferred to the roof peak and bolted in their proper positions along with

the 1" x 2" side pieces.

7. The guy wires were connected as shown in Fig. 5, and were adjusted until the entire array was parallel and squared away.

8. The entire array was rotated by hand until the threaded end of the shaft began to tighten at the rotator flange; the shaft was then pulled up with a large pipe wrench from the attic.

9. The array was synchronized with the indicator needle. When a great circle map is used, it should be remembered that north is geographic north, and not magnetic. When the array had been adjusted for true north, the needle of the indicator was set to north by slipping the belt on the shaft of the array.

10. The array was rotated continuously in both directions several revolutions from the operating position to make sure that everything was posi-

tioned correctly.

February, 1953



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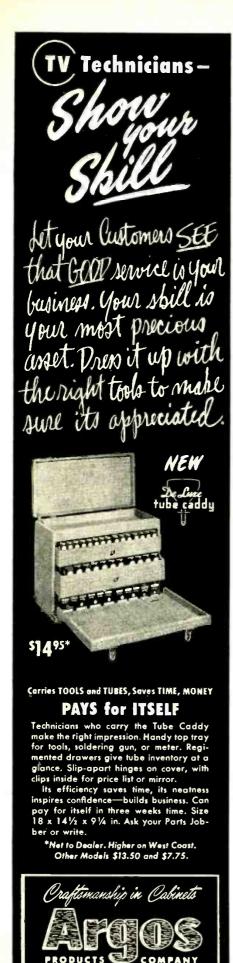
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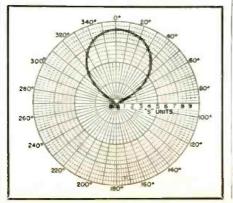
The array may be tuned with the aid of a field strength meter or a receiver with an "S" meter. When the field strength meter was used, it was placed several wavelengths from the array and turned so that the back of the array was facing the meter. The transmitter was connected to the array, and its frequency was tuned to the frequency of the array. With as small an input to the transmitter as possible, the field strength meter was tuned to the operating frequency. The shorting bars of the director and the reflector were adjusted to the position corresponding to the minimum reading at the field strength meter. The director adjustment is more critical than the reflector adjustment, and should be made carefully. This method of adjustment tunes the beam for maximum front-to-back ratio. If maximum forward gain is desired, the array is pointed toward the field strength meter and the stubs are adjusted for maximum field strength.

The pattern for the array, shown in Fig. 10, was obtained with the aid of W2GMN, Fred C. Read. With full input to the transmitter on phone, the array was pointed toward Fred's receiver, located two blocks away. The receiver "S" meter was set to S9, and the reading was recorded. Readings were taken at every 10-degree rotation point, and were transmitted back to the author by means of 40-meter c.w. The entire procedure was repeated several times to check the readings.

Conclusion

As stated at the beginning of the article, the main purpose of building the rotary-beam antenna was to be able to work DX; this antenna has certainly accomplished this goal. To present a clearer picture of the improvement that resulted, it might be worthwhile to look at the record. During the years 1949, 1950, and 1951, 860 DX calls were made and 413 replies were received. The percentage of replies, therefore, was 48. During a previous two-year period, a 66-foot "zepp" antenna showed a reply percentage of 25. while a 33-foot "zepp" showed a reply percentage of 18. The two "zepp" antennas were at the same location as the beam antenna, were

Fig. 10. Field pattern of the 3-element beam, showing high front-to-back ratio.



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.30	watt	ohms:	100-250	0.530	0-18K				22	ea.

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RADIO & TELEVISION NEWS

of the same height, and were fed by the same 600-watt transmitter. A further comparison shows that about 75 per-cent of the DX calls made with the "zepp" antennas were Canadian and Central- and South-American stations within about 2000 miles, whereas the calls made with the beam antenna included stations from all over the globe.

Spot Radio News

(Continued from page 18)

areas. In Ceylon, batteries are also charged at central stations and are often transported to different sites by motor vans and laborers. Access to most of the sites is often through thick jungles, an arduous task involving up to four days of travel just to replace a single battery. And at this time, this antiquated method of providing radio reception is still in use.

ON A 210-acre site directly south of Boulder, Colorado, near the campus of the University of Colorado, the Bureau of Standards has begun construction of a \$4,500,000 lab, to conduct research on the propagation of radio waves and on the expanded utilization of the spectrum for FM, television, facsimile, and radar.

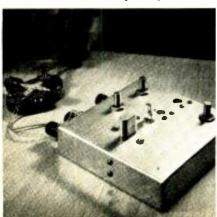
The building will house a staff of about 500, including scientific and clerical personnel, whose efforts will not only be directed to specific problems of research, but to key problems posed by the Defense and State Departments as well as the FCC, for the benefit of the nation and Mr. and Mrs. America. L.W.

TRANSISTOR TRANSMITTER

GEORGEM.ROSE, K2AH, an RCA development engineer, was the principal in an "historic ham first" when he built and successfully transmitted v.h.f. signals over a transmitter based on a single RCA point-contact transistor.

Mr. Rose's equipment was used to contact three ham stations in New Jersey, one 25 miles away.

Over-all view of the home-built transistor transmitter constructed by George M. Rose.



ARB NAVY RECEIVER

105 to 9050 KC. Four Bands, Calibrated Dial, LF-Ship-BC—80 & 40 Meter—Complete with Tubes and Dynamotor. For 21 Volt operation: easily converted to 110 V—12 or 6 Volt. Size: 814 × 784 × 1514 Used: \$20.05

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R.N. Jan. '49) Complete w Tubes, NEW\$4.95
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LANGE TYPE: 110 CFM 34" intake. 21" Dis.

FLANGE TYPE: 140 CFM. 31/2" intake; 21/2" Dis. Complete size: 71/2" W x 71/4" H x 63/4" D. Order No.

FLANGE TWIN: 275 CFM. 41/2" intake: 314" x 3" Dis. Complete size: 113/4" W x 83/4" H x 8-1/16" D. Or-der No. 2C069 \$21.95

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6—24—or 30 Volt 8 Amp		
Two 12 V. 4 A. windings, gives 12 V. 8 A. or 24 V. 4 A		
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175-0-175 V. 40 MA—6.3 V. @ 2.4 A; 6.3 V @ .6 A;Halfshell 2%"x2 3/16"x2%—No. T-23-40 1.75		
350-0-350 V. 90 MA—6.3 V. @ 3 A; 5 V. @ 3 A; Upright—31/6"x31/6"		
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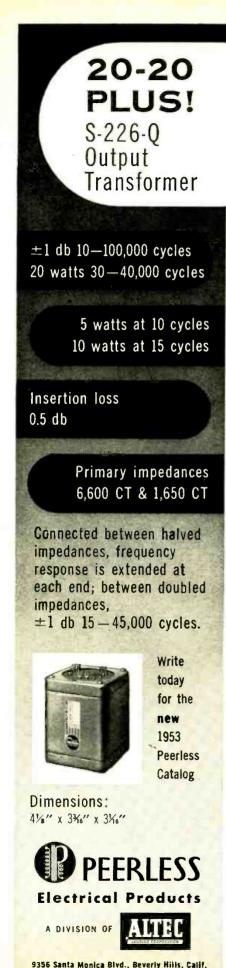
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Current TV Topics (Continued from page 51)

tube receives the video signal and the cathode is at a d.c. potential determined by the brightness control. Therefore a positive pulse must be applied to the cathode and this pulse can be obtained either from the plate of the vertical output tube or from the low side of the deflection yoke. R_1 is used to reduce the amplitude of the pulse to avoid interference with either the sound or synchronizing sections. The leads from the vertical section should be short and kept far away from either the sound or synchronizing circuits.

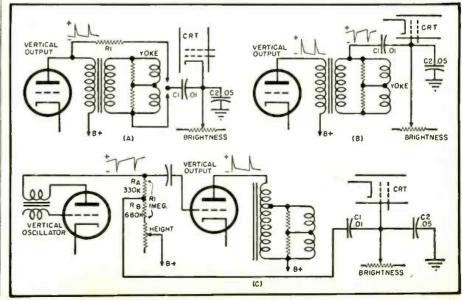
Where the cathode receives the video signal, the circuit of Fig. 4B is suggested. In many sets this circuit is not possible because instead of a regular output transformer an autotransformer is used. This means that only positive polarity pulses are available at the output section which cannot be applied to the picture-tube grid. An alternate scheme is shown in Fig. 4C, where the negative pulse is obtained from the output of the vertical oscillator. The pulse amplitude usually is no more than about 50 volts peak and it is therefore possible to tap down on the oscillator plate resistor R_1 by substituting a 330,000 ohm and 680,000 ohm (R, and R_B) for the original 1 megohm value. This avoids loading down the oscillator and keeps the signal on the output tube substantially unchanged. In Fig. 4. the coupling condenser, C_1 , is given as .01 µfd. because this is a good value for most cases. In order to get sufficient blanking in some sets it may be necessary to increase this condenser to .02, .05, or even .1 μ fd. On the other hand it may be necessary to reduce the blanking pulse if the top or bottom of the picture appears darkened. Reducing either the condenser to .005 μ fd. or connecting a 10.000 to 100,000 ohm resistor in series with it usually achieves good, even blanking.

Foldover

Until the latest TV models came out, quite a few sets were plagued with horizontal foldover. The technician will by now be quite familiar with the complaint: part of the pic-ture appears folded back on itself at either edge. Adjustment of the various horizontal controls sometimes reduced this trouble, sometimes it was removed by extending the picture beyond the edge of the mask and occasionally, incorrect centering hid it. It was soon recognized that in most cases the trouble could not be corrected by the technician but was due to the circuits and components used. The main drawback of the new high-efficiency flyback transformers was their excessive retrace time which caused most foldover. Fig. 5A shows the relation between the horizontal sweep, the retrace of this sweep, and the horizontal blanking pulse which is part of the video signal. As shown, the foldover will appear at the righthand edge of the picture. In reality, the length of the line is much greater than shown in the diagram and the duration of the retrace period proportionally much smaller, but for illustrating the idea this relation was chosen. From Fig. 5A, we see that the retrace period of the sweep is longer than the picture tube blanking. To reduce the retrace time of the sweep would often require a complete redesign of the horizontal deflection section. As a matter of fact most late model receivers use autotype flyhack transformers in which retrace periods are much shorter and foldover does not occur.

For the technician faced with the

Fig. 4. Three basic circuits for blanking vertical retrace lines. (A) Circuit in which the grid of the picture tubes receives the video signal and the cathode is at d.c. potential as determined by the brightness control. (B) The circuit to be used where the cathode receives the video signal. (C) Alternate circuit for use when the negative pulse is obtained from the output of the vertical oscillator.



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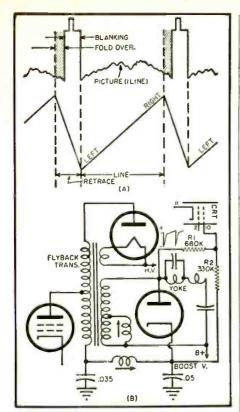
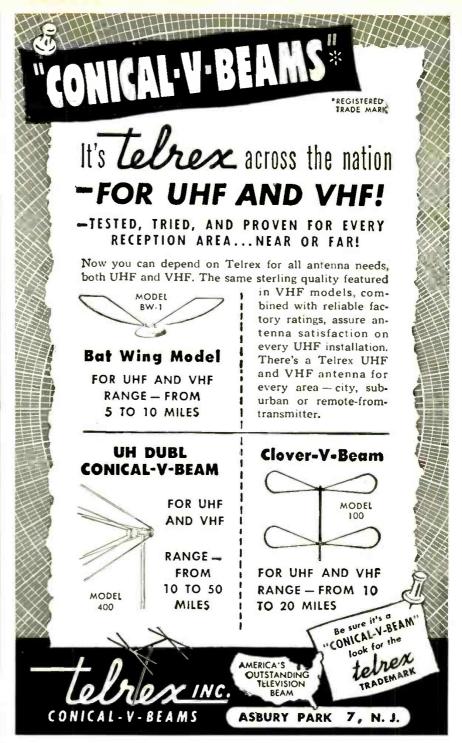


Fig. 5. (A) Relation between the horizontal sweep, the retrace of this sweep, and the horizontal blanking pulse. (B) A simple scheme for extending the blanking period slightly so as to cut off the picture tube during the entire retrace period.

problem of foldover due either to a flyback replacement, big screen conversion, or any other reason, it is only necessary that the blanking period be extended slightly so that the picture tube is cut off during the entire retrace period. Fig. 5B shows a fairly simple and popular scheme for accomplishing this. To get a blanking pulse of the same length as the retrace time, the actual flyback pulse from the flyback circuit is used. To avoid interference with other circuits this pulse is applied to a normally passive picture tube element, the first anode or accelerator grid. This anode is usually at the highest available "B plus" value, the boost voltage from the flyback circuit. A strong negative pulse makes the first anode less positive and thereby cuts off the tube. Such a pulse, ranging up to 2000 volts, is present at the deflection yoke-transformer junction. A portion of this pulse is applied to the first anode through the voltage divider R_1 and R_2 . The values shown for these two resistors were found to work in many cases, but are not absolutely the hest in all sets. If the foldover does not completely disappear, R2 should be increased. If either side of the screen appears darker than the rest, R1 should be increased. A combination of resistor and condensers could also be used, but this introduces additional problems such as waveshape voltage rating, etc.

Installation of U.H.F. Strips

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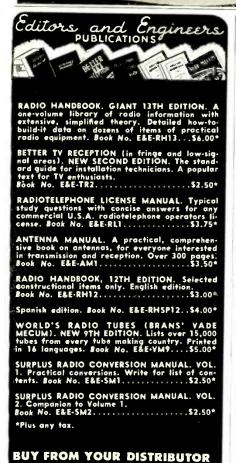
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u.h.f. stations many technicians are confronted with the problem of converting existing v.h.f. sets to receive the u.h.f. channels. In the June and July 1952 issues of Radio & Television News various u.h.f. conversion methods were shown. Since then some of these units have been installed and a certain number of difficulties were encountered. The major problem lies in the double superheterodyning used by most u.h.f. tuners. This requires that the u.h.f. station signal beat with the local u.h.f. oscillator to produce a first i.f. corresponding to one of the v.h.f. channels. The regular v.h.f. tuner contains another oscillator which beats with this first i.f. to produce a second i.f. signal, usually in the 22 to 26 mc. range. In intercarrier receivers a third i.f. signal is obtained at the second detector when the sound and picture carrier beat to produce the 4.5 mc. FM sound signal. It becomes apparent that with two oscillators and three i.f. signals the chances for unwanted beats are quite great and indeed this has been one of the major drawbacks of the double superheterodyne system.

Another source of trouble is from v.h.f. stations adjacent to the v.h.f. channel which now carries the first i.f. signal from the u.h.f. transmission. A good example is the case where Channel 8 is used as the first i.f. to receive the beat from a u.h.f. station and the local u.h.f oscillator. Assume now that a strong local station exists on Channel 7. Under normal conditions the sound from Channel 7 might come through on Channel 8, but since no station is located there, this does not matter. Now, however, the sound from Channel 7 can interfere with the u.h.f. station if it reaches the v.h.f. funer.

There are a large variety of frequency combinations where such troubles can be expected. To complicate matters, many v.h.f. tuners can be modified by means of added u.h.f. strips. Such strips were described in detail in the June issue. Fig. 3 shows one set of strips for the Standard Coil tuner. In this system the local v.h.f. oscillator is tuned to a predetermined v.h.f. frequency, its output passed through a crystal which generates harmonics and either the second or third harmonic is then used to beat the u.h.f. station signal down to a v.h.f. channel. Basically the same scheme is used by Zenith and other manufacturers who supply tuning strips to adapt the v.h.f. tuner for u.h.f. By adding these strips no provision is made to exclude unwanted v.h.f. signals which could readily interfere with the u.h.f. station. Thus the chance for v.h.f. interference is considerable in such installations. Most u.h.f. converters use a special hi-pass filter preceding the tuner to prevent v.h.f. interference.

The best method found to date for dealing with such v.h.f. interference is the use of either a suitable wave trap or else a shorted half-wave or open quarter-wave transmission line tuned to the offending channel. In

each individual case it will be necessary to adjust and experiment somewhat before an acceptable solution is found. In order to remove unwanted beats, the offending signal must first be located and this is best done by substituting a generator for either of the two oscillators or else by using a wavemeter to determine the frequency of the beat signal. The cure is to shift the frequency of either of the two oscillators and in this connection it might be suggested that the u.h.f. oscillator be left alone. Where the strip type of conversion is used the frequency of the basic oscillator can be varied by means of the fine tuning control. A 1-mc, variation of the fine tuning control may mean a 2- or 3-mc, variation of the u.h.f. harmonics, shifting the entire beat sufficiently. The only drawback to shifting oscillator frequency at any time is that it also affects the r.f. passband and, more important, the i.f. section. It is often possible to shift the entire i.f. section by 1 or 2 mc, without substantially changing its characteristics.

Many more u.h.f. conversion troubles are bound to occur and solutions to each of them will, in due time, be found. New u.h.f. techniques, new u.h.f.-v.h.f. tuners and completely new i.f. systems will be developed, but at present the TV technician in a u.h.f. area will have his hands full. A knowledge of the various stations, u.h.f. oscillator, v.h.f. oscillator, v.h.f. oscillator, v.h.f. end their possible beats will be a great help in correcting this type of interference.

In preparing a chart showing such frequencies it should be kept in mind that each time two different frequencies are mixed, four different frequencies are obtained, the two original ones and the sum of both and the difference of both. Local oscillators in the v.h.f. band are usually operated above the incoming signal, but for u.h.f. they are often set below the u.h.f. station signal. When all these possibilities are noted and the frequencies of local v.h.f. stations considered, most of the likely beats and interferences can be anticipated. -30-

HAM CONTACTS

THE FCC has recently warned that American amateurs are forbidden, in accordance with international agreement, to contact foreign stations whose governments prohibit their amateurs from working stations outside their country. Governments currently making this prohibition are Austria. Cambodia, Indonesia, Iran, Viet Nam. Laos, and Thailand.

U. S. hams are also required to comply, when working VK (Australian) DX, with an Australian regulation restricting Aussic hams to sending and receiving only experimental data and remarks of a purely personal nature

The Commission stresses that this list is not to be confused with one published last Spring of countries which permit outside contacts but forbid their hams to handle international third-party traffic.



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1A6G	.59	5W4	.50	68G6G	1.25	606	.63	1908	.70
1A7GT	.47	5 X 4	.40	6BH6	.46	608	.61	1978	.79
1AB5	.59	5Y3G	.32	6B16	.39	6V6GT	.39	1978	.89
1B3	.65	5Y3GT	.32	6BK7	.59	6W4GT	.44	24A	.63
185	.59	5Y4G	.35	6BL7	.59	6W6GT	.44	25AV5	.83
1B7GT	.59	5Z3	.46	6BQ6GT	.59	6X4	.37	25BQ6GT	.62
1C5GT	.43	6A3	.59	6C4	.37	6X5GT	.37	25L6GT	.39
1 E 7	.29	6A7	.59	6C5GT	.39	6Y6G	.48	25Z5	.40
1H4G	.48	6A8	.62	606	.58	7A4_	.47	25Z6GT	.37
1H5GT	.40	6AB4	.44	6CB6	.44	7AF7	.53	25W4	.56
1G6	.60	6AG5	.43	6CD6G	1.11	7B4	.44	26	.45 .39
1L4	.46	6AJ5	.90	6D6	.45	7C6	.40	27	.89
1LC5	.51	6AK5	.75	6E5	.48	7E6	.49	32L7	.40
1N5	.46	6AL5	.38	6F5GT	.39	7 X 7	.70	35B5	.39
1P5	.57	6AQ5	.39	6F6	.37	12ALS	.37	35C5	.41
1Q5	.58	6AQ6	.37	6G6G_	.52	12AT6	.37	35L6GT 35W4	.37
1R5	.45	6AR5	.37	6H6GT	.41	12AT7	.56	35W4 35Z4	39
155	.39	6ASS	.50	6J5GT	.37	12AU6	.38	35Z5GT	.37
1T4	.45	6AT6	.37	616	.52	12AU7	.43	36	.60
1T5	.53	6AU6	.38	6J7G	.43	12AV6 12AV7	.39 .59	41	.42
104	.45	6AV5	.83	618	.69			42	.42
105	.39	6AV6	.37	6K5	.47	12AX4 12AX7	.48	43	.55
1 X 2	.63	6AX4	.53	6K6GT	.37 .44	12AZ7	.69	45	.55
2A3	.70	6B4G	.64	6K7		12BA6	.38	5085	.39
2X2	1.50	6B5	.64	6L6	.64			50C5	.39
3A4	.45	6BA6	.39	697	.45	12BD6	.45	50C6	.59
3E5	.46	6BA7	.57	654	.38	128E6	.39		.41
304	.48	6BC5	.44	658	.53	12BF6	.39	SOLEGT	
3Q5GT	.49	6BD5GT	.59	6SA7GT	.43	128H7	.63	50Y7	.50
354	.46	6BD6	.45	6SD7GT	.41	12J5GT	.42	70L7GT	1.09
3V4	.47	6BE6	.39	6SF5GT	.46	12Q7G	.39	75	.41
				6SG7GT	.41	1258	.70	76	.44
				6SH7	.73	125A7GT	.44	77	.57
				6SJ7GT	.41	12SG7GT	.52	78	.47
				65K7GT	.41	12517	.44	80	.35
				6SL7GT	.48	125K7GT	.48	83	.68
				65N7GT	.52	125L7GT	.47	85	.59
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V.F.O. Multiplier (Continued from page 53)

gang may be used for S_{10} . The underside of the first gang is located just about right for Sin. Sia can be the top half of the first gang (looking at it from the underside of the chassis).

After all wiring has been completed, the unit can be connected to a suitable power supply for initial testing and adjustment. The first step is to check all voltages at the tube sockets. If these are correct, the v.f.o. trimmer can be adjusted so the y.f.o. will cover the proper range. It should tune over the entire amateur 80-75 meter band with some extra room at each end. A communications receiver makes an excellent monitor to check output from the v.f.o.-multiplier unit. The v.f.o. tank coil slug was left all the way in on the original model. After the v.f.o. tuning range has been set, a little preliminary adjustment of the broadband couplers should result in settings which show resonance at the lower end of the 80-75 meter bands. as indicated by a small neon light touched to the "hot" side of each trimmer. The keying lead is grounded for all these preliminary adjustments.

The next step is to check for parasities, and the keying lead should be left unconnected for this. No spurious oscillations from the v.f.o.-multiplier unit should be heard over the entire range of a communications receiver that tunes from 540 kilocycles to 30 megacycles or more. A check should be made with the bandswitch in each of the five positions. The only parasitic oscillation found in the original model was removed by inserting the 500-ohm resistor, $R_{\rm i}$, in the grid lead of the second multiplier tube. If other parasitics are found they should be traced to their source and eliminated before proceeding any further.

Some check should be made on the frequency stability of the unit. Frequency drift due to changing temperatures can be minimized by the use of a proper value of negative-temperature-coefficient condenser in parallel with the v.f.o. tank coil and tuning condenser together.

The third step in adjusting the multiplier unit requires the use of an experimental grid circuit exactly like the one into which the multiplier will work. Plate and screen voltages need not be applied to the experimental stage, but some means must be devised whereby the rectified grid current in that stage can be read with the tube heater lighted. This may be a low range d.c. milliammeter in series with the grid choke, or it may be a 0-200 volt d.c. voltmeter connected across a 50,000 ohm resistor which has been placed in series with the grid choke. The output of the multiplier is connected to the grid of this experimental stage through a 50 µµfd. mica trimmer. The trimmer is set for maximum capacity.



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Set the bandswitch in the fifth nosition, and tune the v.f.o. so a signal is heard on a communications receiver with its dial set at 14 megacycles. Then adjust C_{12} and C_{13} for maximum grid current. Then set the v.f.o. so a signal is heard at 15 megacycles. Adjust C15 and C22 for maximum grid current at this setting. Again set the v.f.o. so a signal is heard at 14 megacycles and repeat the adjustment of $C_{\rm B}$ and $C_{\rm B}$. Then follow the same procedure as before with C13 and C22. By adjusting the broadband couplers in this way it should be possible to find settings at which the grid current in the following stage runs from 11/2 to 2 milliamperes at the 14 and 15 megacycle settings of the v.f.o., and slightly less in between. The final output curve should be two-humped, with peaks on or just outside the edges of the range from 14 to 15 megacycles. and a slight dip in the middle. If this kind of a response curve cannot be obtained by adjusting the four trimmers in the order given previously, reverse the frequencies at which each trimmer is peaked, using the 14 megacycle setting for C15 and C25, and the 15 megacycle setting for C_{13} and C_{18} . If difficulty is still experienced, adjust C13 and C22 at one frequency and C13 and C_{18} at the other. If C_{22} seems to have too much capacity to allow proper adjustment, reduce the capacity

After these adjustments have been made, set the bandswitch to position four and check the output over the range from 7 megacycles to about 7.2 megacycles. The same two-humped curve should be noted. If it is not. find settings of C13 and C15 which will improve output in the 7 megacycle range without materially affecting the output in the 14 to 15 megacycle range with the switch in position five. No adjustments are necessary with the bandswitch in positions one and two because the broadly resonant 80-75 meter coil is in the plate circuit of the first multiplier-buffer tube. Output should be between 1½ and 2 milliamperes over the entire 80-75 meter range.

Minor re-adjustment will probably be necessary after the unit is permanently mounted in the equipment with which it is to be used. The output over the necessary range on each setting of the bandswitch should be checked and the broadband coupler trimmers adjusted for proper response curves.

The unit can be mounted on top of a regular chassis, with 1/4" holes drilled to give access to the broadband trimmers. It will be necessary to mount the v.f.o. multiplier unit to the panel first, so the panel bearing on the bandswitch and the four mounting screws of the National SCN dial assembly can be tightened. Care should be taken to mount the unit in such a way that none of the coils or chokes is in a magnetic field from a nearby power or filament transformer. is particularly true of the v.f.o. tank



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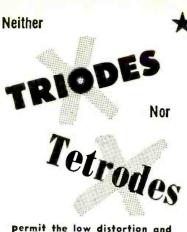
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coil. Frequency modulation at the a.c. frequency of the power or filament transformer will result if the v.f.o. tank is in any stray magnetic field. The unit should be located so that it is protected from drafts. It is better to let it reach a certain temperature and stay there rather than to try to keep it cool. A good source of screen voltage for the v.f.o. is a 30,000 ohm wirewound potentiometer connected across the regulated supply to the v.f.o. plate. This potentiometer can then be adjusted for most satisfactory operation of the v.f.o. multiplier over its entire frequency range and for best keving characteristics. A VR75 tube in series with a VR105 makes a good combination for delivering regulated voltage to the v.f.o. and to the multiplier screens. The plate and screen power supply should be capable of delivering around 70 milliamperes at the required voltages.

Remote B.C. Amplifier

(Continued from page 63)

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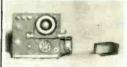
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Technical BOOKS

"ESSENTIALS OF MICROWAVES" by Robert B. Muchmore. Published by John Wiley & Sons, Inc., New York. 232 pages. Price \$4.50.

With more and more services moving into the microwave region as the spectrum becomes more and more congested, interest in the subject has been stimulated to the point where there was a real need for a basic and not-too-technical work covering microwave principles.

Mr. Muchmore has met this need by writing a clear and logical explanation of the phenomena governing the action of microwaves. His style is lucid and straight forward which should prove to be a boon to the student or layman.

The book is divided into fifteen chapters which cover: introductory material, the electromagnetic laws of Maxwell, characteristic waves and wave guides, cavity resonators and filters, characteristic waves and antennas, typical microwave antennas, waves and electron streams—grid-control tubes, klystrons, traveling-wave and multiplestream tubes, magnetrons, electrical noise, microwave radio systems—relays, radar, applications of microwaves in physical research, and microwave measurements.

A glance at these chapter headings indicates the scope of the text and those interested in microwaves should find plenty of food for thought in this volume.

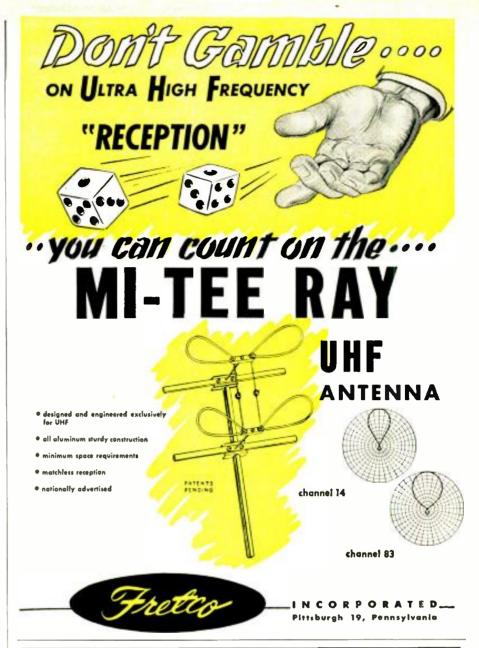
"ELECTRICAL FUNDAMENTALS OF COMMUNICATION" by Arthur L. Albert. Published by McGraw-Hill Book Company, New York. 522 pages. Price \$7.00. Second Edition.

In the ten years since the first edition of this work appeared radio communications, which constitutes a third of the subject matter, have made great strides. Because of these advancements the author has reworked large portions of the original text to bring the reader up-to-date with the state of the art.

The text covers the three divisions of communications, telegraphy, telephony, and radio with its allied branches. Additional emphasis has been placed on radio fundamentals in this edition, along with its allied art—television.

Since this book is designed specifically for beginning students, the explanatory material has been made as simple as possible. One interesting technique which the author has employed is to use illustrative material from the field of communications rather than resort to electrical power analogies or non-related scientific branches.

The sixteen chapters which comprise this book cover such subjects as the fundamentals of electronics; direct voltages and currents; conductors,



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resistors, and insulators; direct current electric power and energy; alternating voltages and currents; the magnetic field and inductance; the electric field and capacitance; electric measuring instruments; alternating current circuits; algebraic representation of vectors; electric networks; bridge circuits; the transmission of electromagnetic waves; fundamental principles of electron tubes; electron tubes as circuit elements; and electro acoustics. A table of natural trigonometric functions has also been included.

"HIGH FIDELITY SIMPLIFIED" by Harold D. Weiler. Published by John F. Rider Publisher, Inc., New York. 208 pages. Price \$2.50. Paper bound.

This compact handbook has been prepared for the benefit of the audio enthusiast who knows and appreciates good music but is not cognizant of the technical "why's and wherefore's".

The author's easy and conversational style helps tremendously in putting the subject matter across to the lavman. He opens the book by discussing the meaning of high-fidelity reproduction, how it may be obtained, and a brief resumé of the type of equipment that is available.

The balance of the book is taken up with a discussion of the individual components which go to make up a high-fidelity music system, i.e., speakers, amplifiers, record players, tuners, and tape recorders.

The text material is lavishly illustrated with actual photographs of commercially-available equipment. A list of high-fidelity component manufacturers is appended for ready refer-

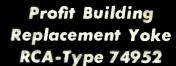
Those planning high-fidelity music systems for their homes will save themselves time, money, and trouble by reading this book first then making their purchases.

"DATA AND CIRCUITS OF MODERN RECEIVING AND AMPLIFYING VALVES" compiled and edited by N. S. Markus & J. Otte. Published by Philips Technical Library. Eindhoven, Holland. Available in the U.S. from Elsevier Press Inc., 402 Lovett Boulevard, Houston 6, Texas. 487 pages. Price \$6.25. Book IIIA, Second Supplement.

This is the third in the Philips series covering receiving and amplifying tubes. The previous volumes covered the years 1933-1939 and 1940-1941. With this book the authors have dealt with tubes brought out by Philips in the postwar years 1945-1950.

Of special interest to engineers is the company's "Rimlock" series of tubes, and the new noval types which include the EQ 80, a specially-designed component for FM and AM-FM receiver applications.

Like the previous volumes of this series, the authors have devoted a generous amount of space to practical applications for the various new tubes. Technical details and performance data are lavishly provided, along with





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RADIO & TELEVISION NEWS

graphical representation of the tube's characteristics.

A separate section in the back of the book provides data on the company's latest measuring and auxiliary equipment line. Each piece of test gear is illustrated, classified, and accompanied by a detailed technical explanation of its performance, etc.

Those who are familiar with the previous volumes in the Philips series will find that the same high standard prevails in this newest publication. Those who are not acquainted with these particular works will find the approach stimulating and informative.

"THERMIONIC VACUUM TUBES AND THEIR APPLICATIONS" by W. H. Aldous & Sir Edward Appleton, Published by John Wiley & Sons. Inc., New York. 156 pages. Price \$2.00.

This pocket-size book packs a wealth of practical information into its comparatively few pages. Although written for the student of general physics rather than the radio specialist, nonetheless the engineer or advanced ham will find much of interest.

Thirteen chapters divide the text material and cover an introduction, the construction of thermionic tubes, the internal action of the two-electrode tube or diode, the internal action of the three-electrode tube or triode, the internal action of multielectrode tubes, the use of tubes as amplifiers, limits to amplification, the use of tubes as rectifiers, the use of vacuum tubes as frequency changers, the use of tubes as oscillation generators, miscellaneous uses of feedback, the use of space charge control tubes at u.h.f., and transit time tubes.

While some knowledge of simple mathematical procedures is requisite for a thorough understanding of the text material, the student should experience no difficulty in handling the subject matter.

Vest-Pocket Receiver (Continued from page 61)

ing "Q". Detuning also takes place, requiring readjustment of the tuning condenser.

Once the assembly and wiring have been completed, and the unit checked for operation, a small screwdriver or alignment tool may be used to tune in the builder's favorite local station. The tuning condenser (C2) may then be left fixed in position permanently.

If the huilder does not wish to leave the receiver tuned to a single station, a small extension might be soldered in place on the trimmer adjustment screw, and a "tuning" knob provided alongside of the "On-Off" switch and volume control.

However, irrespective of the minor modifications undertaken by the individual builder to suit his own requirements, the completed "Vest-Pocket Receiver" should give many hours of pleasure.

This TECHNICAL INDEX is one reason you need this 28-page volume!



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TECHNICAL INDEX

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TO THE AMPLIFIER. Page 8 IMPEDANCE MATCHING Page CONSTANT VOLTAGE DISTRIBUTION SYSTEM...Page 12 IMPEDANCE MATCHING TRANSFORMERS......Page 16 EFFECTS OF MISMATCH UPON POWER

TRANSFER Page 16 CONTROLLING LOUDSPEAKER VOLUME. Page 20 OVERLOAD PROTECTION OF LOUDSPEAKERS...Page 22 PHASING LOUDSPEAKERS Page 23 REVERBERATION Page 23 BAFFLING A CONE SPEAKER.....

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NEW TV PRODUCTS on the Market

PORTABLE TV CAMERA

A portable, self-contained television camera is now available from *Dage Electronics Corp.*, Beech Grove, Ind.

Designed for closed-circuit TV, the new camera measures 14" long, 9%"



high, and 4%" wide. It can be used with any standard television receiver, permitting an unlimited range of screen sizes. No alterations are necessary to the receiver. Daylight or normal room light is sufficient for clear transmission and reception in most cases.

U.H.F. LINE

A closer-spaced, open-wire transmission line for u.h.f. has been released by *Gonset Company*, 80 S. Main St., Burbank, Calif.

The No. 18 gauge solid copper wire is spaced at ½" by means of polystyrene spacers. The closer spacing restricts the field and minimizes dissipation losses and reflection "bumps". Surge impedance is 375 ohms. Attenuation is approximately 2 db per 100 feet at the low end of the u.h.f. band and approximately 3 db at the high end (dry). The u.h.f. attenuation increases moderately when the line is wet.

U.H.F. ANTENNA OFFERINGS

Fretco Inc., 1041 Forbes St., Pittsburgh has introduced the "Mi-Tee Ray" antenna which has been designed exclusively for u.h.f. reception. This all-aluminum unit measures $9^{1}{}_{2}$ " x $10^{1}{}_{2}$ " x $16^{1}{}_{2}$ ". It is pre-assembled for easy installation.

JFD Mfg. Co., Inc. of 6101 16th Ave., Brooklyn 4, N. Y. has added a bow-tie antenna with screen reflector to its u.h.f. line. Delivering between 4 and 6 db in a single array, with gain increasing as frequency increases. the antenna is especially suited for suburban installations.

LaPointe-Plascomold Corp.. Rockville, Conn. is marketing the "Ultra Q-Tee Suburban" which is similar to the company's present Channel 2-83 "Ultra" model except that the u.h.f. "V" portion of the antenna is replaced by an 8-element u.h.f. yagi. It is de-

signed for fringe area u.h.f. reception as well as reception in all multichannel v.h.f. areas.

Telrex, Inc., Asbury Park, N. J. has added the Model #300 "Duplex" yagi to its u.h.f. line. The new antenna is a multi-element beam, small in size, light in weight, and readily installable above existing v.h.f. antenna systems.

Walter L. Schott Company. 3225 Exposition Place, Los Angeles 18, Calif. has two new all-channel u.h.f. antennas available for the trade. The "Reflecto-Fan" includes a screen reflector to give directivity in the horizontal and vertical plane. It is constructed of heat-treated alloy with insulators of special polystyrene compound. The reflector is designed for low wind resistance. The second antenna is a "Corner Reflector."

U.H.F. TUNERS

General Electric Company is now in production on u.h.f. tuners for its TV receivers. Two variations of the tuner will be available; both can be installed by field technicians without removing the chassis from the cabinet.

One type, for use in *G-E* sets made since January, 1949, provides control of the unit from a selector knob on the front panel. For sets made before January, 1949, the u.h.f. control is designed to be installed on the side of the cabinet.

TV TEST PROBE

General Cement Mfg. Co., Rockford, Ill. has introduced a tester for checking high-voltage TV circuits. Measuring about 7" in length, the unit glows when in contact with high voltage.

It can be used for checking highvoltage rectifier tubes, output and transmitter tubes, and high-voltage transformers. The probe is merely brought in contact with the component to be checked. For testing high-voltage filter resistors, the tester is



moved along the body of the resistor with an open or cracked resistor making the tester glow at the trouble point.

TY ANTENNA TOWERS

Alprodco, Inc., Kempton, Ind. is offering three aluminum towers for TV antenna installation applications.

RADIO & TELEVISION NEWS

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850-0-350 @ 300 ma, 6.3 @ 4A, 6.3 @ 8A. 5V @ 3A. Pri. 115V, 60 cy. AC. . . only \$7.95 en.

450-0-450 (a 200 ma. Pri. 115V, 60 cy. AC. 5V (a 3A, 6.3 (a 5 amp. la shielded case.

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The Type AT-6W standard unit will carry a static top load of 300 pounds at a recommended height of 120 feet. The Type AT-6C commercial tower will carry 400 pounds at a height of 150 feet while the Type AT-6E economy model is designed to handle 125 pounds at 48 feet. The first two units are self-supporting to 18 feet and 24 feet respectively. The economy model must be guyed every 18 feet.

All of the towers come knocked down in easy-to-handle sections. A data sheet covering the company's entire line is available on request.

"DETECTO" PROBE

Kapner Hardware, Inc., 2248 Second Ave., New York 29, N. Y. is offering an inexpensive testing tool which permits instant tracing of high-voltage TV troubles

The "Detecto" probe is equipped with a built-in lamp which lights when



high voltage is present. It will check operation of the horizontal amplifier and high voltage transformer by indicating the presence or absence of high voltages. Complete instructions are included with each probe.

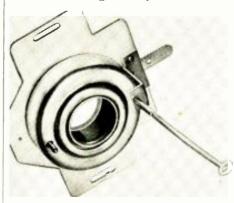
U.H.F.-Y.H.F. ANTENNA

Channel Master Corp., Ellenville, N. Y. is featuring an all-v.h.f.-u.h.f. antenna, the "Ultra Fan, Model 413."

The u.h.f. section features "free-space" terminals, two stamped holes to minimize wind resistance, and single transmission line operation. The v.h.f. and u.h.f. bands are electronically isolated by a 2-stage filter which automatically eliminates all interaction. No switching is necessary in tuning from one band to the other.

FOCUS COIL

Heppner Manufacturing Company of Round Lake. Illinois, has redesigned its "P.M. Focomag" unit to fit 21" and 27" magnetically focused tubes



as well as small sized picture tubes. The efficiency of the ring magnet is said to be such that only 4 ounces of Alnico are required. Another new fea-



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and a Sparker in one handy unit. It TESTS picture tubes—measures Cathode emission, locates shorts between elements, locates high resistance shorts or leakage as high as 3 megohms. REACTL ohms. REACTI-VATES dim tubes. SPARKS OUT electrical leakage.



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2 Instruments in 1 . . . As a REACTIVATOR it renews brightness and detail of dim CR Tubes, without removal of tube from set. It's also an accurate TESTER same as the above. 110V-60 cycles; wt. 3 lbs.

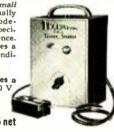
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elements. Saves many picture tubes and small tubes which would usually be discarded. Cathode. grid leakage is an especi-ally common occurrence. The Sparker also gives a rapid check of gas condi-tion of the tube.

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1N5GT	.57	6BA6	.45	65A7GT	.52	12BZ7	.75
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155	.47	6BC5	.53	6SK7GT	.50	12SK7GT	.50
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354	.55	6BH6	.57	6U8	.85	1908	.94
3 V 4	.56	6B16	.48	6V6GT	.46	1978	.79
5U4G	.43	6BK7	.85	6W4GT	.45	25BQ6	.89
5V4G	.73	6BL7	.83	6W6GT	.57	25L6GT	.48
5Y3G	.34	6BQ6	.89	6 X 4	.34	25Z6GT	.42
5Y3GT	.30	6BQ7	.85	6X5GT	.33	35A5	.48
6AB4	.46	6B27	.95	6Y6G	.59	35B5	.47
6AG5	.54	6C4	.34	7N7	.52	35C5	.47
6AK5	.95	ecBe	.53	12AT6	.38	35L6GT	.47
6AK6	.63	6CD6	1.85	12AT7	.68	35W4	.31
6AL5	.40	6F6GT	.45	12AU6	.43	35Z5GT	.30
6AQ5	.46	6F8G	.93	12AU7	.53	50B5	.47
6AQ6	.42	6H6GT	.49	12AV6	.38	50C5	.47
6AR5	.38	6J5GT	.40	12AV7	.80	50L6	.47
6ASS	.50	616	.62	12AX7	.61	11723	.39
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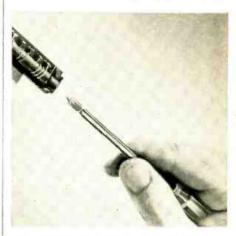
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ture is a specially designed, breakproof flexible nylon adjusting shaft which replaces the rigid shafts formerly employed. The flexibility of the new shafts eliminates accidental breakage during installation.

A built-in picture positioning lever is used to center the picture. Mounting arrangements are according to the user's specifications. Contact the company for full information on the new 'Focomag.'

TUNING SLUG RETRIEVER

R. N. Hunter Sales Co., 3499 East 14th Street, Los Angeles 23, California, is now marketing a new tool which has been designed to retrieve



the tuning slugs in standard coil tuning units, such as those used in RCA, Admiral, Hoffman, and many other television receivers.

The slug-retrieving screwdriver incorporates a unique non-magnetized holding mechanism which enables the technician to retrieve the slug without removing the chassis.

The method employed is simple. The specially-designed blade of the retriever is slipped into the tuning unit opening until it engages the slot on the head of the slug. When contact is made, a forward pressure on the handle of the tool firmly seats the patented locking pin and the slug is then withdrawn and placed in its proper tuning position.

CONDENSER-RESISTOR TESTER

Sprague Products Company, 51 Marshall St., North Adams, Mass. has developed a condenser-resistor alyzer to help speed TV servicing.

The Model TO-4 "Tel-Ohmike" has push-button range selection, extended capacitance ranges from 1 µµfd. to 20,-000 µfd., direct reading of insulation resistance to 20,000 megohms, direct leakage current reading of electrolytics at rated d.c. working voltage, and a three-range power factor measurement of electrolytics. All condensers are automatically discharged for safety after test by releasing the pushbuttons.

Resistance measurement range of the unit is from 21/2 ohms to 25 megohms at line frequency. A 16-page technical instruction manual accompanies each instrument. A descriptive bulletin, M-499, is available on request.

BAR GENERATOR

RMS, 2016 Bronxdale Avc., New York 60, N. Y. is making a low-cost portable bar generator, the Model BAR-1

The unit transmits a modulated carrier on Channels 4, 5 or 6 as predeter-



mined by the technician, producing both vertical and horizontal bars on the screen. A control is provided for adjusting the number of bars on the screen. The instrument is moderately priced. -30-

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56 (Fig. 1), 57 (Fig. 5) JFD Manufacturing Co.
56 (Figs. 2 & 3), 57 (Fig. 1)
Ward Products Company
57 (Fig. 6)
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110 Allied Radio Corporation
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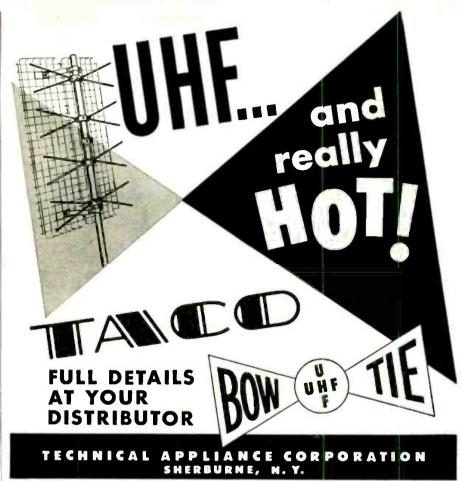
ERRATA

When using the RADIO & TELEVISION NEWS Preamplifier (November, 1952, issue) with an Audak pickup, change resistor R, (Fig. 3) from 22,000 ohms to 100,-000 ohms. For optimum results the Audak requires a load of 47.000 ohms. R in parallel with Ra will provide 50,000 ohms which is satisfactory.

In the article "A Novel Capacitance Relay" appearing in the December, 1952, issue, the circuit diagram shows "117 volts a.c. or d.c.". The unit will not operate on d.c. and this statement should read "117 volts a.c.".

In "Spot Radio News." December issue, a misstatement occurred. Station KPTV in Portland was the first u.h.f. television station in the country and in the northwest but station KING-TV. Seattle, was actually the first TV station in the Pacific Northwest. Our apologies to KING-TV for this slip-up.

In the article "A Low-Cost Audio Oscillator" appearing in the January, 1953, issue, the values of condensers C₁-C_n (Fig. 3) are not clearly indicated. They should be as follows: C, C-1.2 µfd. (20-200 cps): C2, C .-- 12 µid. (200-2000 cps); Ca. C μfd. (20-200 kc.).





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2122	5.50 7F7		74 807	1.59
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ı	2K47460.00	6C06G 1.69	RK48 6.85	WL676 39.95	1N4859
ı	2K48118.00	C61/5C21 6.95	RK49 7.50	WL67734.00	1N51 45
I	0A2 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	6J4 6.66	RK61 3.05	CK531DX 2.19 CK541DX 1.99 CK544DX 2.99 CK544DX 2.99 CK546DX 1.99 CK547DX 1.98 CK571AX 2.99 CK547DX 1.98 CK571AX 2.49 CK567D 2.49 CK577 3.10,49 WL579 10.49 WL579 1	CK5702 1.49 CK5703 1.29 CK5703 1.29 NX14 Diodes NX15 Diodes NX15 Diodes NX16 D
ı	3823/RK22 4.95	6J5GT47	80	707B13.50	1N55 2.35
I	3824 5.40	6K4A 6.45	82 1.69	715A 6.00	1N5689
ı	3825 4.50	6L6 2.09	82V 1.39	715C19.80	1N58 1 19
ı	3828 7.90	6L6G 1.35	83 1.45	717A90	1N6060
ı	3C2277.00	6L6GA 1.35	83V 1.79	7188Y48.45	1N61 2.10
١	3023 9.90	SEATOT 2.29	FG95	718CY48.45	1N63 /K63. 2.49 1N64
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١	303314.98	6587V 1 10	FG98 19.95	7214 2.49	1N69 1.19
١	3C34/HK24 5.49	6507 90	FG104 37 98	7234 11.95	K34 . 1.19

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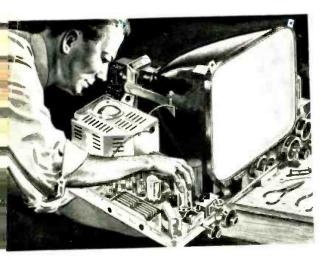
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Rating-for-rating, Mallory FP Capacitors give longer life at higher temperatures and greater ripple currents. They'll give trouble-free performance at 185° F. (85° C.). They are the only fabricated plate capacitors on the replacement market.

For all plastic tubular replacements you can count on Mallory Plascaps® the same way you do on FP's. They eliminate problems of shorting, leakage, unsoldered leads and off-center cartridges.

Nothing will lose a customer faster than a set that won't stay repaired. That's why it is always good business to specify brand as well as rating when you order parts. And if you depend on Mallory you can put an end to call-backs, get precision quality, yet pay no more.

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NEW LITERATURE

TRANSISTOR PROGRESS

The November, 1952, issue of the Proceedings of the Institute of Radio Engineers was completely devoted to the multitude of advances which have been made in transistor research and development. The 528-page journal, containing 51 individual articles, covered all phases of transistor progress. Many of the articles described new applications of transistors in amplifiers, oscillators, rectifiers, electronic computers, and switching circuits.

Copies of this transistor issue are available from the Institute of Radio Engineers, 1 East 79th Street, New York 21, N. Y., at \$3.00 each.

TV EQUIPMENT COMPLEMENTS

All equipment used in a television station is arranged into a few functional groups in the bulletin entitled "Television Equipment Complements for Station Planning" which has been published by the Television Transmitter Division of Allen B. du Mont Laboratories, Inc. 1500 Main Avenue, Clifton, N. J.

The detailed complement of each group is listed with prices and each complement is given a number for easy reference. A short description of the function of the complement is also in-

cluded in each case so that the station planner using this bulletin can select equipment for any size station, large or small, and arrive at the approximate total cost of his equipment.

TWO-WAY RADIO

Use of two-way radio for better coordination of men, materials and machines is discussed in an eight-page illustrated booklet published by the General Electric Company. Entitled "Instant Communication," the booklet is slanted to those who use materials handling and emergency service equipment, and others who have plant protection problems.

Also contained in this publication is a list of 27 G-E offices throughout the United States from which advisory service is now available on communication problems. Copies are free on request to the Advertising Inquiry Section, General Electric Company, Electronics Park, Syracuse, N. Y.

RADIOTELEPHONES

Eight radiotelephone models, two radio direction finder models, and various accessory units are described in a new eight-page catalog. Identified as Form 852, it is available from Applied

Electronics Company, Inc., 1236P Folsom Street, San Francisco, Calif.

Besides a description of the basic design features of these instruments, the catalog includes a full tabulation of models showing number and types of channels, frequency ranges, receiver sensitivities, transmitter power outputs ranging from 40 to 500 watts peak, tube complements, power requirements, dimensions, and weights.

ELECTRONIC INSTRUMENTATION

In a 32-page booklet, the Berkeley Scientific Division of Beckman Instruments, Inc., 2200 Wright Avenue, Richmond, Calif., briefly describes electronic instruments which provide direct reading digital presentation of information together with their principal industrial applications. "Electronic Instrumentation" covers high-speed counting; counting plus control; precise interval timing; and measurement of rpm, pressure, temperature, flow, viscosity, velocity, frequency, distance, etc.

EMBEDDED SELENIUM RECTIFIERS

The Rectifier Division of Sarkes Tarzian, Inc., located at 415 North College Avenue, Bloomington, Ind., announces publication of a new four-page folder dealing with embedded selenium rectifiers. Designated as Catalog B1, this folder gives detailed information on the various types of embedments made by Sarkes Tarzian, Inc. A copy will be mailed free upon request to the manufacturer.

"VIBRATRON"

Model 652 "Vibratron" is a portable instrument for vibration analysis and dynamic balancing. It can be used for balancing practically any rotating part, of any size, without removing the part from its installation, in the range from 500 to 40,000 rpm.

A four-page bulletin describing this device in detail is available from the International Research and Development Corp., Columbus, Ohio.

THERMOPLASTICS

"Custom Extrusions in Thermoplastics" is a new service folder prepared by the Anchor Plastics Company which contains comprehensive information on the characteristics of thermoplastics. Forms and shapes of extruded plastics are discussed, and a general summary of how thermoplastics may be used by industry is given.

This folder may be obtained by writing to Anchor Plastics Company, 36-36 36th Street, Long Island City, N. Y.



and Pilot Regulated CARRIER REPEATERS (for use in conjunction with the CFD-B Terminals on long haul circuits.)

COMPLETELY AUTOMATIC PILOT REGULATION OVER A 20 db RANGE, Built-in "SLOPE CONTROL" includes an extra 10 db equalization for non-conforming telephone pairs.

RYCOM'S CFD-B is assembled from Western Electric component parts, and is mounted COMPLETE with ringing, terminating and power supply equipment in ONE STANDARD AAR 8-FOOT RACK. Standard commercial performance is guaranteed. • Basic line Equalization of 15 db by manual controls. • The range of operation is through a maximum of 30 db over an operating range of 3 to 32.3 kilocycles. • Two-way pilot-regulated repeaters are available for circuits having more than the allowable 30 db loss. • 1000/20-Cycle Voice Frequency Ringers are available for one-, two-, three-, or four-channel ringing. A FULL LINE OF ACCESSORIES is offered, including: • Voice Frequency Repeater Balancing Nets, • Cable Matching Transformers, • Universal Way Station Filters, and • Mounted Sub-cycle Ringing Power Supplies.

RYCOM'S CFD-8 provides FOUR DUPLEX VOICE CHANNELS AND RINGERS at a LOWER COST to you than most three-channel carriers now on the market! And WE CAN MAKE IMMEDIATE DELIVERY!

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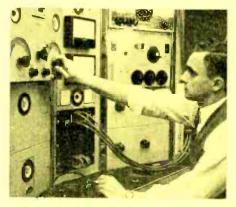
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RADIO CORPORATION of AMERICA



COAXIAL CABLE SYSTEM

A revolutionary coaxial cable system, with triple the telephone circuit capacity of those now in use, has been de-



veloped by Bell Telephone Laboratories and is undergoing exhaustive field trials prior to its installation in the Bell

System. It is expected to go into actual service on circuits between New York and Philadelphia early in 1953.

Known as "L-3" carrier, the new system will enable one pair of coaxial pipes (pencil-size tubes of copper within the cable itself) to handle simultaneously more than 1800 telephone conversations or 600 telephone conversations plus one television program in each direction. It will be the first carrier system on which both television signals and regular telephone conversations can be sent over the same pair of coaxial pipes at the same time. (Photograph shows a Bell engineer testing transmission characteristics.)

IEC STANDARDS

Nineteen countries were represented by 418 delegates at a series of meetings

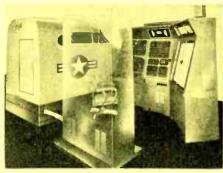
of the International Electrotechnical Commission at Scheveningen, Holland, last September, to discuss international agreement on electrical standards. The United States participated in almost all of the technical meetings.

Among the important actions taken was the authorization of a new technical committee to develop standards for electronic tubes. A number of standards were completed for submission to the national committees, including safety rules for amplifiers and loudspeakers, several standards for radio components, and a revision of standards for power capacitors.

Arrangements were made for extending cooperative action on standards of joint interest to IEC and the International Commission on Rules for the Approval of Electrical Equipment (CEE).

TWIN-ENGINE FLIGHT TRAINER

U. S. Navy airmen will now "fly the beam"—including the new omni-range—in twin-engine ground trainers as the



new ERCO Flightronic trainer takes its place in the fleet's All Weather Flying School at Corpus Christi. Designed by the Engineering and Research Corporation, Riverdale, Md., under contract to the Special Devices Center, Office of Naval Research, this instrument trainer features generalized twin-engine type cockpit and performance, the new Navy colorand shape-coded control knobs, and the Special Devices Center's new standard radio aids simulator and flight plotting board.

GIANT TV ANTENNA

Resembling "Big Bertha" herself, this 86-foot television transmitting antenna is undergoing preshipment tests at *General Electric Company's* Syracuse, N. Y., plant. Only half of the antenna is pictured, the other half being behind the test building.

This 8500-pound giant soon will boost by 12 times the transmitter power of



Station WCPO-TV in Cincinnati, Ohio. The preshipment tests are made to insure that the antenna will efficiently accept and radiate TV signals from the station's Channel 9 transmitter.



COMPOUNDS

Zophar waxes, resins and compounds to impregnate, dip, seal, embed, or pot, electronic and electrical equipment or components of all types; radio, television, etc.

Cold flows from 100°F. to 285°F.

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Military types CR15, CR16, CR18, CR19, CR23, CR24, CR27, CR32, CR36, CR47 are representative of current production by Bliley. Complete range of types and cross reference index is given in Bulletin 43.

SHIP-TO-SHORE



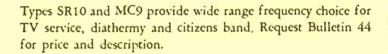
Types MC7, SR5 and SR8 are suggested for shipboard dependability. Price and details given in Bulletin 44.

BROADCAST

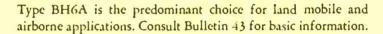


Types BC46T, MO3B, TC92 are first choice for automatic temperature control in AM, FM and TV transmitters. Consult Bulletin 43 for basic details.

SPECIAL PURPOSE



COMMUNICATIONS



STANDARD

Types KV3, MC9, SMC100 and MS433 cover reference frequencies from 100 kc through 10.7 mc. Price and "stock tolerances" given in Bulletin 44.

AMATEUR

Types AX2 and AX3 together with Bliley packaged oscillator Model CCO-2A were designed to bring precision and price together in the Ham Bands. Price and details are given in Bulletin 44.

ULTRASONIC DELAY LINES

Custom built fused quartz delay lines provide high stability and precision time intervals for manipulation of pulsed or pulse modulated signals. Consult Bulletin 45 for technical information.

FREQUENCY STANDARDS

Model BCS-1A is a high stability instrument for precision reference at 100 kc. Ideal choice for research and development laboratories. Descriptive information given in Bulletin 43.





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Personals



DR. ROBERT ADLER, who joined Zenith Radio Corporation, Chicago, Ill., in 1941 as a member of its research division, has just been appointed associate director of research. During the intervening years, Dr. Adler has made numerous contributions to the advancement of the electronics industry and to the improvement of communications equipment used by the armed services. He was awarded a Fellowship by the Institute of Radio Engineers in 1951.



F. CLARK CAHILL is now chief engineer of the Engineering and Production Division of Airborne Instruments Laboratory, Inc., Mineola, L. I., N. Y.; he formerly served in the Laboratory's Research and Engineering Division as supervisor of the Radar Section. During World War II, Mr. Cahill was associated with the Radio Research Laboratory at Harvard University as head of a war research work division. He has been with Airborne since 1945.



EDWARD L. COCHRANE, Vice Admiral, U.S.N., (Ret.), and Dean of the School of Engineering at Massachusetts Institute of Technology, has again been elected a director of Raytheon Manufacturing Company, Waltham, Mass. Admiral Cochrane first served in this capacity for Raytheon from 1948 until 1950, at which time he took a leave of absence from M.I.T. to direct the maritime administration in Washington as chairman of the Federal Maritime Board.



L. F. HICKERNELL, chief engineer of Anaconda Wire & Cable Co., Hastings-On-Hudson, N. Y., was recently elected a member of the board of directors of the American Institute of Electrical Engineers. Mr. Hickernell served as the chairman of the Detroit-Ann Arbor Section from 1929 to 1930; since then he has worked on many AIEE committees, both general and technical. His term as director will extend from January, 1953, through July, 1954.



DR. URNER LIDDEL has joined Bendix Aviation Corporation to direct product development in applied physics and atomic energy. Prior to his most recent position as chief of the physics branch of the U. S. Atomic Energy Commission, Dr. Liddel served as a civilian in the Office of Naval Research where he was director of the Division of Physical Sciences. He is a Fellow of the American Physical Society and the New York Academy of Sciences.



WILLIAM C. LUPFER has been appointed director of contract relations for Avion Instrument Company, Paramus, N. J., where he will be responsible for technical representation of all products. In 1943, Mr. Lupfer became associated with Sylvania Electric Products Inc., as contract and facilities supervisor for the Central Engineering Division, and more recently he was with Allen B. Du Mont Laboratories, Inc., as government contracts administrator.

A.F. Wattmeter

(Continued from page 7)

pling is employed between the two output transformers. The difference of the outputs is taken by reversing the connections of one thermocouple.

Protection against thermocouple overload and burn out is provided by the double-diode 6AL5 clippers interposed between the two amplifiers. These are adjusted to clip or cut off the output at a voltage value just below the point at which the thermocouple heater currents reach 125% of rated value. Since the couples are rated to stand 150% current, a small safety factor is included here.

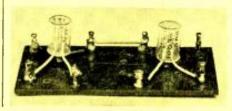
A calibration curve of meter reading vs. input power to resistive or reactive loads is shown in Fig. 3. For a given power input, change of load power factor over a wide range of capacitive or inductive angles makes no change in the reading. For all values of load voltage between zero and 150% of rated value, and with the load current circuit open, the meter stays at zero power.

The particular couples chosen for speed of response have heater ratings of 100 ma., 2 ohms, and couple ratings of 25 millivolts, 7 ohms. The indicating instrument used has a range of 50 microamperes and a coil resistance of 160 ohms. Full scale readings with a load power of 1.5 watts can be obtained.

Speed of response is not as slow as might be expected, full scale being reached from zero in slightly less than one second. For small change from a median reading, the response is even more rapid. Because of the protection given by the diode clippers, there is no fear of burn out or damage due to overload, and the instrument becomes as foolproof as a vacuum tube voltmeter.

Frequency range depends on the selection of the input step-up transformer and coupling capacitors, and to a very limited extent on the choice of the output transformer. The range of 50 to 15,000 cycles can be easily covered with conventional design, and this can be extended through the selection and loading of the input transformer. For extreme frequency ranges, the input transformer can be eliminated and input taken directly from the shunt. Additional voltage gain of about 50 can then be provided with another amplifier stage of conventional design.

Assembly of vacuum thermocouple pair.



an oyster never advertises

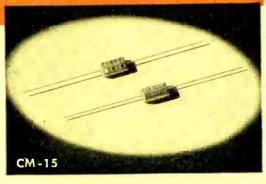
He seems to think you ought to like him for his shell, in spite of the fact that it looks no different from a million other oyster shells. If he's got a pearl inside, why doesn't he say so.

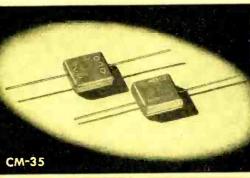
CAPACITORS LOOK PRETTY MUCH ALIKE FROM THE OUTSIDE, BUT EL-MENCO'S HAVE SOMETHING IN THEM and we want the world to know it.

Into every El-Menco Capacitor goes superb design, precise workmanship and the finest of materials. The finished unit is then factory-tested at *double* its working voltage to *insure* satisfactory performance on whatever job it is given.

No wonder we are *proud* to put our name on these capacitors—no wonder they have won the highest praise for their absolute reliability.

The range runs from the smallest (CM-15-2-525 mmf. cap.) to the largest (CM-35-3300-10000 mmf. cap.)





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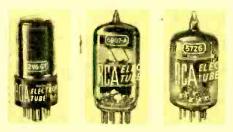
WILLIMANTIC, CONNECTICUT

new

RCA TUBES

The Tube Department of Radio Corporation of America, Harrison, N. J. has released three new tubes: a beam power amplifier, a medium-mu twin triode, and a "premium" twin diode.

Intended primarily for use in the output amplifier of automobile radio receivers operating from a 12-volt storage battery, the 12V6-GT is a beam power tube of the heater-cathode type. A single 12V6-GT operated with a plate and



screen voltage of 250 volts can deliver a maximum-signal output of 4.5 watts.

The 6BQ7-A is a medium-mu twin triode of the miniature type designed for use as the first r.f. amplifier tube in a v.h.f. television-receiver tuner or as a low-noise i.f. preamplifier tube in a u.h.f. television receiver employing a crystal mixer. It supersedes the 6BQ7.

Especially useful as a detector in circuits utilizing wide-band amplifiers, the 5726 is a high-perveance, miniature twin diode. Constructed to give dependable performance under shock and vibration, this is a "premium" version of the 6AL5W.

HYTRON TUBES

Hytron Type 27EP4 is a 27" rectangular, 90°, all-glass, magnetically focused picture tube which provides an effective area of over 400 square inches. Features include an aluminized screen, single ion-trap gun design, and a neutral-density, spherical face plate.

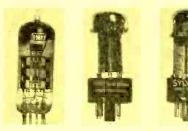
Type 1N64 is a germanium diode designed to meet the requirements for a video detector in television applications. It is application-tested at both the low and high intermediate frequencies.

Both of these tubes are manufactured by the Hytron Radio & Electronics Co., Salem, Mass.

TV PENTODE AND TWO DIODES

A new television pentode, the 12BY7, and two diodes for use in television horizontal frequency damper circuits have been announced by the Radio Tube Division of Sylvania Electric Products Inc., at Emporium, Pa.

The 12BY7 is a high-transconduc- , tance sharp-cutoff video pentode de-



signed for service in television receivers. It features miniature T-61/2 construction, and will furnish large output voltages across low values of load resistance and supply voltage.

Types 6AX4-GT and 12AX4-GT are half-wave, indirectly heated diodes contained in T-9 envelopes. They are designed to withstand the extremely high voltage pulses of line frequency between cathode and both heater and plate elements normally encountered in direct drive circuits. The 6AX4-GT and the 12AX4-GT are identical except for heater characteristics: the 6AX4-GT requires 6.3 volts at 1.2 amperes, while the heater of the 12AX4-GT requires 12.6 volts at 600 ma. ~ (B) ~~

SKL WIDE-BAND DISTRIBUTION YSTEM FOR TELEVISION





views of SKL Model IV Amplifier mounted Model 420 Amplifier in Model 420 Amplitter Cabinet, mounted on a telephone pole crossarm (top), pole (bottom). Courtesy Vermont Tele-vision, inc.

The -SKL- Distribution System provides simultaneous distribution of up to thirteen television channels, FM signals, and, if required, broadcast signals. Although the -SKL- system is inexpensive in initial cost, no effort has been spared to provide high quality, long lasting, low obsolescence designs and equipment. An unusual feature of the -SKL- system is the Model 212TV Chain Amplifier. These broadband amplifiers continue to operate even though a tube fails, which insures the high reliability so necessary in such a system. The -SKL- system is designed to have the lowest maintenance cost of any system on the market today, not only because of the reliability of the amplifiers which require no tuning or adjustment, but also because vacuum tubes have been eliminated in all other parts of the system. Only the -SKL- system can offer the long life, low obsolescence and low maintenance costs that are required for the long, profitable operation of distribution systems.

Write today for further information.

Right: Photo of erection of one of the two Horn Antennas at Barre, Vermont, for Vermont Television, Inc. These antennas, having 20 db gain, provide good signals from WBZ-TV Boston, 140 air miles, and WRGB Schenectady, 130 air miles.

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To definitely establish the superiority of Sylvania Picture Tubes, in comparison with other brands, Sylvania called an outside research organization . . . the United States Testing Company.

Eight picture tubes of nine different manufacturers were selected and submitted to identical electrical and mechanical tests.

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NEW PRODUCTS

ULTRA-LOW FREQUENCY OSCILLATOR

An ultra-low frequency oscillator with standard rack panel construction has been announced by the Krohn-Hite Instrument Company. Model 400-C simultaneously provides both sine- and square-wave voltages at any frequency

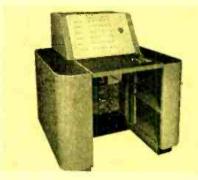


between 0.009 and 1100 cps. The sinewave output may be used either balanced or single-ended. Maximum output is 30 volts peak-to-peak across a 1000-ohm load.

Special circuitry to eliminate tuning and bandswitching transients has been incorporated in this RC bridge oscillator. Descriptive pamphlet is available on request from the Krohn-Hite Instrument Co., 580 Massachusetts Avenue, Cambridge 39, Mass.

TV MASTER SWITCHBOARD

Increased operating control and flexibility are made possible by the television master switchboard recently developed by Federal Telecommunication Laboratories, Inc., Nutley, N. J. Completely self-contained, the unit permits the channeling of six separate inputs to six destinations by means of indirect relay



switching. These relays may be located in the console or at a remote rack.

Automatic clearing, termination and holding features have been incorporated in the switchboard, as well as adjustment of the gap or lap switching interval. The built-in fader employs a twochannel video amplifier through which any two incoming signals may be routed; the output signal may then be reinserted as an additional signal source. Tally lights and internally illuminated push buttons aid in operating effectiveness.

NOISE ANALYZER

Hermon Hosmer Scott, Inc., has announced a versatile sound analyzer which separates noise, sound and vibration signals into their component frequency bands. The high- and low-pass filters can be independently adjusted in steps of ½ octave, and a simple interlock permits the passband width to be fixed in any multiple of ½ octave. The



position of this passband can then he adjusted throughout the audible range by a single control.

Housed in a saddle-leather case with a shoulder strap for portable use, Type 420-A includes a calibrated attenuator, an indicating meter meeting ASA standards, and an output jack for general purpose filter applications.

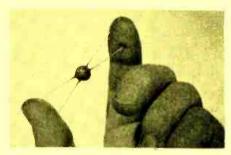
Inquiries should be sent to V. H. Pomper, Hermon Hosmer Scott, Inc., 385 Putnam Avenue, Cambridge 39, Mass. Bulletin is available on request.

MINIATURE PULSE TRANSFORMER

The smallest pulse transformer now commercially available was recently developed by P C A Electronics, Inc. Weighing less than .03 ounces, the MPT 101-0.1 is slightly smaller than a pea, making it specially suited to miniature assemblies; it will, however, operate equally well in conventional circuits. New design techniques and a special

iron core make possible 0.1-microsecond pulse widths and rise times of less than .005 millimicroseconds when used in recommended P C A circuits.

MPT 101-0.1 meets MIL-T27 test specifications. It can operate indefinitely



at temperatures ranging from -70°C to +125°C., and will operate normally for a short time at +150°C. Although it is designed for pulse forming, it can also be used for pulse coupling. For further information, write to P C A Electronics, Inc., 6368 De Longpre Avenue, Hollywood 28, Calif.

WAVE ANALYZER

Analysis of the frequencies and amplitudes of signal components in a complex waveform is accomplished in a simple and direct way with the new Sierra Model 121 wave analyzer. Signal components are read directly on a 4" indicating instrument calibrated in decibels. Voltage is calibrated with an internal 100-kc. injection oscillator, and a listening jack is provided for monitoring the signal being measured.

Just introduced by the Sierra Electronic Corporation, 813 Brittan Avenue, San Carlos, Calif., this 15 to 500 kc. wave analyzer incorporates a novel two-attenuator design which permits a wide range of measuring amplitudes without the introduction of instrument



distortion. It has an input level range of from +42 dbm to -70 dbm at a 600-ohm impedance level; input impedance is 10,000 ohms in the passband.

SCINTILLATION DETECTOR

A new scintillation detector, Model DS-1, has been announced by Nuclear Instrument & Chemical Corporation, 229 West Erie Street, Chicago 10, Ill. Designed for efficient gamma-ray counting in clinical and laboratory applications, the detector is provided with a

(Continued on page 30)

ing. The amplitude, the width, or the time of the pulse may be the analog of the function transmitted. On the other hand, in pulse code modulation the samples of the transmitted function are represented digitally.

Besides the time-sharing of equipment, another reason for sampling data is that an observation or a measurement may take a specific length of time to make. In radar, the time needed to receive an echo at maximum range defines the highest permissible pulse rate. The measured range is represented by an analog distance on the face of the oscilloscope. A motion picture is another example of sampled analog representation. Each frame is a sample of the object's illumination in terms of a chemical analog. The limitation of bandwidth due to sampling is vividly illustrated in movies when the wheel of the stage coach seems to rotate backward.

In order to indicate how an unsampled quantity can be represented digitally, Table I has been prepared. A portion of the sine wave is described in a continuous fashion within an accuracy of three decimal digits. This is done by indicating the degrees (or times) at which the function changes by a quantizing unit. No sampling is involved because the function is defined at all values of the independent variable.

One can build digital units or even digital computers to operate in a continuous manner, but time-sharing of equipment is precluded. This means that a separate element is needed for each digit (parallel unit) and for each operation. A dozen additions would call for a dozen parallel static adders. Such designs are possible and may be practical. A complex diode matrix may be designed to give the binary sum of two binary inputs, which energize the matrix. An experimental tube, the computron', has been partly developed to perform static arithmetic operations. At a recent computer symposium in Pittsburgh, a paper was presented on a special-purpose continuously operating digital computer'.

Elaboration on the difference and the relation between quantizing and sampling may be in order. Both processes introduce discontinuities, but while quantization produces a discontinuity in the value of a quantity, sampling produces a discontinuity in the times at which a quantity is specified. Figure 3 shows a portion of a sine curve quantized but not sampled in part (A) and sampled but not quantized in part (B). The step-discontinuities of quantization depend on the magnitude of the dependent variable, while the impulse-discontinuities of sampling depend on the independent variable.

Although quantization and sampling are fundamentally different effects,

they are interrelated. For example, it would be foolish to tabulate (sample) a sine wave at every millionth of a degree if it is defined only to three decimal places. Similarly, if sampling is done at every ten degrees, there is little advantage in a quantizing accuracy of ten decimal places. In numerical analysis, quantizing errors are called roundoff errors, while the errors arising from sampling are called truncation errors. In an efficient numerical procedure, these two types of errors are balanced.

The analogous situation has been commonplace in conventional analog equipment design. The counterparts of quantizing noise and sampling delay are respectively noise and response lag. Resulting errors (called respectively static and dynamic) should be of the same order in a well-designed analog unit.

Conclusion

It has been indicated that the division of units into digital and analog classes is often obscure and sometimes confusing. Three features have been proposed—positional notation, quantization, and sampling—as more fundamental in characterizing the nature of particular equipment.

Understanding these basic characteristics is not just of academic interest; it can also help in orienting engineers in new avenues of endeavor. By combining these basic properties in various degrees, new ideas and equipment may be more easily created than by thinking in terms of what is conventionally meant by digital and analog. Consider the future problems and solutions which may be ahead of us.

An interesting problem is the balancing of errors due to sampling and errors due to random noise. In serial digital computers, adjustable word lengths may be thought of as a means of changing the quantizing error and the realtime sampling rate simultaneously. Halving the word length could almost double the machine speed and would increase the quantizing error while de-

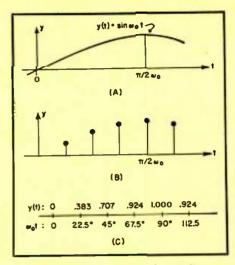


Fig. 2. The process of sampling.

(A) A continuous function of time.

(B) Result of periodic pulsing. (C)

Sampled function displayed digitally.

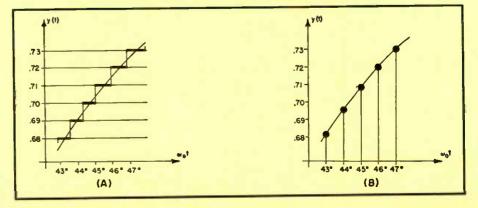
creasing the sampling error. The corresponding design change in an analog case makes the unit less accurate but also less sluggish at the same time.

A fascinating possibility is the use of units consisting of analog (nonquantized) elements combined in a digital manner, just as in the examples of the electric clock and the gas meter. For the transmission of data, such representation is not new. The coarse and fine dials with corresponding selsyns have been used in numerous cases. Could some kind of a computation be done on data so represented?

As techniques in designing compact digital equipment improve, the use of digital schemes for special purposes will become more and more popular. For fixed programs, the magnetic drum may prove a much more efficient and rapid storage element than for general purposes. Digital computations with nonsampled data may also be expected. In addition to the examples already cited, new developments, such as the perfection of ferroelectric techniques, might make such static computers generally practical. These computers will have

(Continued on page 30)

Fig. 3. (A) Portion of a sine curve quantized but not sampled. and (B) portion of a sine curve sampled but not quantized.



ω _o r lin i	Degrees	y(t) = sin ω _o t	
From:	To:		
17400	. 2	*):	
	•	•	
		•	
44.72	44.81	0.704	
44.82	44.86	0.705	
44.87	44.95	0.706	
44.96	45.03	0.707	
45.04	45.11	0.708	
45.12	45.19	0.709	
45.20	45.27	0.710	

Table 1. Indication of how an unsampled quantity can be represented digitally.

unit; each relay is twice as significant as one of its neighbors, although it is physically identical. Or take the time clock at the entrance of a factory; the hour wheel has a much greater effect on the weekly pay check than the physically identical minute wheel.

Now consider a gas meter. One type of gas meter in existence shows about five small dials, like small clocks. Each dial is calibrated from 0 to 9 and boasts one hand only. The gasman reads the total consumption as a five-digit number. Although the five indicators are identical, they have different influence on the gas bill. So far, everything that has been said about the meter would class it a digital unit. Only when the individual digits are examined will any doubt arise, for each hand moves in a continuous fashion. As the gas flows, so moves each hand; therefore, each hand (with its own scale factor) is the analog of the gas consumed. Were the movements of the hands rigged with some escape mechanisms so that they would go through a revolution in ten distinct and equal jumps, the gas meter would be called digital without a doubt.

Quantization

This difference in the mechanism of an individual digit belongs in the discussion of the second basic feature, quantization. Assume an n-digit binary relay register; then for any finite n

greater than one, it will certainly be a digital unit. Even when n goes to one, the single-relay register is still likely to be considered digital because it can occupy only two possible states, i.e., it gives a quantized measure of whatever it represents. Had a decimal register been assumed, the individual digit would again be considered a digital unit because it is capable of assuming only ten different states.

As the number of possible states increases, the quantized nature of a unit becomes obscure and it is finally called analog. Indeed, some people say an analog unit is that which is quantized into an infinite number of states. Actually no shaft, however well machined, can stop at any of an infinite number of possible angles. The voltage on a condenser is generally considered a good example of an analog; yet it cannot change in smaller steps than the voltage due to a charge of a single electron.

To have faith in quantum theory, the fact that everything is quantized must be accepted in the final analysis. If so, how many possible states must a single-digit unit be capable of occupying—a hundred, a thousand, or a million—before it should be called analog? A direct answer to this question could only be arbitrary. The important factor is that quantization introduces an uncertainty into a physical quantity.

When a three-digit decimal counter reads 115, it may indicate that the value of the represented physical quantity is between 114.5 and 115.5. Therefore, the quantized representation is accurate within a tolerance. However, so is a nonquantized representation. If the indicator of a voltmeter stops at the 115-volt mark, it may only be known that the voltage is, for example, 115 ± 0.3 .

Thus, an error is associated with both quantized and continuous indications. In what respect do these errors differ? They differ in their statistical distributions. Figure 1 shows possible distributions of errors in the examples used above. A quantized representation of 115 volts may mean anything between 114.5 and 115.5 with equal probability. If so, the error is uniformly distributed, as illustrated in Fig. 1(A). On the

other hand, the nonquantized representation generally has a less definite error distribution, which is often assumed to be normal. The tolerance limits may then correspond to the probable error, and such a distribution corresponding to the above example is shown in Fig. 1(B).

Just as statistical methods have recently been applied to noise analysis in communication engineering, they have long been applied to quantization errors or roundoff errors. The use of the same methods in both cases is not accidental; rather it underscores the fundamental connection between uncertainties due to varied causes.

Sampling

The third aspect that is bound to enter a discussion of this kind is the process of sampling. Sampling can be defined as the act of taking specimens of a dependent quantity at particular values of the independent quantity. If time is the independent quantity, sampling implies that data are measured, defined, or examined only at particular instants of time.

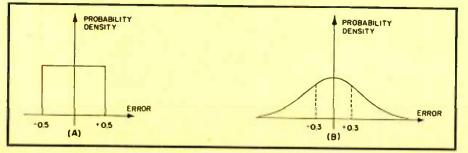
Thus, sampling is basically related to the time and manner of observing data, rather than the type of unit involved. It is true that most kinds of digital units, such as digital data transmission equipment and conventional digital computers, require the sampling of data; nevertheless, digital units can be built that operate in a continuous fashion. It is further true that information approaching or leaving an analog unit is usually continuous; however, for technical convenience, sampled data are sometimes employed in analog systems. The only generality that can be stated is that when equipment is time-shared or when the observation of data takes a discrete length of time, the data involved must be sampled.

The process of sampling is illustrated in Fig. 2. Part (A) shows a continuous function of time, which may be displayed on an oscilloscope. The height of the luminous line above the base line is the analog of y(t). If the grid of the cathode-ray tube is pulsed on periodically, the sampled display of part (B) results. In part (C), the same sampled function is expressed digitally.

This simple illustration may raise two questions. First, although analog sampling is possible, why would it be used? Second, how can sampling be avoided in the digital case?

Consider pulse communication. It is well known that if it is desired to transmit a band of B cps, it will be necessary to use a pulse repetition rate of at least 2B. The pulsed transmission of data has the advantage that the same channel may be used for several sets of information by time-multiplex-

Fig. 1. Possible distributions of errors in the examples given. (A) Uniformly distributed error. (B) Nonquantized representation of error distribution.



FUNDAMENTAL CHARACTERISTICS

THOSE who are familiar with various complex present-day computers will have no difficulty in classifying a specific one as being either "analog" or "digital." This classification into analog or digital computation is apt to be considered both exclusive and exhaustive. It is not difficult to put such two-valued faith to task. This faith may have been strained (though not broken) for the first time, perhaps, when the digital differential analyzer appeared on the scene. Some described it as a digital computer programmed in an analog fashion. Future computers may require. not a single, but a repeated employment of both of these words.

However, no revolutionary developments in the computer field are necessary to cause hopeless entanglement with this limited vocabulary. Suppose a novice were to ask humbly for an explanation of the difference between digital and analog. It would be natural to try to clear up this difference once and for all with a few simple examples. Take the speedometer of a car. The speed indication is by means of a shaft whose angular position is the analog of the speed of the car. This is a fine example of an analog unit, although an innocent reference of the novice to the numerical calibration of the dial might leave an uneasy doubt in the mind. The mileage indicator, on the other hand, is an excellent example of a digital unit: the leftmost wheel counts one for each 10,000 miles, the next wheel for each 1000 miles, and so on down the line. Unfortunately, the purity of this example is rudely shattered by the rightmost wheel; this black wheel of the family turns in a continuous fashion as any decent analog shaft would and seems to carry those large numerals only for the sheer purpose of confusion.

By this time there would probably be a distressed expression on the beginner's face, and, in search of a better example, the electric clock on the wall might be considered. Both hands of such a clock are mounted on continuously rotating shafts whose positions are the analog of time. When about to call the clock an analog unit, however, the beginner might suddenly announce that the two hands of the clock seem to be related to each other in a manner very similar to the wheels of the mileage indicator. In fact, are not the hands of the clock like digits, one showing finer details of the measured quantity than the other?

At this juncture, it might seem like a good idea to execute a strategic retreat and call the clock a unit consisting of OF DIGITAL

ANALOG

UNITS *

By JOHN M. SALZER

Hughes Research & Development Labs.

The terms "digital" and "analog" by themselves are not adequate to describe a computer fully.

analog elements combined digitally. Indeed, it could even be said that this description would fit all clocks and watches. But then the pupil might point out that his watch says "tick-tock" and really measures time by counting the ticks and the tocks, that somebody had told him counting was an action characterizing a digital unit, and that this would make at least the second hand of his watch digital rather than analog! If this is not obvious, it is certainly clear that a stop watch moves in discrete jerks. To add to this burden of proof, it is only necessary to recall the big clock in any high school corridor, which jumps at one minute intervals.

After such an unhappy encounter with a novice, it would certainly be appropriate to re-examine the situation and it would not take very long to find that "digital" and "analog" are about as fortunate classifications for physical units as straw hats and round hats would be for men's headgear. Just as almost every hat is round in some respects, so is any measuring device or computer the analog of something in some respects. The analog of temperature, for example, could be a voltage in an analog unit or a number in a digital unit-in both cases within a certain accuracy. If an analog computer is the analog of a differential equation, a digital computer is the analog of a difference equation.

Whereas the analog class seems to be basically unrestricted, the digital class has more definite boundaries, as will be pointed out below. The real difficulty with the use of these words is caused by an endeavor to make them describe too much at once. Properties which are more fundamental should be reverted to and the equipment classified in terms of these properties. The writer has proposed' the following three features as a

- 1. Positional notation
- 2. Quantization
- 3. Sampling

A purebred digital computer would incorporate all of these features, a thoroughly analog one none. But now examine each quality separately.

Positional Notation

Positional notation is a feature that is fundamentally digital. In the number 888, there are three identical digits; however, they carry different weights according to their relative positions. The high precision attainable in a digital unit is closely tied in with this positional notation. It is only necessary to use more digits of the same kind to increase the accuracy.

There are two ways in which the relative positions of the digits of a number can be recognized: in space or in time. A parallel machine handles all digits simultaneously and requires identical equipment (arranged in space) for each digit. On the other hand, a serial machine recognizes the weight of a digit by the relative time of its appearance at a particular point.

If it is agreed that "digital" means that which consists of digits—and how could it not be so?—, then it is clear that positional notation is a cardinal property of a digital unit. A binary relay register, for instance, is surely a digital

^{*}This article is based on a paper presented at the National Electronics Conference which was held in Chicago, Sept. 29, 30 and Oct. 1, 1952.

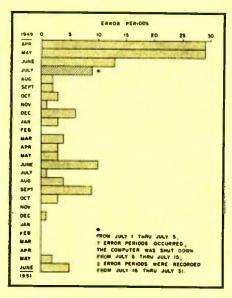


Fig. 4. Performance of the five-digit multiplier during the reliability run.

more rugged units. It is not known that all of these weaknesses would have caused operational failures if they had remained, but as a conservative measure they were regarded as potential faults and were therefore corrected.

During the 96 days following shutdown, the number of error periods decreased to seven. The error rate for the remainder of the 27-month run was an average of one every 286 hours.

Vacuum Tube Life

Significant information on vacuum tube life has been obtained from records on tubes used in the five-digit multiplier. The multiplier contains about 375 tubes (sockets) of which approximately half are types extensively used in the Whirlwind computer (40% of type 7AD7 and 10% of type 7AK7). About 18 per cent of the tube complement is type 6AS6, while small numbers of other types comprise the remainder.

Figure 3 shows the life characteristics of (1) the 7AK7, a dual-controlgrid pentode which was manufactured under pilot plant conditions, (2) the 7AD7, a video amplifier pentode purchased from commercial production, and (3) the 6AS6, a miniature dualcontrol-grid tube also from commercial production. The plot is percentage survival vs. length of service for original and replacement tubes. The criterion for the end-of-life of a tube is the tube's failure to perform satisfactorily in the circuit to which it is assigned. Life of the 6AS6 tubes is apparently much shorter than that of the other two types, because the 6AS6's are used in circuits that have smaller operating margins and the effective life of tubes in a given piece of equipment is closely related to circuit design. If it had been possible to build circuits in which

changes in tube characteristics had no effect on circuit performance, then the percentage of survival would have been much higher than these curves show.

A question sometimes raised in discussions of tube life is whether tubes tend to have a definite period of usefulness and therefore should be replaced as a group after a certain length of time or whether the failures occur at a fixed rate so that nothing would be gained by wholesale tube replacement. Experience with the multiplier seems to point to the latter type of behavior and certainly indicates that wholesale replacement is not warranted within the period of time shown on these curves. In Fig. 3, the data are shown on a semi-log plot with smooth curves (the solid lines) drawn through the points so that the slope of a curve is a measure of the rate of tube failure. For all three types the rate of failure decreases for increasing length of service, as indicated by the flattening out of the curves. However, the samples are probably too small for this fact to be considered significant. To get a conservative measure of tube life in this equipment, points have been determined where 50 per cent of the tubes would have remained if failures had continued at their initial rates, as shown by the broken lines. These figures are 6400 hours for the 6AS6, 14,000 hours for the 7AD7, and 29,000 hours for the 7AK7.

Other Components

No capacitors or r.f. chokes failed during the test and only two pulse transformers had to be replaced. On the other hand, it was necessary to replace 29 of the 120 carbon resistors selected to less than 1% tolerance for use in flip-flop circuits. Crystal clamps were also troublesome in flip-flop circuits, where a back resistance of at least 0.5 megohm is essential. One hundred clamps of a special high-backresistance type similar to the 1N38 were used in these circuits, and a total of 78 replacements was necessary because of the small tolerances. By comparison, 386 crystals (type 1N34 or equivalent) used in other less critical circuits required only 32 replacements.

Because a guarantee of maximum reliability was the intended goal, this sensitive clamp circuit should have been redesigned. However, rather than interrupt the test, a simple marginal-checking routine was applied periodically to the clamp circuits and the deteriorating crystals were quickly located. In this case, then, the desired reliability was ensured at the expense of additional preventive maintenance.

The importance of extensive operating experience in discovering unpre-

dictable factors that influence reliability was emphasized on several occasions. Two examples are of interest. As originally designed, the multiplier had pilot lights to indicate the presence of the +150-volt and +250-volt power inputs to each panel. These lights were 110-volt lamps fed from the respective supply points through appropriate dropping resistors. During the reliability run, it was discovered that occasionally an error count was caused by the burning out of one of these lamps. A search revealed that the dropping resistors were mounted near the filter circuits at the bottom of the panel and that the leads at the top of the panel were cabled for some distance with several wires which distributed power to the circuits on the panel. Under these conditions, interruption of current to a lamp caused a sudden jump in voltage on the wire to that lamp. This voltage jump, capacitively coupled into the power distribution circuits, was responsible for the errors observed. Relocating the dropping resistors at the lamps rather than at the filters eliminated the trouble.

The second example of unpredictable factors which can affect reliability was discovered accidentally. A metal coat tree in the multiplier room was habitually used by a few employees who worked in that portion of the building. One employee observed that a static discharge from hanging his new plastic raincoat on the coat tree caused multiplier errors. The exact way in which these were introduced was not determined. Previously, qualitative tests had been made to discover whether the system was sensitive to radiated signals and negative results were obtained. A commercial r.f. bomber was used for these tests and no attempt was made to cover the complete r.f. spectrum.

Noise Measurements

One of the aims of the multiplier reliability test was to examine the adequacy of maintenance techniques and, if possible, to discover new techniques which might be applicable to the Whirlwind I computer. Toward this end, some experiments were carried out to determine the sensitivity of the system to noise signals.

In the majority of electronic circuit applications outside the computer field, an occasional transient disturbance whose amplitude is comparable to that of the wanted signal is of little or no consequence. Interpretation of signals within these systems, whether by human beings or electrical equipment, involves an averaging or filtering process which effectively discriminates against noise. In a digital computer, however, interpretation of signals is done by memory

(Continued on page 31)

voltages, generally screen voltages, in selected circuits of the multiplier so that the components operate under great stress. Any component with a low operating margin will effectively lose this margin during the check and the circuit will not operate. When a test problem is run, the operator can then isolate the weak component and replace it.

Power for the multiplier is supplied from three motor-generator sets whose d.c. outputs are -100, +150, and +250 volts. Power for marginal checking is obtained from a G-E amplidyne whose d.c. output can be manually varied from -100 to +100 volts. During marginal checking this generator is switched in series with the d.c. supply to the circuits which are to be checked.

Extended Reliability Run

On April 1, 1949, the multiplier started a reliability run which extended for 27 months. During this time, the machine continuously multiplied two five-binary-digit numbers and checked for a correct result at the end of each multiplication. The multiplications required about 8 microseconds each and were repeated at the rate of 15,000 times a second. When errors occurred, they were recorded by electromechanical counters and an Esterline-Angus inking recorder. Three counters were used as a "two-out-of-three" check; twice a day they were tested carefully to be sure they would respond to a single-error pulse.

Performance requirements were rigorous. All errors of undetermined origin and those from failures of defective, deteriorating, or accidentally damaged components were counted. Those resulting from failures of power supplies were also charged against the system. The only exceptions were errors caused directly by two failures in city power, two power line failures, and a transient introduced into the power line by a local thunderstorm.

For the first 18 months, about half an hour of each working day was spent in preventive maintenance. During the last nine months, as performance improved, this checking was reduced to twice a week. In addition, trouble-shooting for intermittent failures, not isolated by marginal checking, was necessary—especially for the first six months.

A log was kept during the entire run, with entries stating when errors occurred and what remedial action was taken. An operation chart was drawn daily from the information in the log to provide an over-all picture of the multiplier's reliability. The longest error-free run extended for 143 days, or nearly five months. It was interrupted when, for some unknown rea-

son, a power supply fuse burned out.

The test was terminated June 30, 1951, because operating experience on the Whirlwind I computer had reached a point where little benefit could be obtained from further studies of the five-digit multiplier.

Error Periods

Figure 4 summarizes the number of error periods that occurred during each of the 27 months. An "error period" is defined as the discrete period during which any number of errors occur without interruption. This number may range from one to several thousand, but since single errors, as well as multiple errors, can invalidate results and require the attention of an operator, each error period is considered as having the same weight regardless of the number of errors recorded. The total number of error periods over the 27 months was 142, or an average of one every 136 hours.

Work During Shutdown

Over half of the error periods (78) occurred during the first 96 days (April 1 through July 5, 1949). Considerable dependence had been placed on the marginal-checking facilities as a means of obtaining and keeping a high level of system performance, but this large number of error periods indicated that the new maintenance technique alone was not sufficient.

Because daily checking ensured that all circuits basically had wide operating margins, it was concluded that the frequent errors were caused by transient disturbances rather than by slow drifts in circuit tolerances. Intermittent connections were suspected first, and for lack of more refined methods, the search for such connections was made by

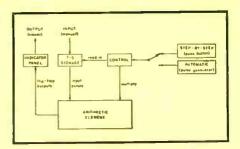
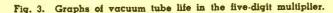
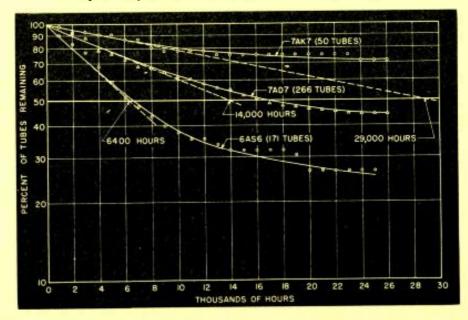
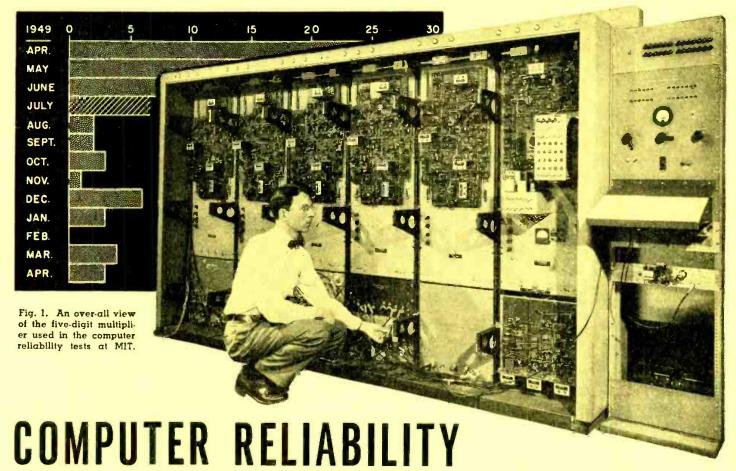


Fig. 2. Block diagram showing logical design of the five-digit multiplier.

painstakingly tapping panels and components. Within a short time sufficient weaknesses were found to indicate that a shutdown for overhaul was necessary. Nearly all of the faults discovered were ones which caused momentary rather than permanent failure. Furthermore, they would have been overlooked if evaluated by the usual criteria of performance; they were shown up in this case by the extreme sensitivity of the multiplier acting as a detecting instrument. The defects found were (1) insufficient spring pressure in cartridge-type fuse holders, (2) inadequate contact pressure in power distribution relays, (3) momentary shorts or leakage between elements within vacuum tubes, (4) poor connections in adapters which had been provided to permit use of lock-in-base tubes in circuits built for octal-base tubes, (5) loose screws on powerwiring terminal strips, and (6) unsoldered or cold-soldered component connections. The shutdown was utilized to correct all of the faults that had been discovered and to guarantee reliability further by eliminating all unnecessary contacts (such as relays and manual switches) and by replacing all fuse holders and tube adapters with







By

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Performance criteria of electronic digital computers based on results of an extended 27-month life test.

AINTAINING system reliability in a large digital computer is a far different problem from that encountered in the operation of radar, television, and other communication systems. A stray pulse or an intermittent failure of any one of thousands of electrical components, for example, may cause a circuit to function improperly and thereby invalidate all subsequent calculations. The engineer who enters the field of electronic computation must therefore adopt an entirely new concept of system reliability, based on the elimination of single errors. Unfortunately, he cannot find the criteria for implementing this concept in any textbook; he must learn them gradually from the experience of others and through his own cut-and-try methods.

The purpose of this article is to place on record the results of a 20,000-hour reliability run of a prototype digital computer, in which the goal was error-free operation for extended periods. Although this life test does not offer a specific answer to every question

it raises, the findings may give the reader a point of departure for developing his own philosophy on the subject.

Five-Digit Multiplier

Before the construction of the MIT Whirlwind I electronic computer* could be completed, it was essential that pertinent data be obtained on the reliability of basic circuits and the life expectancy of vacuum tubes and other components. Since no information on the extended operation of a system such as the Whirlwind could be found in the literature, a five-digit multiplier (Fig. 1) was built as the proving ground for the new pulsed circuits and components.

A short description of the multiplier will aid the reader in understanding the discussion of the life test which follows. The logical design of this prototype computer is shown in Fig. 2. The arithmetic element uses 275 vacu-

*A high speed digital computer sponsored by the Office of Naval Research.

um tubes, 350 crystal rectifiers, 800 resistors, 675 capacitors, 100 pulse transformers, and 80 r.f. chokes. Design was limited to one arithmetic process because the circuits and techniques are similar for each process; multiplication was chosen because of the strict circuit requirements it imposes. Storage and input-output elements were not stressed and appear in the simplest forms: toggle switches, push buttons. and indicator lights. The control was built from special pulse-control test equipment developed at MIT* and contains approximately 100 vacuum tubes and 950 other components.

When two numbers are to be multiplied, they are inserted manually into the registers of toggle-switch (T-S) storage. The numbers are read into the arithmetic registers and multiplication is executed by 0.1-microsecond pulses. A control switch provides for either automatic (2-mc.) or step-bystep (push-button) operation. Results are displayed in binary notation by flip-flop indicator lights.

A preventive-maintenance scheme, called "marginal checking," was built into the system in order to detect deteriorating components before they could cause errors in computations. (The rack at the extreme right in Fig. 1 holds these circuits.) The function of marginal checking is to vary certain

*Described in the Aug., 1951, through February, 1952, issues of RADIO-ELECTRONIC ENGINEERING.

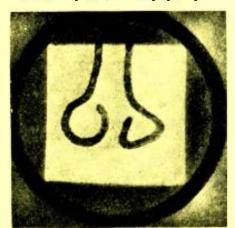
pulses. For amplification of the secondary emission, it is expedient for the inner surface of the receiving plate to be covered by a special layer which possesses great secondary emission.

The method of obtaining a visible picture may be altered, as shown in Fig. 3(A). Here, the piezoelectric quartz plate (1) serves as the base of the vacuum triode (2). An ultrasonic beam falls on the outer surface of the piezoelectric plate (1), the inner surface of which is covered by a photosensitive layer. Under the action of the ultraviolet beam (3), uniformly illuminating the inner surface of the plate, photoelectrons are emitted which-accelerated by the application of an electrical field-pass through the system of magnetic and electrical lenses (4) and fall on the fluorescent screen (5). On the screen, as in the usual electron microscope, only the image of the source of electrons may be seen-in this case, the image of the distribution of photoelectric emission from the surface of the piezoelectric plate (1). Distribution of photoemission on the surface of the plate is in precise conformance to the distribution of the piezoelectric charge, which reproduces the configuration of the ultrasonic field. On the screen (5), the image of the ultrasonic field can be seen; this is a repetition of the image of the object, established by the ultrasonic field, in conformance with the magnified scale.

The resolution capability in this case is dependent on the length of the ultrasonic wave, on the thickness and dielectric property used in the piezoelectric plate, and on the construction of the lens system. Ultraviolet radiation, illuminating the quartz plate, can be replaced by a homogeneous electron cluster.

Another version of the ultrasonic microscope is illustrated by Fig. 3(B). This, as in the preceding version, depicts the object received in magnified scale on the screen (5). However, in

Fig. 4 Utrasonic microscope image of metallic loop immersed in opaque liquid.



this scheme, the screen (5) consists of a thin plate on which a photosensitive mosaic layer is drawn, causing secondary electrons under the action of falling electrons to be collected on the annular anode (6). Electrons in the beam (7) fall on the screen (5) and, as in the usual television tube, move line and frame, equalizing in such a manner on the screen (5) as to form an image of the object by electrical potential. The change in secondary-electron emission is amplified and passed to the second tube, in which the cathode beam movement is synchronized with the cathode beam (7). In this case, the image of the object is received on the screen of the second tube.

It should be noted that the capabilities have to be determined not only from the facts mentioned above but also by additional factors of another kind, primarily by the complexity of the vibrations of the quartz plate which is excited by different types of ultrasonic beams; the action of these beams induce not merely longitudinal waves but also transverse and surface waves, which will distort the image. Use of the quartz plate is accomplished by special cuts and choice of the proper method of strengthening (border conditions), which may be diametrical, and the surface waves in the quartz plate are greatly attenuated to increase the clearness of the picture. Applications for the ultrasonic microscope evidently are diversified enough and have sufficient possibilities to warrant rapid growth in this field.

Now to the description of the experimental performance of the ultrasonic microscope in scientific laboratories:

In Fig. 4, a metallic object is shown immersed in an opaque liquid (magnified ten times).

Figure 5 illustrates a glass rod and glass tube of equal dimensions. In the rod, the clear space shows ultrasonic waves partially suppressed. The tube displays uniform illumination, as the

Fig. 5. Image of glass rod (left) and tube (right) in a homogeneous field.



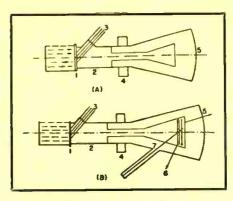


Fig. 3. Two alternate versions of the ultrasonic microscope. (A) Image is formed by acceleration of secondary electrons from treated surface of quartz plate 1. (B) Image is formed by electron beam 7 which scans element 8.

ultrasonic ray does not pass across the tube. Therefore, the shape, with the help of the ultrasonic microscope, may be distinguished by the presence of a capillary.

In Fig. 6, the rod and tube are again shown, illuminated by a different type of ultrasonic ray. This discriminates between particles illuminated with different intensities and therefore depicts alterations.

With the ultrasonic microscope, especially good observations may be made of structures. It must be determined which structure of the ultrasonic wave will give exactness of transmission without a type of deformation. When the radiating quartz plate oscillates in the fundamental mode, and no object is being examined, a light even spot is obtained. For oscillations above the fundamental, a nonuniform illumination results.

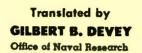
In the ultrasonic microscope, the object conforms to the tube, bound with the ultrasonic wave, and the image conforms to the transmission tube, on the screen of which the object is seen. One form of an ultrasonic microscope is shown in Fig. 1.



Fig. 6. Glass rod (left) and tube (right) in a nonhomogeneous uitrasonic field.



ULTRASONIC MICROSCOPE*

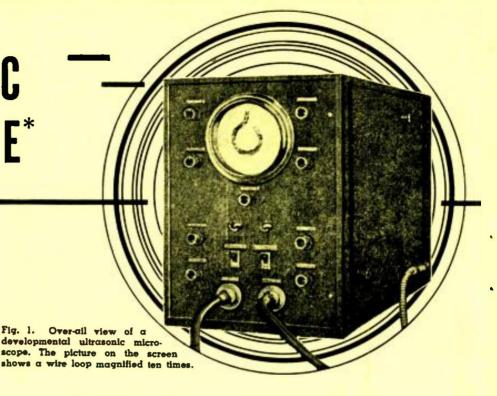


THE successful development of ultraacoustics and the obtaining of very
short ultrasonic waves, of the order
of the wavelength of visible light, has
led to the development of an ultrasonic
microscope with which it is possible to
view the picture of an object in magnified scale. Inasmuch as nearly all bodies
in nature are transparent to ultrasonic
waves, the ultrasonic microscope is expected to have a very wide field of application. Its principle of operation
may be found in the proposal of S. Y.
Sokolov in 1936 (U. S. patent 2,164,125,
issued June 27, 1939).

Operation of the ultrasonic microscope may be described as follows. A narrow beam of ultrasound is bunched (Fig. 2), and radiated by a piezoelectric quartz plate (1) to illuminate the object under examination (2). Reflections of the ultrasonic beam from the object fall on an acoustical collector lens (3), the focus of which is set for reception at (4), consisting of a piezoelectric (e.g., quartz) plate.

The reception plate is located at the base of the tube (8). The narrow beam of the cathode rays (7), inside the cathode ray tube, falls on the inner surface of the narrow plate and dislodges secondary electrons, which are then collected by the anode (9).

Under the action of the charge, the image on the inner surface of the narrow plate comes from the region of the ultrasound, and secondary electrons are emitted when the surface of the plate is made to undergo a change. This change of secondary emission results in greater current acting on the anode (9), the magnitude being increased by special amplifiers and passed to the modulator arrangement of the cathode of the tube (6). Then the intensification of the cathode beam in the tube (6) causes a fluctuation which conforms to the variation of secondary emission from the



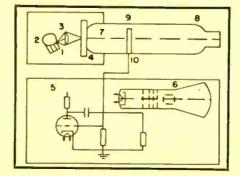
Ultrasonic waves have been successfully used as the source of illumination in a microscope.

surface (4). This is accomplished by the television method of synchronism of motion by lines and frames of the cathode beams of the tubes (6) and (8). The screen of the cathode tube (6) then shows the semblance of a picture as distributed by the electrical charge on the receiver plate (4).

Piezoelectric charges appear on the surface of the quartz plate at the same points where deformation has taken place. Therefore, a picture is distributed on the surface of the quartz plate in exact conformance to the ultrasonic field in the focal plane of the lens (3).

Inasmuch as the configuration of the ultrasonic field in the focal plane in its line of conformance portrays the object, this object is immediately seen on the screen of the tube (6). Transposition of the object understandingly gives the appearance of transference of its image to the screen.

Fig. 2. Diagram illustrating the principle of operation of the microscope.



Magnification of the image, given in the description of the system, is determined by the ratio of the linear dimensions of the cathode tubes (6) and (8). Calculations show that in the ultrasonic microscope magnification approaches the order of tens of thousands of times. The resolving capacity depends on the cross-sectional area of the cathode beam in the tube (8), parameters of the piezoelectric plate, and length of the ultrasonic waves.

Experiment shows that a frequency of 10° cycles can be obtained without particular difficulty and that there is a good possibility of obtaining a frequency of 10¹° cycles. In water, the length of ultrasonic waves at a frequency of 3 x 10° cycles is equal to 5 x 10⁻⁵ cm., i.e., the wavelength of visible light. At that frequency, the resolving power of the ultrasonic microscope may reach an extreme, close to the resolving power of the optical microscope.

For capillary waves, the speed of diffusion is considerably less; and the wavelength accordingly is much smaller than the wavelength of visible light. Consequently, if the radiation type of capillary waves can be obtained at higher frequencies in the future, there will be an opportunity to increase the resolution capacity of the ultrasonic microscope by one or two orders to compare with the best optical microscope.

The objects under examination can be illuminated with a continuous ultrasonic beam as well as with single im-

^{*}Translated from an article entitled "The Ultrasonic Microscope" by S. Y. Sokolov which appeared in the Russian Journal "Progress in Physical Science," Vol. XL, Jan. 1950.

Controls may be added for additional individual adjustment, usually taking the form of resistors in the circuit. However, it should be noted that coefficient a_2 of (3) appears in the results of (7) and (8). Any additional resistance added to the circuit for adjustment purposes has the effect of linearizing the circuit, reducing the value of a_2 , and thus lowering the sensitivity of the circuit when used as a wattmeter.

Since three coefficients appear in the series (3), three independent adjustments are theoretically needed. These additional adjustments may be obtained by use of triodes or pentodes with grid bias controls, but the over-all result is not changed—to achieve and maintain a match of volt-ampere characteristics over an applied voltage range of possibly 50 to 1 is not a practical matter with commercial tubes.

Use of Thermocouples

It should be noted that the important property required of this circuit is its ability to square, or cross-multiply, the input voltages, since it is only the squared term of (3) which leads to the result of (7) or (8). Another electrical device that inherently employs this squaring property is the thermocouple, as its output is obtained from heat or i^2R input to its heater.

Actually, the thermocouple has been employed for many years as a squaring device in a wattmeter, sometimes used in the electric utility industry. When so used, the device is known as a Lincoln "thermal converter" wherein a d.c. electromotive force is generated proportional to load watts, this d.c. electromotive force then being telemetered or transmitted over telephone lines to a distant point where the power is indicated or recorded.

The desired squaring property is present in the thermocouple together with certain disadvantages, such as limited overload capacity, slowness of response, low heater resistances, and thus rather large current inputs. By using electronic amplifiers and techniques in the thermal converter circuit, it is possible to overcome all of these disadvantages except the slowness of response. This can be controlled to some extent by the selection of very small thermocouples of low heat capacity, and an anticipating electrical circuit can be added if needed.

Thermal Converter

The principle of the thermal converter is illustrated in Fig. 2, from which it can be seen that this unit is fundamentally the same as the electronic unit of Fig. 1. Thermocouples are employed to square the respective sum and difference input voltages, and to subtract the outputs, leaving a net

current through the microammeter M which is proportional to power in the load circuit. In Fig. 2, H indicates heater connections, C the couple connections; vacuum-mounted thermocouples are preferred.

There is one objection to the use of the simple circuit of Fig. 2. Theory indicates that the circuit has maximum power sensitivity when voltages E_1 and E_{2} of (8) are equal. Since it is not usually desirable to make the series voltage drop of IR: equal to the line voltage E, because of excessive losses, some form of amplification of voltage $E_z = IR_z$ is desirable. In order to reduce the loading effect of the wattmeter on the circuit to a minimum, an electronic amplifier is indicated. It should be pointed out, however, that the amplifier will only be required to be linear, all squaring or nonlinearity of characteristics being a function assigned to the thermocouples.

The Wattmeter Circuit

The circuit of the amplifier incorporated between the shunts and the two thermocouples is shown in Fig. 5. A 50:1 step-up transformer is used across the shunts, as this seemed an easy way to obtain isolation and a voltage increase. Shunt values are chosen to produce 20 millivolts at full-load current. and the line voltage is taken off the shunted potentiometer at a point providing one volt maximum. It is realized that the use of good transformers is necessary at this point if wide frequency response is to be obtained. However, if a poor transformer is used, its performance can be considerably improved by shunting the secondary with a loading resistor.

The first amplifier stage is conventional. The second stage employs two

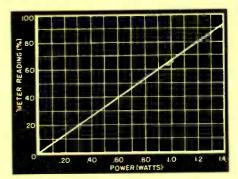


Fig. 3. Typical calibration curve.

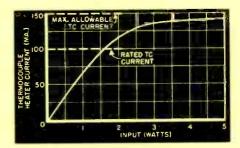
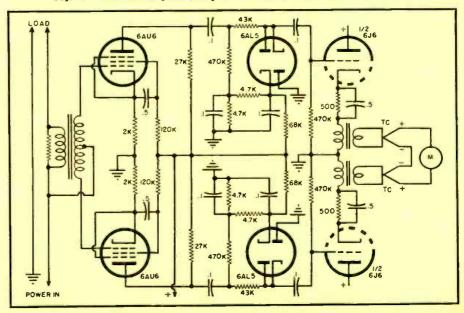


Fig. 4. Performance of vacuum tube limiters in preventing the thermocouples from burning out.

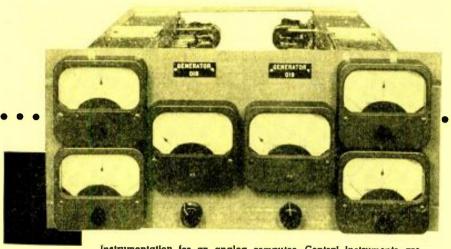
6J6 tubes, with halves paralleled, and with cathode-follower output. This form of output provides much wider frequency response from a given transformer than if the more usual plate output were used. In this case, the transformers are needed for matching the relatively low-resistance thermocouple heaters (2 ohms, 100 ma.) to the 6J6 tubes, and low-cost tube-to-voice coil transformers were found to be satisfactory.

It should be noted that this is not a push-pull amplifier since the two side channels are amplifying different signals $(e - iR_2 \text{ and } e + iR_2)$, and no cou
(Continued on page 20)

Fig. 5. Schematic diagram and parts values for the complete instrument.



A THERMOCOUPLE A.F. WATTMETER*



J. D. RYDER
and
M. S. McVAY
University of Illinois



Instrumentation for an analog computer. Central instruments are electronic voltmeters and outer vertical pairs are wattmeters.

By using electronic amplification, many disadvantages of the thermocouple for measuring power are overcome.

A UDIO-FREQUENCY power measurements have usually been made by dissipation of the power in a known resistive load, since few audio-frequency wattmeters have been available. Numerous proposals appear in the literature covering low-burden electronic instruments which usually employ some form of square-law circuit, as in Fig. 1, but practical forms of the instrument have rarely appeared.

Usual Theory

It can be seen that the input to diode (or triode) V_1 in Fig. 1 is:

 $e_1 = e - iR_2$. . . (1) and the input to diode V_2 is:

 $e_1 = e + iR_2$ (2) where e is the instantaneous value of voltage applied to the load, and i is the instantaneous value of current flowing to the load. Resistors R_2 are assumed small and equal.

In the usual manner, if the diodes

have identical volt-ampere curves given by:

$$i = a_0 + a_1e + a_2e^2$$
 . . . (3)
then the anode current of V_1 is:

$$i_1 = a_0 + a_1 e - a_1 i R_2 + a_2 e^2$$

The output or load circuit is acted upon by the difference of currents i_1 and i_2 , and it is apparent that all positive terms appearing in both equations will cancel, leaving only a result equal to twice that of the negative terms in (4). Thus:

$$i_{out} = i_t - i_1 = 2a_1iR_2 + 4a_2eiR_2$$
 (5)

If the applied electromotive force is sinusoidal, or $e=E_1$ sin ωt and $i=I\sin(\omega t+\theta)$, where θ is the power factor angle of the load, then the output current is:

$$i_{out} = 2a_1 I R_2 \sin (\omega t + \theta) + 4a_2 E_1 I R_2 \sin (\omega t) \sin (\omega t + \theta). (6)$$

If $IR_2 = E_2$, the above becomes by expansion:

 $i_{out} = 2a_1 IR_2 (\cos \theta \sin \omega t + \sin \theta \cos \omega t)$

 $+ \frac{2a_2E_1IR_2(\sin\theta\sin2\omega t)}{-\cos\theta\cos2\omega t}$

If this difference current is applied to a d.c. or average reading instrument M, only the last term of (7) will deflect the meter, since the first two terms represent a.c. currents. These may be bypassed around M by a suitable capacitor.

If $IR_2 = E_2$, then the instrument M is deflected by a d.c. current of value: $i_M = 2a_2E_1E_2\cos\theta$ (8) which is proportional to the average load power, angle θ being the load power factor angle. Thus meter M becomes an indicator of average load power.

Reasons for Dissatisfaction

Certain assumptions have been made in reaching the above results, and these are:

- (a) The two tubes have identical voltampere curves, or pass identical currents for all values of applied voltage.
- (b) The matching of (a) exists throughout the life of the tubes, and for all values of heater voltage.
- (c) The tube volt-ampere curve is accurately expressed by (3), and no higher power terms are present.

In practice, it has been impossible to find or to maintain tubes or crystals meeting these assumptions, such that power measurement accuracies of better than 5% can be achieved without severely restricting the load current or voltage to a very small range. Two tubes or two crystals may be matched to equal quiescent currents or values of a_0 , by adjustment of the tap on R_1 , but balanced currents will probably not be obtained at other applied voltages. This action, of course, indicates unequal values of a_1 and a_2 .

*This article is based on a paper presented in Chicago at the 1952 National Electronics Conference, held Sept. 29, 30 and Oct. 1.

Fig. 1. Basic form of the square-law circuit used for power measurement.

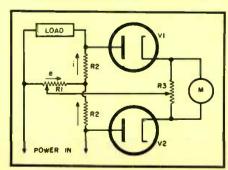
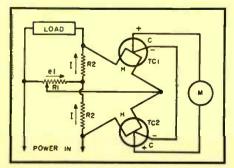


Fig. 2. Schematic diagram showing basic principles of thermal converter.



sponse range limited to the intelligence frequency to be investigated. By considering the theory of galvanometer operation, it is easy to realize that since the flux density is a constant, more force will be produced by a constant current if the number of turns is increased. Unfortunately, more turns increase the mass, so the natural frequency is low. Conversely then, reducing the number of turns will increase the natural frequency but reduce the force or degree of rotation of the mirror.

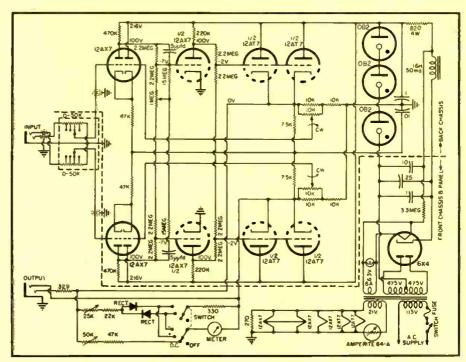
Data received at telemetry stations is generally stored on magnetic tape, which is played back after the test has been completed, and is recorded directly on a recorder which produces a visual and permanent record. In the oscillograph recorder, the photosensitive paper travels at a constant speed while an accurate time base is recorded, and the information is presented as a trace deflection proportional to the intelligence data. The usefulness of the record is threefold-an experienced engineer can view a record after a flight and, reading it as a graph, estimate performance; he can read data accurately by tabulating each period of time required; or if the data are to be fed from magnetic storage into electronic computers, he can determine which portions are worth while tabulating or printing and at what rate it should be accomplished.

Applications

Utilization of recording oscillographs to record data in telemetry installations at the guided missile test ranges has become a necessity. Merely to place them on benches or tables is most inefficient and not in keeping with the present "state of the art." If varying work loads exist whereby "setup conditions" have to be changed occasionally, the work becomes very difficult and discouraging. In fact, where lack of standardization is apparent, so much individualism creeps in that set procedures cannot be adhered to. The result is eventually disastrous. Sooner or later, while under pressure or while training new personnel on the job, the time will come when the signals supposedly connected to the instrument will be missing from the record.

The early oscillographs were developed to enable seismograph recordings to be made in geophysical exploration, and they still find wide application in that field. In these early models, small pickups would indicate amplitude and the recorder itself would apply a time base so that small exploding charges could be set off to indicate terrain configuration.

Radio telemetry is one of the prime users of oscillographs today, and has



Circult diagram and parts values for the galvanometer amplifier.

fostered or made practical many of the improvements on oscillographs which have been adapted in the past few years. Recording oscillographs are in use in the majority of telemetry systems as one of the means of recording data, and they will be found on most of the missile test ranges. Some of the ranges employ 20 to 40 such instruments.

The recording oscillograph, when used by itself, can be operated on a laboratory bench or table. While the instrument is only 12-14" high, 10-12" wide and 18-24" deep, it requires a considerable amount of free space for cabling, galvanometer adjustment, _ changing drive speed, magazine loading and operational viewing. In fact, every side must be accessible except the bottom and the back. Unfortunately, to provide accessibility, many instrumentation installations merely space them wide apart in rows on tables. Thus, all the engineering planning of the installation is lost somewhere in a maze of cabling that resembles a conglomeration of short-circuited onearmed bandits. The small oscillograph now requires a floor area of about nine square feet.

Oscillograph Racks

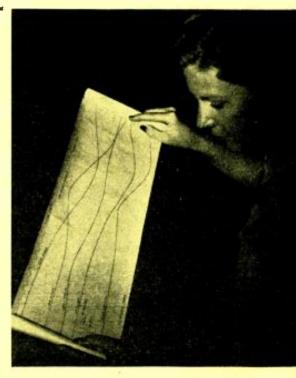
Because of experiences gained from the other missile test ranges, the engineers in the AFMTC's Technical Systems Laboratory felt that it was necessary to develop and fabricate oscillograph recording racks for installations of elaborate telemetry facilities, and furthermore, that centralized recording techniques should be employed. The final AFMTC design provided for all

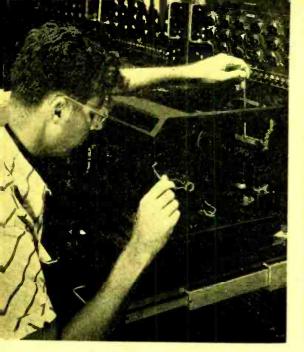
information from as many as three 16-channel or six 8-channel FM/FM telemetry systems to be available for "set up" at each oscillograph.

Each oscillograph rack is complete in itself. Separate panels are provided for each group of data outputs from the telemetry stations. This permits easy expansion or adaptability to other types of instrumentation for standardization. The basic design parameters were to provide proper installation and

(Continued on page 28)

Typical oscillograph record with trace lines and timing markers identified.





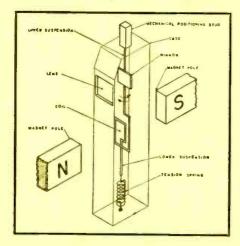
A technician is adjusting the position of a galvanometer in the oscillograph.

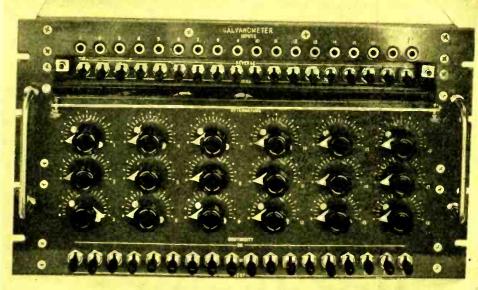
- Good sensitivity (low frequency, 0.033 ma./in.; high frequency, 40 ma./in.)
- 3. Wide frequency response (0-2000 cps)
- Rugged construction (suitable for field, mobile or airborne installations)
- 5. Accuracy (1%)
- 6. Replaceability (electrically and mechanically interchangeable)
- 7. Cost (\$100 to \$150 each)

Damping

The suspension of the galvanometer is a free moving element, so that its action under forced vibration follows all the theory and formulas pertaining to such motion. Of primary concern to the user is the motion of the element when a signal is applied. The mass of the movement and its inertia will distort the motion of the recorded output in relation to the input if rapid changes occur. Thus, the damping

Pictorial cutaway illustration of a typical D'Arsonval galvanometer element.





Front view of galvanometer panel, showing function controls as well as polarity switches which are recessed and normally protected by the hinged cover plate.

characteristics of the element as associated with its circuitry should be understood.

Basically, two fundamental damping mediums are used: (1) fluid damping, i.e., the suspension rotates within a viscous fluid, and (2) electromagnetic damping, which utilizes the back emf generated by the coil moving in a magnetic field. Actually, any galvanometer has additional damping effects produced by both mediums since the air in which an electromagnetically damped galvanometer moves produces some of the fluid damping effects, and the source impedance of a fluid damped galvanometer furnishes electromagnetic damping. The total damping is the arithmetical sum of all the per-unit dampings of the particular system.

Damping is used mainly to control the frequency response but it also introduces a phase shift (very slight), protects the galvanometer from violent overswings, and controls the time required to respond to sudden changes in current.

Normally, 0.64 per-unit damping or 64% of critical damping is used since it produces maximum frequency range with minimum inherent error. Unfortunately, many users procure galvanometers and standard shunts without realizing that circuitry associated with the galvanometer may at times seriously alter the damping characteristics.

Frequency Response

Whether electromagnetic or fluid damping should be used is mainly determined by the frequency response required and the driving current available. The electromagnetic type is generally more desirable since it normally has higher sensitivity and a far lower temperature coefficient. With the pres-

ent manufacturing techniques, it can be shown by the following basic formula that the limiting factor for electromagnetic galvanometers is the frequency response:

$$R = K/F$$

where R is the shunt resistance in ohms, K a constant of construction and installation, and F the frequency.

From the above, it is easy to understand how the shunt resistance R becomes lower in value as the frequency F is increased. Table 1 has been prepared from values in one of the instruction manuals furnished with a commercial recording oscillograph. Actually, the shunt resistance will never become zero but its value will become less than the internal resistance of the galvanometer and its low sensitivity will render it useless, fluid damping then being necessary.

The present oscillographs utilize a magnetic block to provide proper flux density for all the galvanometers in the instrument. Thirty-six galvanometer element installations are common in blocks of about four or five inches long. The frequency response range, linear \pm 5% at 64% of critical damping, of commercially available galvanometers is from 0-2000 cps. Greater sensitivity is obtainable by selecting elements—whenever possible—that have a flat re-

Table 1. Relationship between response, the shunt resistance, and sensitivity.

Frequency Response (cps)	Shunt Resistance (ohms)	Sensitivity (ma/in.)
0- 60	350	0.033
0-100	180	0.035
0-180	83	0.040

GUIDED MISSILE DATA RECORDING

JAMES B. WYNN, JR.*
and
SAM L. ACKERMAN**

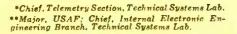
Air Force Missile Test Center Patrick Air Force Base

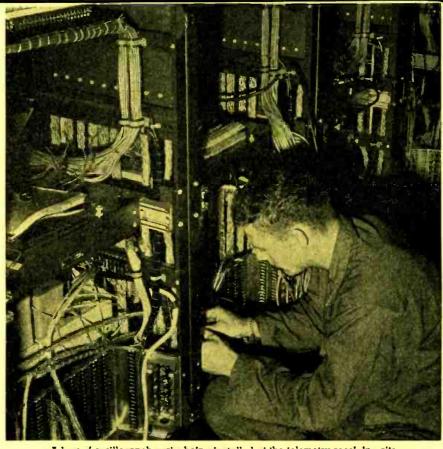
HOSE in nearly every craft or profession have at one time or another had the occasion to record data. In the fields of electricity and electronics, perhaps the furthest advances have been made in precision data indicating and recording of scientific phenomena. The recording oscillographs, utilizing galvanometer elements, provide an ideal means for observing and recording static and dynamic data, and will be the main subject of this article. Auxiliary or accessory equipment recently developed to provide flexibility and standardization of installation and operating techniques at one of the advanced missile radio telemetry stations at the Air Force Missile Test Center, Patrick Air Force Base, Florida, will be discussed in detail.

The Recording Oscillograph

For those not familiar with this type of recorder, it may be well to describe in some detail the fundamental aspects of this instrument. No doubt the oscillograph which would normally come first to mind would be a conventional electronic unit with a scope tube on the front, similar to the common TV set, and with a camera focused on the oscilloscope tube. However, as mentioned before, the equipment to be discussed uses a galvanometer as the active indicating element. The recording oscillograph is really quite simple -it is composed of a light source, a mirror moved by a sensitive meter movement to reflect the light, and a photosensitive medium to record the reflected light beam.

A review of the recording galvanometer oscillograph manufacturers listed in business guides indicates that this is a multi-million dollar enterprise. However, only a few of the available manufacturers produce recorders satisfactory for extensive use, and for precise measurements in the field of missile or aircraft testing. Most of the reasons for this will become self-evident, and a survey will show that





A bay of oscillograph racks being installed at the telemetry receiving site.

Photographic oscillographs are widely used to record data obtained from telemetering systems.

some of the mechanical and electrical characteristics of a few far surpass the others.

The Galvanometer

The galvanometer element, which on occasion may have been presented too mysteriously, is in reality a d'Arsonval meter movement without any pointer; a small mirror replaces the pointer. The movement of a current-carrying wire in a magnetic field is one of the basic concepts of electromagnetic theory and this principle is utilized in converting the electrical energy into mechanical energy in the galvanometer. Degree of force or motion produced is mostly dependent upon the flow of electrons, the number of turns of the conductor, and the strength of the magnetic field. Thus, with the present design, a compact element exists which very conveniently converts the flow of electrons to the proportional movement of a mirror. The moving beam of light reflected from the mirror is then projected on a ground glass screen for viewing, calibration and setup purposes, and is simultaneously projected onto photographic material to preserve the data permanently.

Main components required to make up the galvanometer are: a coil of wire, a suspension for positioning the coil of wire, a mirror, and a case or shell. Of course, the galvanometer must be positioned in a magnetic field for operation, but this magnet is separate and external for operational reasons. A photo-optical system is used in conjunction with the mirror since it provides the means for producing a record without extracting any appreciable energy from the galvanometer. Characteristics of the galvanometers in general use conform to the following:

1. Small size (approximate dimensions: \%" to 3/16" by 2" to 2\%")

4 3

HQA, HQC, HQD CASE 1 13/16"Dia. x 1 3/16"High



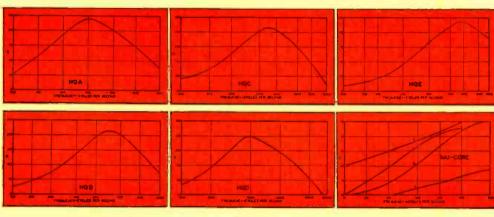
HQB CASE 1 5/8"x 2 5/8"x 2 1/2"High



HQE CASE 1/2"x 1 5/16"x 1 3/16"High

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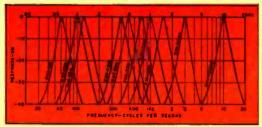


Type Ho.	Induct Val		Net Price	Туре Но.	Induc Va		Het Price	Type No.	Induc Va		Net Pric
HQA-1	5	mhy.	\$7.00	HQA-16	7.5	hy.	\$15.00	HQC-1	1	mhy.	\$13.0
HQA-2	12.5	mhy.	7.00	HQA-17	10.	hy.	16.00	HQC-2	2.5	mhy.	13.0
HQA-3	20	mhy.	7.50	HQA-18	15.	hy.	17.00	HQC-3	5	mhy.	13.0
HQA-4	30	mhy.	7.50	HQB-1	10	mhy.	16.00	HQC-4	10	mhy.	13.0
HQA-S	50	mhy.	8.00	HQB-2	30	mhy.	16.00	HQC-5	20	mhy.	13.0
HQA-6	80	mhy.	8.00	HQB-3	70	mhy.	16.00	HQD-1	.4	mhy.	15.0
HQA-7	125	mhy.	9.00	HQB-4	120	mhy.	17.00	HQD-2	1	mhy.	15.0
HRA-8	200	mhy.	9.00	HQB-5	.5	hy.	17.00	HQD-3	2.5	mhy.	15.0
B-ADH	300	mhy.	10.00	HQB-6	1.	hy.	18.00	HQD-4	5	mhy.	15.0
HRA-10	.5	hy.	10.00	HQB-7	2.	hy.	19.00	HQD-5	15	mhy.	15.0
HQA-11	.75	hy.	10.00	HQB-8	3.5	hy.	20.00	HQE-1	5	mhy.	6.0
HQA-12	1.25	hy.	11.00	HQB-9	7.5	hy.	21.00	HQE-2	10	mhy.	6.0
HQA-13	2.	hy.	11.00	MQB-10	12.	hy.	22.00	HQE-3	50	mhy.	7.0
HQA-14	3.	hy.	13.00	HQB-11	18.	hy.	23.00	HQE-4	100	mhy.	7.9
HQA-15	5.	hy.	14.00	HQB-12	25.	hy.	24.00	HQE-5	200	mhy.	8.0

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FILTER CASE M 1 3/16 x 1 11/16, 1 5/8 x 2 1/2 High



These U.T.C. stock units take care of most common filter applications. The interstage filters, BMI (band pass), HMI (high pass), and LMI (low pass), have a nominal impedance at 10,000 ohms. The line filters, BML (band pass), HML (high pass), and LML (low pass), are intended for use in 500/600 ohm circuits. All units are shielded for low pickup (150 mv/gauss) and are hermetically sealed.



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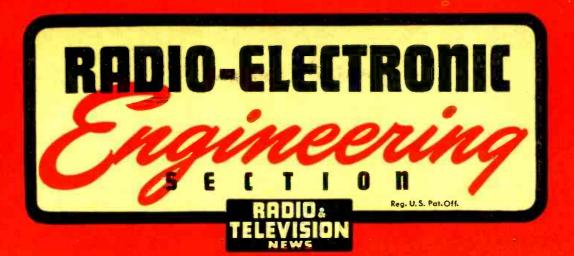
BM1-60]	BMI-1500	LM1-200	BML-400
BMI-100	BMI-3000	LM1-500	BML-1000
BMI-120	BMI-10000	LMI-1000	HML-200
BM1-400	HMI1-200	LMI-2000	HML-500
BM1-500	HM1-500	LMI-3000	LML-1000
BMI-750	HMI-1000	LMI-5000	LML-2500
BMI-1000	HM 1-3000	LM1-10000	LML-4000
			LML-12000

LINE TRANSPORMER CO.

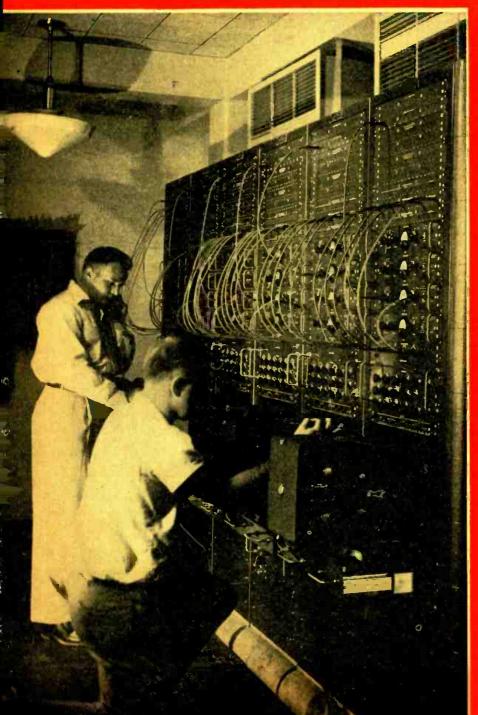
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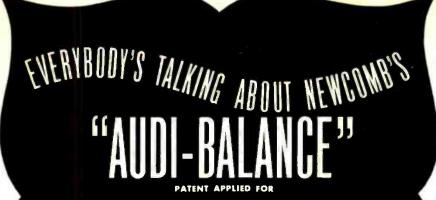
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Edited by H. S. RENNE and the Radio & Television News State

Technicians making final oscillograph calibration adjustments on guided missile data recording equipment at Patrick Air Force Missile Test Center. Mr. J. Wynn. Jr., co-author of article on P. 3, is at left.

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Write for Catalog

Ernest Lawrence, who has developed a simplified tri-color tube, which will soon be demonstrated in New York again; the original model was shown a year ago. According to Resnick, Paramount has invested well over a half-million dollars in this color tube, and \$300,000 in another TV development. a subscription system, which employs a coin box to unscramble scrambled pictures as they are received over a wire or otherwise.

As this column is being prepared, the merger issue is still deadlocked and appears to be a long way from settlement.

LONG DISTANCE overseas transmission is not only a project of our Voice of America, but many European countries, too. In Belgium, two 100-kilowatt transmitters are used for French and Flemish transmissions.

Several types of antennas are used; curtains directed toward the Belgian Congo and rhombics also directed to this zone and to this country, too. A reversible rhombic is also used to beam signals to Scandinavia.

TV is attracting the attention of many new European countries, reports from the continent indicate. In Norway, a substantial sum of money has been appropriated for experimental tests on a 7-megacycle and 625-line system. It is expected that the tests will last about two years.

Extensive tests are also being conducted in Spain over the Chamartin de la Rosa station. Under consideration are the erection of TV stations at Barcelona and Bilbao.

France will expand its TV activities, and by 1958 will probably have a nationwide service featuring their 819-line system.

A NOVEL LISTENING plan is in use in Northern Rhodesia, according to EBU. About ninety community receivers are hooked up for group listening in the Lusaka area.

In the early summer of '52 a 15-kilowatt short-wave transmitter was placed in service in Rhodesia. In addition, a mobile recording unit was sent out and covered over sixteen-thousand miles, making over 1300 discs of tribal choirs and other native music.

Community listening has also been reported to be very popular in Ceylon. By the end of September of 1950, 825 receivers had been installed at different community centers, rural development society offices, preaching halls, schools, temples, cooperative stores, etc.

Community broadcasting has also been used in Bombay, Madras, and Delhi. Today there are over 4000 receivers in operation all over the country.

Most receivers are operated from batteries and thus maintenance is a problem. To provide battery power, a network of battery-charging centers is used. In Madras, there are 67 such

(Continued on page 147)

RADIO & TELEVISION NEWS



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Presenting latest information on the Radio Industry.

By RADIO & TELEVISION NEWS' WASHINGTON EDITOR

THE PROJECTED TV SPAN across the nation, with stations in practically all of the states, often enthusiastically described by many in Washington and industry, seemed to be well on its way to becoming a firm reality, as the closing days of '52 appeared. With nearly 140 grants already issued to new TV operators in four-fifths of the states, and sincere promises from the Commission that hundreds more in all states would soon receive building permits, the prospects for the robust growth of TV looked bright indeed to everyone.

Whereas, only a few months ago, a few states seemed to be favored in the allocation race, nearly all were now receiving a share of the rich prize. The interesting expansion is illustrated in the partial listing of grants issued, at this writing, in the table on page 70.

In studying the table it will be noted that some existing TV areas. with v.h.f. stations, have received new stations which will be operated on the higher hands. One such market is Philadelphia, which now has three stations, and will soon have a u.h.f. station operated by WIP on Channel 29. Other cities in the new and old role are Greensboro, North Carolina and Johnstown, Pennsylvania. Here, Channels 57 and 56, respectively, will compete with the present very-high installations. The Channel 29 grant to the "City of Brotherly Love" was the first u.h.f. authorization to a major metropolitan center and represented an important trend in approvals from the processing staff. It had been felt that grants of this type would be delayed and perhaps not issued until 53. The earlier issuance was described as a major change in philosophy toward large city high-low band operation which would serve to spark sales of TV sets in areas believed riding close to a saturation point among viewers. In Philadelphia, dealers and distributors beamed when the high channel announcement appeared in the local papers. Notwithstanding the fact that the new station will not be placed in operation for some time, interest soared and sales jumped.

THEATER TV, which had a very brief airing during the late winter months of '52, became steeped in gloom as the official hearings began in '53. Many in

the theater industry felt very doubtful about the ultimate success of allocations of channels for theater circuits.

According to the general counsel for motion picture exhibitors, the Commission has shown little enthusiasm for the assignment of channels to the theater. He indicated that most of the questions asked by the Commission during the hearing seemed to indicate that the legislators were not too keen about the proposed system. It was hoped, he said, that the facts presented during the lengthier hearings will convince the Commission that the theaters should have the requested channels, and as soon as possible.

THE ROARING DEBATE in the hearing offices of the Commission concerning the merger of ABC and Paramount, which it was generally felt would taper off with the release of Hearing Examiner Leo Resnick's approval of the merger, flared up with the objections filed by the broadcast bureau of the Commission.

The Resnick report was an extremely interesting document, covering every phase of the case and revealing some intriguing data on Paramount's role in the television industry. It was noted that the motion picture producer began to study the possibilities of TV as early as 1937, when it invested in Du Mont. They then applied for experimental television licenses in both Los Angeles and Chicago from which developed the present stations KTLA and WBKB. The transmitters for these stations were said to be among the first built, and the antenna and transmitter at Mount Wilson near Los Angeles was noted as being the first to be established at that focal point.

The report also indicated that the flicker maker has been instrumental in the development of video recording and large-screen TV, too. They have developed a camera and projector which can record TV images almost instantaneously, after they are received, on film said to be suitable for almost immediate projection on large screens used in theaters. In addition to these activities in TV, it was said, the company has become interested in color TV, through participation in the company formed by Dr.



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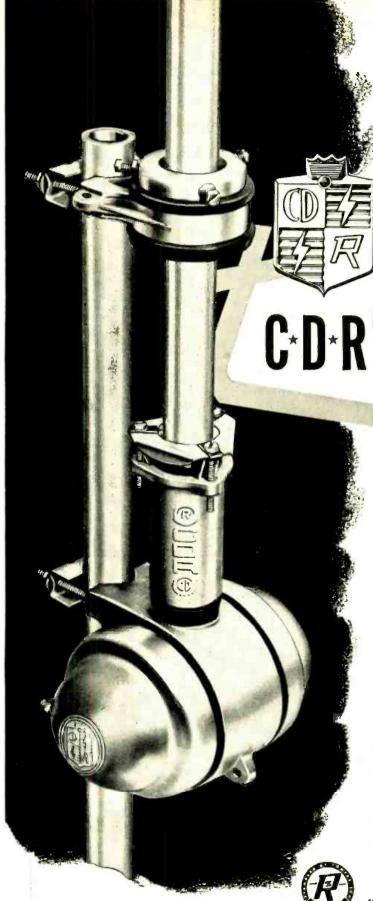
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February, 1953





THE TELEVISION SERVICE OPERATOR

MANY letters coming to our desk are from technical trainees attending classes in our trade schools and colleges. These students, generally, state that they are learning radio or television theory and practice as preparation for a career in the servicing business. Typical questions asked include: "What do I need to start a service shop?", "Should I specialize in television service exclusively or should I consider both radio and television?" and "What test equipment will I need for television servicing?"

It is a well established fact that television installation and service requires considerably more test instruments and other equipment than does radio. Such equipment can be very costly and, in the case of the independent service technician, almost prohibitive in areas of limited clientele. TV test equipment must be sensitive and accurate. In many cases it is too massive or heavy for home servicing and belongs on the test bench where it can be conveniently and effectively used. A well-equipped shop is a prerequisite for television servicing.

The service shop, however well equipped, is but one link in the chain of equipment required by the progressive service operator. Successful TV service contractors have learned that to cope with the many problems that arise in TV areas they must not only have a well trained staff of technicians but that their men must be properly equipped with the tools of the trade.

Paul Forte of the Television Contractors Association recently named several important components that are required to render good service. They include a panel truck or specially fitted car. In it must be carried a supply of tools, equipment, and spare parts that are in most common need. When a television set can't be repaired with these facilities, the car or truck must be suited so that a chassis and/or cabinet can be brought back to the shop for bench work. Such vehicles cost money and represent another investment on the part of the service contractor.

Since there are, roughly, about eighty different makes of television sets and thousands of models, the effectively operating contractor must have a complete library of diagrams, schematics, and service notes. These cost money, and taking care of them, adding to them, and using them costs time and money. Without them no man can claim that he is ready to service television.

A service operator cannot properly

function unless he has records of all service calls. These are not things he keeps in his wallet. He's got to have files and forms and he's got to have somebody work on them to keep them up-to-date. That means he has to have an office and someone in it to handle service requests and dispatch them promptly. These things cost money, a cost that can't be borne by the independent technician. If he does bear them, then he isn't an independent technician any longer; he's either a contractor or a service operator.

He must have special equipment and facilities for installations which include the erection of antennas. This, definitely, requires a truck. He can contract the antenna installation to someone else but that is hardly a good method of conducting a business. Trucks, too, cost money and are an integral part of the investment that must be put into a television service operation, as well as into the cost of service.

Since he's dealing with expensive television equipment in the customer's home, he has to carry Public Liability and Property Damage Insurance. He has to carry other insurance on his vehicles, test equipment, parts stock, and other facilities. It costs more money! It's all part of the investment that goes into a properly handled service business.

If the so-called independent technician says he doesn't need these things in order to maintain himself in the television service business, he is kidding himself. Certainly he won't kid the public, upon whom he depends for business

There is little time, if any, for the aggressive technician to relax and sit back with a hope that he can keep pace with the fastest growing industry in our time. Instead, he must constantly keep abreast of new developments. in addition to performing his routine tasks as each day passes. He must continually study new circuits, new products, new applications, and new techniques.

He must learn all that he can about u.h.f. behavior, circuitry, antenna theory, and troubleshooting. He must employ common sense in his relationship with the public he serves. He must conduct himself as a successful business man and be ethical.

If he trains himself NOW and if he builds a firm foundation based on the experience of other technicians—the television service operator can certainly look to a future of interesting opportunities in this industry we choose to call electronies. O.R.

RADIO & TELEVISION NEWS

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No. Size 8253 3½" Single 8257 7½" Single

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G-U	
UNIVERSAL	STAND-OFFS
(Machin	e Screw Type)

No.	Length
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8032	5 ½"
8035	71/2"



UNIVERSAL STAND-OFFS (Wood Screw Type)

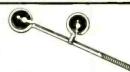
No.	Length
8027	31/2"
8028	51/2"
8029	71/2"
8030	12"



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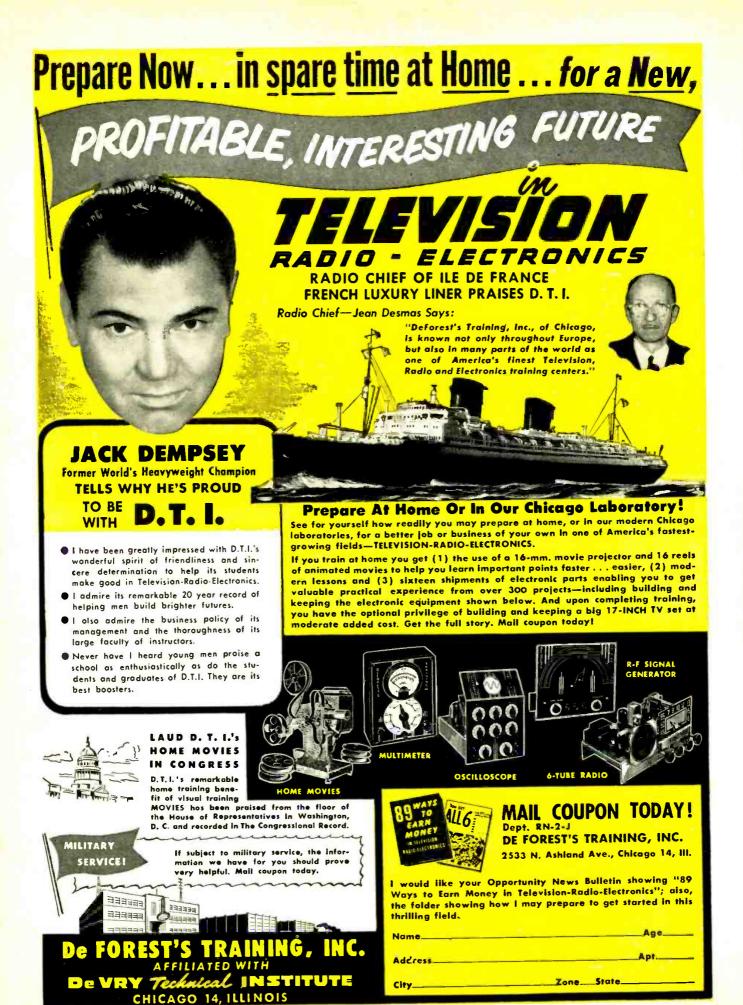




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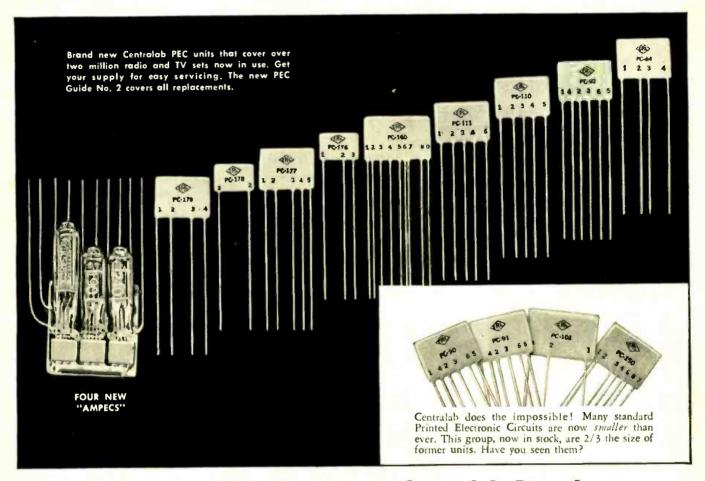
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RADIO-ELECTRONIC ENGINEERING EDITION

RADIO & TELEVISION NEWS

FEBRUARY 1953

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A.F. WATTMETER

ULTRASONIC MICROSCOPE

COMPUTER RELIABILITY

CHARACTERISTICS OF DIGITAL AND ANALOG UNITS

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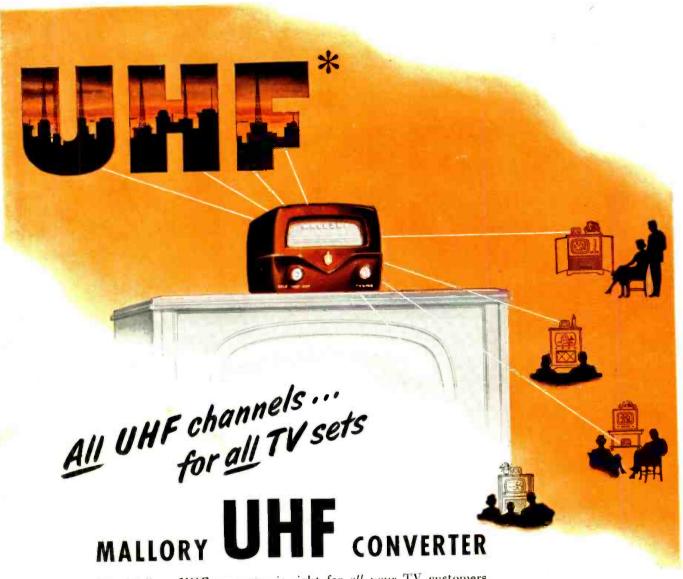
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J. S. H. Sales Company 153 Jersey City Technical Laboratories 88 Kelsey Company 143 Klein Company, Manuel 135	V & H Radio & Electronics
Lampkin Laboratories	Waldom Electronics, Inc
Lee Electronic Laboratories, Inc. 108 Leeds Radio Company 148 Leotone Radio Company 145 Lidher, Otto 118	

reduce this effect although other symptoms of distress may occur. In the event of an input signal containing rapidly damped wave trains, such as might be produced by the phase-mixing technique, demodulation-distortion components will tend to occur at a higher rate than in a signal containing wave trains of fairly long duration. Similarly, loudspeaker hangover may represent a greater problem due to the increased intensity of the transients.

In conclusion, it appears that controllable phase-shift mixing in reproducing equipment has a number of unique advantages in securing the best possible sound. This technique can be used for corrective purposes in obtaining greater clarity of reproduction either in the original signal, in the audio equipment being used, or in the acoustic characteristics of the listening environment and appears to achieve some of the desirable characteristics found in live listening or twochannel binaural reproduction. The ability of phase-shift mixing to greatly affect transient-to-sine-wave relationships as well as altering the apparent pitch of asymmetric sounds likewise suggests the need for a re-evaluation of many audio practices, circuits, and reproducing components. In the author's experience it is possible to obtain improved clarity and quality of the reproduction of indifferently good audio equipment through use of the acoustic phase mixing alone, inasmuch as multiple-path sound reproduction tends to allow the phase-sensitive properties of the auditory apparatus to be used by the listener, a situation not found when listening to the direct output of a single radiation source. Similarly, the experimenter will undoubtedly find that phase shift mixing represents one of the most versatile and interesting techniques of varying the characteristics of an audio system.

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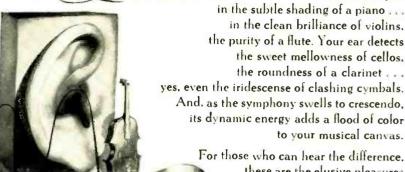
Page	Credit
36 (Fig. 1) Technical Appliance	
36 (Right) Walter L. Sch	
27 (Fig. 4), 38 (Fig. 8C), 56, 51, 113, 115, 122, 127. Radio Corporation of A	111.
37 (Fig. 6) Davis Elec	
46 Emerson Radio & Phonograph	
55National Broadcasting Corp.	

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ERRATUM

In the circuit diagram of Fig. 7, page 62 of the November issue ("4 Problem Preamps"), a 1 megohm resistor was omitted from the diagram. It should be inserted between the grid of the second half of the 12AX7 tube and ground.





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Tone Controls

(Continued from page 57)

equipment and the listener. The general relationships to observe are that phase shift and subsequent mixing tends to lower the apparent frequency of transients and asymmetric waveforms and if the phase rotation is greater than 90 degrees will tend to The opposite suppress sine waves. relationship is when phase shift, inversion, and mixing takes place in which event the apparent frequency of transients and asymmetric waveforms is increased for phase rotations of less than 180 degrees. Likewise. sine waves will tend to be suppressed in the case of phase rotations of less than 90 degrees.

As mentioned earlier, the effect of phase-shift mixing is generally to increase the ratio of transients to sine waves in the reproduction. In addition to some of the previously mentioned advantages this effect may cause reproduction with greater "presence," apparently due to the fact that transients stimulate individual room resonances to a greater degree, an element apparently easily recognized by a listener thoroughly familiar with his particular acoustic environment. Nevertheless, the reproduction of a signal having a high transient-to-sinewave ratio usually means that the peak power handling capabilities of the audio system must be considerably greater than that of a system handling continuous wave trains in order to present the same apparent loudness level to the listener. Likewise other problems may present themselves. such as an interesting form of distortion which the author characterizes as "demodulation distortion."

In considering speech or music it should be realized that the various wave trains tend to produce a modulation envelope, which can be produced either by a tone of constant pitch or by a combination of unrelated frequencies. Usually these modulation envelopes vary from a few cycles-persecond on up into the audible range. If nonlinearity or rectification is present in the audio system, such as might be caused by second harmonic distortion in an amplifier stage, then the envelope components will tend to be demodulated and will appear in the output as a spurious low frequency tone. In the case of a phonograph pickup having a serious ringing resonance, even in the ultrasonic region, the effect of demodulation distortion will be to introduce spurious noise components of a frequency dependent upon the amplitude of the exciting transient and the consequent duration of the ringing envelope. The cure for these effects is, of course, low distortion circuits, however, it is of interest to note that if nonlinearity is present in the loudspeaker system the use of tweeters and woofers with low frequency acoustic cut-off may help to

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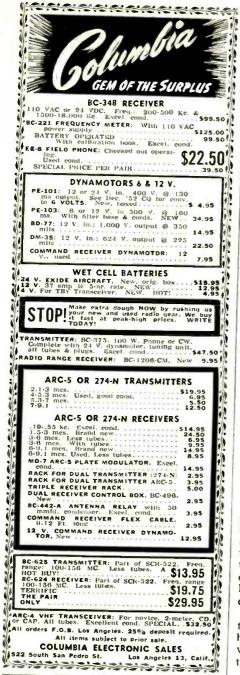
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cal service associations should arrange themselves in small groups so that members can meet regularly at a central point close to their homes. Perhaps twice a year the entire city association could sponsor a big meeting in some central location to hear an outstanding lecturer or plan a service clinic that would feature discussions of the important technical developments or servicing problems.

Service Industry Identification

A common complaint among service shop operators is that manufacturers are not interested in the problems or welfare of the independent service industry. This is not true for the average manufacturer realizes full well that a strong, financially successful servicing industry will provide a healthy, stable market for his product. It is equally obvious that a manufacturer cannot get enmeshed in the problems of the service industry without getting involved with some laws that tell him to keep his nose out of other people's business.

The independent service industry has several unused "tools" available to it that would lift the entire activity to a much higher level of importance in the industry. The most important of these tools lies in the way you order tubes, parts, and supplies from your jobbers. How often do you speci-fy the brand names you want when you order tubes, parts, or supplies?

How important are you in any manufacturer's "chain of distribution"? If you do not order your tubes, parts, and supplies by brand name—and insist on getting the brands you order-you are not important at all. You are merely a small part of a mass market for these products. Your parts jobber is the key man in the manufacturers' chain of distribution because he selects the brands that you accept without question.

Consider this: If you order fifty tubes from your jobber and accept any brand that he supplies, you as an individual mean nothing to any individual tube manufacturer.

But suppose you specified a particular brand when you ordered tubesand insisted on getting that brand. Then you become very important to that tube manufacturer because your preference for his tubes has placed you on his sales team. Your jobber will become less important in that manufacturer's chain of distribution because he knows that if one jobber will not or cannot fill your order for his brand of tubes you will go to some other jobber who will. You become a very important factor in that manufacturer's distribution chain,

The independent servicing industry would increase its importance immeasurably in the eyes of manufacturers if every service shop operator would specify a particular brand on all tubes, parts, supplies, and accessories he orders from his jobber-and would insist on getting the brands he specifies.

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the complexion of the service industry. Prior to the advent of TV it was entirely possible for an ingenious technician possessed of some business acumen, able to get along well with people, and willing to work long hours, to make a pretty good living out of servicing radios. Not much equipment was needed for radio service work since the characteristics of the conventional a.c.-d.c. circuits were so well known that almost eighty per-cent of the jobs could be completed without the use of even a v.o.m.

TV changed all that. Larger chassis, more tubes per set, multiple circuits, bulky picture tubes, and on the job servicing, plus a number of other factors, made it necessary for the operator of a TV service business to get familiar with work planning, organization of time, and adequate record keeping. The need for precision test instruments, trucks, larger stocks of tubes, parts, and supplies add up to a substantial investment that can seldom be carried by the income from one man's time. So the TV service business man has employees and all of the attendant responsibilities of keeping his help profitably occupied.

TV service adds up to a tremendous dollar volume business. This attracts the attention of men who are not necessarily TV technicians. They are basically business men who know that good management can operate any business at a profit where there is such a large and growing market for the needed service.

Successful TV service operators are businessmen primarily, whose major interests are in selling service, reducing costs of operation, watching inventories, and planning the work of their employees to make a profit from the labor they are buying.

These men need service business associations. They need to know their competitors in the service business. They need to cooperate with their legitimate competitors to discourage practices that are both unprofitable and not in the best interests of the owners of TV sets. A good trade association can actually create more business in any given area through programs of user education.

Technical Associations

Then there are many thousands of men employed in servicing who are mainly interested in the technical phases of the business. Lots of men now engaged in TV receiver servicing do not aspire to own their own service businesses. They prefer the technical side of the business and would rather work as a top technician in a good service organization than run their own service businesses.

These men prefer to belong to technical associations where they can discuss circuitry and technological advances with their fellow technicians. We should have more such associations in the industry. Perhaps they could be termed ISE—Institute of Service Engineers. In large cities techni-

RADIO & TELEVISION NEWS

Hal Chase of Chase Television Service, president of the Association, gives a lot of his time in planning and directing the Association's activities. "TSA News" has been developed into a self-supporting house organ with a wide circulation in the area. Recently they launched a "consumer" bulletin which is included as a section of "TSA News." It is available in quantities to members for mailing to their customers. The consumer bulletin carries TV-connected news of interest to set owners and is supported by merchants who advertise in it.

The Association holds regular monthly business meetings. These are held in a private dining room in a downtown hotel with members and guests meeting for dinner. After dinner a guest speaker usually gives a short talk on some subject of immediate importance to service executives with the regular business meeting and round table discussion of problems following it. Parts and set distributors attend these monthly business meetings.

The technical meetings include at least one general service clinic each year. The purpose of the service clinics is to permit technicians to get circuit information on all standard TV sets in as short a time as possible. Distributors display their latest model chassis and have either factory or distributor service personnel on hand to discuss circuit individualities with service technicians.

TTLB Lecture on U.H.F. TV

The TSA recently sponsored the Television Technicians Lecture Bureau's lecture on u.h.f. TV. In this type of lecture the technician is able to get a complete picture of all possible installation and servicing requirements that may be demanded for u.h.f. reception. It covers u.h.f. converters and how they are applied to present v.h.f. receivers. Sample units of most converters are displayed and alignment procedures are demonstrated for the converters that may need to be aligned in the field.

The presentation then covers the circuitry of the new u.h.f.-v.h.f. combination receivers and technicians are shown what they may be called upon to do in servicing these new sets in the field. And, since the antenna system may possibly be the most important element in the reception of u.h.f. programs, either in converted v.h.f. sets or in the new u.h.f.-v.h.f. combinations, an extensive coverage of u.h.f. antenna and systems requirements is included as a part of the lecture.

These technical training programs as carried out by TSA and ARTSD are planned to conserve a technician's time by giving him the maximum amount of practical information in a minimum of time.

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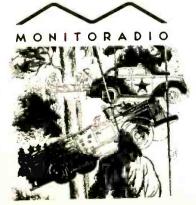
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Why Do Service Associations Fail?

Many service associations have been formed with a great deal of enthusiasm only to quickly wither and die from ennui. Why? The first reason is that associations usually are formed when service businesses are in trouble. Those who join think an "Association" will solve their troubles. Usually, the first acts of an association are along the lines of "forcing" someone to do something or to quit doing something that the members think is hurting their businesses.

For an association to be successful it must first be ready to "give" something to the industry in which it operates. Its members must be willing first to get their own business houses in order before they start asking others to clean up theirs.

A successful organization must have a series of self-help programs. These must be carefully planned, intelligently organized, and carried out aggressively. This requires time, effort, and thought on someone's part. It also takes money. If the officers of an association are not willing-or not able -to give unstintingly of their time and effort to develop and carry out these self-help programs the organization will wither away. If the members are unwilling to pay the dues necessary to defray the expenses necessary to operate an association it cannot exist.

The first requirement of an association is to have a carefully planned series of activities that will cover the business phases of a service company and the technical developments in the industry that affect service, and will provide an opportunity for the members to get acquainted socially. The second requirement is for the association to have an officer, or officers, who can afford to give the time and have the natural "drive" to keep this program rolling.

All too often after an association is formed the members are too husy to engage in association activities when business is good and they can't afford it when business is bad.

A Case History

The Television Service Association of Michigan is a comparatively new organization that has created an important place for itself in the TV industry in Detroit. Like ARTSD and other successful associations, it is primarily concerned with the problems of service as a business but at the same time, keeps its members and Detroit technical service personnel abreast of technical developments by sponsoring service clinics and lectures.

TSA has the active support of both set and parts distributors in the area and they work closely with the Better Business Bureau and law enforcement agencies in policing service business practices in the city.

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RADIO & TELEVISION NEWS

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January, 1953

part of a man and his wife to the customers who had made their success possible

Close to one hundred manufacturers' representatives and company officials attended the party. It was high-lighted by the surprise presentation of a Certificate of Appreciation to John T. Thompson, replacement tube sales manager for GE, for his company's consumer campaigns on behalf of the independent service profession. The presentation was made by Fred Colton of Graham & Colton, president of the Associated Radio & Television Service Dealers, Inc., as an award from the Association.

Ray and Polly Whitehead were also surprised with an ARTSD Certificate of Appreciation which was presented by Sam Oppenheimer of the Columbus TV Laboratories, vice president of the association.

Lesson in Cooperation

For many years Columbus, Ohio, has been one of the "cleanest" radio-TV service areas in the country. When the TV boom struck it attracted, as in all other areas, some "fast-dollar" and quick change service operators. But down through the years the ARTSD had created a healthy respect for the quality and high standard of service performed by its members. They were able to get the wholehearted support of the Better Business Bureau and other civic organizations in weeding out the parasites who were trying to feed off the ignorance of the set-owning public about what they should pay for and receive in the way of competent TV service.

There are two important factors back of the continuing success of the Associated Radio & Television Service Dealers in maintaining a healthy climate for radio-TV service as a profitable business activity in Columbus. The first is the amount of time that is given by its officers to create and carry out the Association's programs. These well-conceived programs regularly cover all facets of interest to the men engaged in the business of service. First, they hold their regular monthly sessions where they discuss frankly all phases of the operation of their businesses and all factors that influence the course of their businesses; next they conduct a regular series of technical sessions to keep their members and their members' employees abreast of the fast-growing technology of the industry; and third, they have regular social gatherings that enable the members' families to get acquainted.

The second important factor in ARTSD's success is the excellent cooperation between the Association and Columbus parts and set distributors. Every three months the members of ARTSD invite all Columbus distributors to have dinner with them and afterwards air their grievances against each other. Columbus distributors have cooperated whole-heartedly in this program and it is quite possible that, as a result, Columbus is a poor



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RADIO-TV Service Industry News

AS REPORTED BY THE TELEVISION TECHNICIANS LECTURE BUREAU

WHEN officials of manufacturing organizations attend gatherings of people now engaged in the business of servicing radio and television receivers they express amazement at the evident high caliber of the men who own and operate today's service businesses. In the eves of too many people in the industry who seldom come in direct contact with present day service business executives, the servicing of television and radio receivers is still handled by a faceless, motley mass of people who, in the aggregate, constitute a tremendous market for replacement parts, tubes, and supplies, but whose identity as individuals is of no consequence. Many people still hold the mental picture of the average individual service business operator as being an unkempt character who is content to work for a marginal income and who is either not interested or incompetent to run his service activities in a business-like manner.

A Distributor's Party

A few weeks ago we were invited to attend a parts distributor's party for his service customers. This was something new. There are endless parties given by manufacturers for their distributors and by the distributors for the representatives, and vice versa, but this was the first time we had had an opportunity to attend a party given by a parts distributor for his service cus-

tomers and their wives and sweet-

Seven years ago a former radio service technician started a parts distributing business in Columbus, Ohio. Ray Whitehead and his wife and partner, Polly, launched the infant business in a modest-sized storeroom not overly stocked with replacement tubes, parts and supplies. The business grew rapidly and on their fifth anniversary, the Whiteheads threw a party for the service business customers in central Ohio whose purchases were responsible for the success of the business.

They held another party on their seventh anniversary. They rented the ballroom of a popular hotel to entertain their customers and rented all of the other rooms on the same floor so their suppliers could display the latest products and meet the Whitehead customers. Enough chairs to seat eight hundred people were set up in the ballroom and another two hundred in an adjacent room to accommodate any additional guests who might attend.

The expression "the place was bulging at the seams" is the only adequate description of the tremendous crowd of service people and their wives who accepted the Whiteheads' invitation to attend their anniversary party. Possibly more than 1500 service executives, technicians, and their wives came. It was not a "sales meeting"—it was a gesture of appreciation on the

Part of the crowd of more than 1500 service executives, technicians, and their wives who attended the service party given by Whitehead Radio Company, Columbus, O.



RADIO & TELEVISION NEWS

Two insulated mounting strips attach to the top of the modulator case at each end. The r.f. chassis grounds to one point only on the modulator case to foil v.h.f. circulating currents flowing between the metals. (Those circulating currents can cause untold grief by contributing to excessive r.f. feedback!) In addition to providing insulation, the strips are saw-slotted to afford footing for the bottom edges of the r.f. chassis, preventing slippage.

The case and r.f. chassis are fabricated from heavy brass plate, silverplated, and polished. It is emphasized that this development model was silver plated not to enhance its electrical characteristics, but only to satisfy an aesthetic whim of the designer! The reader may construct a similar transmitter upon pewter or platinum, depending upon his taste and the size of his bankbook.

In constant use for the past several months, this transmitter has worked the same DX as have stations using more than five times its power input of twenty watts. Ninety-five per-cent of the DX contacts were solid QSA 5. using a four-element beam from a flat city location. This operation indicates that at W6WGD, a hilltop and kilowatt seem unnecessary for more than routine enjoyment of the two-meter band.

"THE BACKTRACKER"

By JOHN M. HAMILTON

WITH grounded plate and cathode, no Wgrid leak nor "B" supply, maybe our little set, "The Backtracker," shouldn't work at all; yet it does, bringing in local and DX stations with plenty of headphone volume.

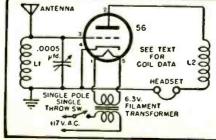
The set was built around a discarded Type 56 receiving tube (any other indirectly-heated tube will work), which obviously operates as a "square law" detector. The two coils shown in the circuit diagram form a grid-plate coupler, which increases the sensitivity and selectivity.

Coil L₁ consists of 100 turns of #28 enamel wire on a 1½-inch cardboard tube. L₂ consists of 300 turns of #28 on a 1¼ inch form. L₂ slides inside of Li to form the coupler.

Tuning is easy. Rotate the condenser until a station is heard; then pull out L2 until the volume is strongest. The frequency may be changed considerably by pulling out L₂ several inches. From our home in Youngstown,

Ohio, using an ordinary 70-foot aerial. we've logged 27 broadcast stations. Our best DX so far is KOA, Denver, 1500 miles away-logged in the wee hours! 30-

Complete schematic of a simple one-tube set.



January, 1953



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end of the QSO. In order to meet these requirements, the modulator was designed to offer "broadcast" fidelity, supplying approximately ten watts of undistorted peak voice power to the carrier from an unusually small pack-

Exclusive use of miniature dual triodes results in the smallest practical size for the modulator. With reference to Fig. 7, note that a single cascaded 12AX7 comprises the speech amplifier for a crystal microphone. An r.f. decoupling filter, R1-C1, serves to isolate r.f. from the speech input grid.

The shunt-coupled UTC 0-6 "Ouncer" transformer drives a 12AT7 amplifier; this dual triode provides push-pull amplification to drive a second 12AT7 cathode-follower stage which, in turn, drives a 12AU7 as the class B modulator. Use of the cathode-follower driver tube eliminates the necessity for a driver transformer, an item of some importance where space is at a premium.

Any type of small modulation transformer designed for 10,000 ohm plateto-plate class B service may be employed rather than the unit recommended, the prerequisite being that its secondary should encompass an impedance range of 3000 to 5000 ohms to match the class C load. The transformer used provides three secondary taps of 3000, 3750, and 4500 ohms. At a plate voltage of 300 and loaded to 70 ma., the class C load represents 4643 ohms, matching the 4500 ohm tap closely enough to result in linear modulation

Power supply for the modulator remains identical to that required for the r.f. section, although its current rating need not exceed 100 ma. The 12AU7 has a static plate current of 15 ma. with -221/2 volts of battery bias and peak current of 75 ma. Oscilloscopic inspection of the 20-watt carrier shows linear modulation of approximately 97%, while signal reports place special emphasis upon the excellence of quality and the powerpacked audio sidebands.

Fig. 6 illustrates modulator construction; a case measuring 10" long, 31/4" deep, and 31/2" high encloses the complete unit. Parts layout follows schematic circuitry down a straight line from input to output; components bolt to a strip of aluminum "breadboard" which mounts above the bottom of the case upon four corner stand-off spacers. Fig. 2 shows the breadboard inverted to illustrate the wiring technique and parts placement.

When constructing the modulator, it will be found that point-to-point wiring becomes necessary, as the compactness of the unit is similar to that of a hearing-aid amplifier. Extreme caution in wiring will result in the least feedback in a high-gain system of this size. When operating properly, the gain control may run wide open with zero feedback, although this offers more gain than is required for the normal modulation of 20 watts input.









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RADIO & TELEVISION NEWS

Two-Meter Master

(Continued from page 41)

The filter network, R_8 - C_{13} - C_{14} , helps to isolate stray r.f. from the modulation transformer. The r.f. chokes RFC2 and RFC_3 are identical, wound on a short $\frac{1}{4}$ " diameter polystyrene or ceramic dowel. 24 turns of #28 enameled wire provide adequate choking at 144 mc

All tube heaters are wired so that the "B-" ground return serves as half of the heaters return; at the final amplifier, the 832A heaters bypasses

to ground through Cis.

Cross neutralization of the final shows lengths of solid hookup wire connected from the grids, across the back of the tube socket, and out through small holes in the socket mounting bracket. The holes support feedthrough bushings, which rigidly support the neutralizing wires running parallel to the plates outside the glass envelope of the tube. When neutralizing the amplifier, start with wire lengths adjacent to the tube's plates extending about ¾" from the feed-through bushings. Clip off about a sixteenth inch at a time until the amplifier stabilizes. Do not try to operate the amplifier without neutralization; at these frequencies, its use becomes mandatory unless one was born under a very lucky star!

The r.f. section requires 300 to 325 volts d.c. at a current of 175 ma. Any power supply meeting these requirements may be used, and most junk boxes may provide enough parts to run 20 watts input. Separate power supplies are employed for the r.f. and audio sections of the transmitter.

Physical construction of the r.f. section is made upon a "U" channel measuring 10" long, 314" wide and 214" deep. Inasmuch as W6WGD has been operated from hotel rooms and similarly restricted spaces for the past twenty years, an absolute minimum of space was utilized in this design, if only from force of habit. The unit may be constructed according to its builder's preference, although a similar parts layout should be followed.

Due to its small size, the transmitter uses miniature one-inch meters to read final grid and plate currents.

With reference to Fig. 4, note the point-to-point wiring; resistors Rs and R_i are bolted together through their lengths to form a single unit, supported by heavy wires making connections to various tie points. The power input connector provides support for this and other circuit components, as does the second tripler tube socket. Actual constructional features are left to the ingenuity of the reader.

Modulator Section

To convey maximum intelligence, the carrier must be modulated as fully as the law allows; the speech should have good fidelity and crisp response to be clearly defined at the receiving

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Korean Broadcasting System, Office of Public Information, Pusan, Republic of Korea. Schedule is 1600-1830, 2100-2400, 0300-1030. (Cushen, N.Z.)

A station noted on 9.310A around 1710-1847 sign-off in Danish and Greenlandic is believed to be Godthaab, Greenland. Has bad QRM at times. (Bellington, N.Y.; Kary, Pa.)

A new outlet in Sao Paulo, Brazil, is noted on 11.855 around 1830. (Niblack, Ind., others)

ISWC, London, says "The Voice of Zion," Israel, has an experimental transmission to South Africa on Sundays 0630-0730 over 15.550 (frequency may be varied).

YVMG, Radio Popular, 4.810, Maracaibo, sent QSL card; listed YVMG, 4.810, 2 kw.; YVMH, 1250 kc., 2 kw. QRA is Apartado Postal No. 347, Maracaibo, Estado Zulia, Venezuela. Says is affiliated with BBC, NBC, United Nations Network of Peace, as well as Radio Programas de Mexico. (Patterson, Ga.)

Schedules of *Radio Tirana*, Albania, on 6.560, 500 watts, and 7.850A, 3 kw., are 2300-0100, 1100-1130, 1215-1700; *English* is listed for 2345, 1600. (Radio Sweden)

Bellington, N. Y., notes the clandestine Yugoslav Emigrant Station on 6.887A parallel with an outlet on 7.500A around 1750; has man and woman alternating in European language.

British Honduras is to have a better short-wave service soon; a 5 kw. shortwave station is expected to be in operation at Belize by next March. (Catch, England)

Radio France-Asie, Saigon, Indo-China (Vietnam), has been noted back on its old 11.83 channel from 11.924A, signing off 1125. (Balbi, Calif.)

Sanderson, Australia, notes a much improved signal from the Chinese Air Force Station, Taipeh, Taiwan, on 9.750A at 0700 when has *English* ses-

sion. May have installed a new and more powerful transmitter?

Radio Free Europe noted on 10.300A when tuned 1000; melody followed by call, then program in Hungarian; news in Czech 1015. (Pearce, England)

The Free Greek Radio appears to be on about 6.970; intercepted at 2255 when had Greek language session running past the hour. Signal was gone when retuned 2315. (Kary, Pa.)

A clandestine station announcing as "Freidomsender" is heard in Sweden on 7.700 at 0230-0245.

EDV10, Estacion Escuela Radio S.E.U., Madrid, sent usual QSL card; said is on 7.170 but enclosed schedule for Esperanto transmission (at 1430) which gave channel as 42.33 m. or 7.088. (Pearce, England)

When this was compiled, the BBC's programs for the Western Hemisphere were listed-North American Service To Canada, USA, Mexico, 1000-1215, 17.715; 1300-1545, 11.930 (Mon.-Fri.); 1500-1545, 9.825 (Mon.-Fri.); 1545-1700, 9.825, 6.195. Special Programs-For Falkland Islands, Sun. only, 1130-1200, 17.810; for West Indies, 1815-1845, 9.580, 6.035. General Overseas Service-To West Indies, Central America, South America (north of Amazon), 1500-1700, 11.750; 1700-1815, 9.580, 6.035; 1845-2200, 6.035. To South America (south of Amazon), 1500-1700, 11.820; 1700-2200, 9.410, 6.110. To 1700-1845. USA, Mexico, Canada, 9.825; 1700-2200, 6.195; 2300-0115, 6.110.

Acknowledgment

Many thanks for the splendid cooperation during 1952. May 1953 bring you the best in SWL'g. Sorry that space limitations would not permit the use of more of your fine reports this month. Please continue to send your best tips to Kenneth R. Boord. 948 Stewartstown Road, Morgantown, West Virginia, USA. Thanks!—K.R.B.



duled 0130 on 6.100, 9.505; 1100-1115, 6.100, 7.200; 1315-1330, 6.100, 6.150; 1645-1700, 6.100, 6.150 (WRH)

Press Time Flashes

When this was compiled, a station on 4.950, identifying (in English) as "the Broadcasting Service of Radio Belize" was being heard around 1830-1904 closedown. (West, Va.) Good level in West Virginia but with CWORM and aircraft phone QRM. Is British Honduras.

The Radio Clube de Angola, Luanda, Angola, is now using a new channel of 4.873 in parallel with 9.632, 11.865; heard from around 1330. (Ridgeway, South Africa)

The Central Broadcasting Station, Lusaka, 4.826. North Rhodesia, is noted around 1210 with dance records: with talk in English 1230, BBC news relay 1300; probably signs off 1400. (Pearce, England) Ridgeway, South Africa, lists ZQP at 0700-0900 on 7.220: 0900-1100 on 7.220 and 4.826; 1100-1230 on 7.220, 4.826, and 3.275; 1230-1400 closedown on 4.826. 3.275.

The Japanese Communist station Radio Free Japan broadcasts on 10.180, 11.896 at 1500-1600, 2200-2300, 0500-0600, 0730-0830; uses Japanese only; is probably located in Communist China. (Japanese Short-Wave Club)

Legge, New York, notes Radio Free Europe afternoons (EST) on 11.855, 11.725, 9.717, 9.695, 9.607; fair signals around 0600 on 11.745, 11.675. (NNRC)

An Arabic-speaker reported some months ago by Cushen, N.Z., heard on 5.000, has been identified by Bert Bluman, Israel, as located at Kuwait in the Persian Gulf; operates 1130-1400 and identifies only at sign-on; programs are all-Arabic. (Radio Australia) (Al Kuwait is a sultanate in Arabia, south of Iraq. on the northwestern coast of the Persian Gulf; it is a British protectorate with a population estimated at 50,000.-K.R.B.)

Latest schedules for the COURIER, the Voice of America's "Truthship, are 1200-1615 to Near East and 1730-1900 to Caucasian USSR on 6.015; 1730-1900 on 7.200 to Caucasian USSR. VOA is now sending out QSL cards for reports on reception when the COURI-ER was testing from the Panama Canal Zone some months ago.

By this time, the 1953 edition of WORLD RADIO HANDBOOK, compiled in Copenhagen. Denmark, hy O. Lund Johansen, should be available from Ben E. Wilbur. 1000 Connecticut Ave., N.W., Washington, D.C. It is written in English.

"Australian DX-ers Calling" is now aired each Saturday 2300 on 15.200; each Sunday 0030 on 15,200, at 0300 on 9.580, 11.760. 17.840, and at 0902 on 9.580, 11.840, 15.320.

The Korean Broadcasting System operates a network of 15 stations, two of which are short-wave-HLKA on 2.510, 7.935, each 1 kw., and located in Pusan. A new short-wave station will open shortly in Seoul. using 10 kw. QRA is Hahn Ki Syan, Chief Engineer,

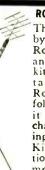
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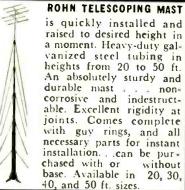
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nounces; 1100 gives news in French; 1115 dance music; a Soviet transmitter swamps the station around 1125. (Ridgeway)

Sao Tome—CR5SB, 17.677.5, noted Sundays 0750 when tuned with dance music; at 0757 had call, guitar music, details of next program and closing announcements in Portuguese; left air 0800A after "A Portuguesa." (Pearce, England; Ferguson, N.C.) CR5SC, 4.809, is good level opening 1430. light musical programs to closedown 1600; gives call frequently (by man). (Ridgeway, South Africa)

Saudi-Arabia — Djeddah is noted opening around 2215 on 6.177A and 7.245A with usual interval signal; uses Arabic; closes around 2304A. (Bellington, N.Y., others)

Somalia—Mogadishu, 7.383. is heard from 0915 in Arabic to 1200. when goes into Italian until 1300 closedown. (Ridgeway, South Africa)

South Korea—HLKA, 7.935A. Pusan noted 0630 with Western music and Korean news. (Sanderson, Australia) Wada, Japan. says is now operating on 7.935 and 9.555 at 1600-1800. 2130-0030, 0330-0900, all in Korean. Flynn, Calif., reports HLKA on 4.4785 at 0845, S6, in oriental language. much QRM.

Spain-Radio Mediterraneo, Valencia, is noted now near 6.995 from audibility around 1425. Radio Juventud le Murcia has been moving around, noted more recently on 7.105A with dance music 1655; gave call in Spanish 1700, and was soon buried by sign-on of a Radio Free Europe station. A Spanish Nationalist outlet has been heard on 7.420, but it is not Radio Menorca; signs on 1500 with singing of march and signs off with similar number 1705; call sounds like "Transmite Radio Cartagena." (Pearce, England) FET1, 7.006, noted 1630 with Spanish program of news. music. (Sanderson, Australia) Malaga. 7.012A. is still noted with Spanish Home Programs around 1515 onwards, fairly good level. (Ridgeway, South Africa)

Sweden — Radio Sweden, 11.705, noted with news 2300, then music. (Sanderson, Australia) Heard on 15.-155 with news around 1000, fair level. (Scheiner, N.J.) Noted on 9.535 at excellent strength 1900-2000. (Deem, W. Va.)

Switzerland — Damascus, 17.865, heard 0945-1045 to India-Pakistan. (Pearce, England) On 11.913A with news 1720-1730 closedown. (Black, Pa.)

Tahiti—Radio Tahiti, 6.135, Papeete, is heard around 0000; signs off 0130. (Kary, Pa.)

Taiwan — BEC26. 10.060A. noted from 0910 tune-in with Chinese session to 1000 closedown. (Pearce, England) Taipeh, 15.235, heard with news 2200 to North America. (Annala, Oregon) BEC32, 9.775A, Taipeh, noted 0700 with English commentary and Western music; asked for reports. (Sanderson, Australia) A Taiwan outlet is noted on 7.045A around 0500-1030 closedown; call seems BEC22, BEC32, or BEC34; is not parallel with 9.855

which is heard quite irregularly; another Taiwan station is noted on 7.340A to 1030 or 1100. (Wada, Japan)

Tangiers—Radio Africa is on a new channel of 7.192 as early as 1015. and as late as 1745. (Pearce, England; Kary, Pa.) Radio International, 6.110A, noted with news in Spanish 1700. (Pearce, England) Pan-American Radio, 7.300. is heard with clock chimes (12) at 1900 and multi-lingual announcements to 1904 sign-off. (Kary, Pa.)

Thailand — Bangkok, 11.910, has English session 0500-0630, fair level; announces also 15.630, 7.140 (is nearer 7.105—K.R.B.), 6.240. (N. Z. DX Times)

Uruguay—Radio Electrica, CXA10. has extremely good signal from around 1130 with classical music; call is given every half hour by man; has QRM from Radio Dakar at 1400. Radio Ariel, CXA3, 6.075. is noted at good strength from around 2030 to closing 2200. man gives call in Spanish. (Ridgeway, South Africa) Niblack, Ind., notes CXA10, 11.900, at good level 1800 and closing 2210.

USI (Indonesia)—A station believed Djakarta is heard with strong signal mornings to 1030 closedown on 9.865; at times location sounds like "Jogjakarta," however. (Stark, Texas; Kary, Pa., others) Noted on 9.585 from around 0800-1030 closedown. (Balbi, Rosenauer, Calif.)

USSR— Radio Tashkent, 6.825. is noted with English for India-Pakistan 1000-1030. 1115-1130 (some days English begins 1030, however). (Pearce. England) Moscow is noted on 11.68A with English (review of Moscow press and music 0500-0530 fade-out. (Jones. France) Frequencies used by Moscow for the 1820-0100 period to North America are 15.330, 15.250, 15.230. 15.110. 11.910. 11.830. 11.810, 11.710. 9.670. 9.650, 9.550, and 7.240 (some of these are actually relays by satellite countries); the 0800-0830 transmission to North America is over 17.830, 15.440, 15.360, 15.180, 15.120, 11.910. (Kary, Pa.)

Vatican—HVJ, 5.968. noted 1545 with chimes and then news in Italian. (Sanderson, Australia) Noted on 11.74 with news 1000, fair level; also heard on this channel with English 1315. (Scheiner, N.J.) Noted with English period 1315 also on 9.550. (Kary, Pa.) According to NNRC. HVJ has news Wednesdays. only 0930-0940 on 17.775 for Near East.

Venezuela—Radio Rumbos has English session Mon.- Fri. 1800-1900 over 4.970, presented by Jay Farr; first 45 minutes is disc jockey session called "Supper Club" and last 15 minutes (1845-1900) consists of a roundup of latest world and local news. (West, Va.) YVKB. 4.8903, noted S5 at 0612; YVMM, 4.9096, was S5 at 0615; YVKM, 5.0294, noted S5 at 0619, CWQRM. (Oskay, N.J.)

Yugoslavia—Belgrade, 6.100, noted signing on 2330; has English 0130 and then is heard parallel on 9.505. (Bellington, N. Y.) English is now sched-

tests) to Turkey at 1430-1515 and to the United Kingdom 1515-1600 closedown on 7.010, 9.484. (Pearce, England, others) Heard with news 0330-0340 near 17.715. Noted with strong signal in program for Indonesia 0630-0715 on 17.835; announced 15.270 in parallel. (Pearce, England) Heard on 15.335 at 1915 with program for home listeners. (Sanderson, Australia) Is noted daily on 6.285A around 0700-1000, all-native; identifies often. (Wada, Japan) Now uses 9.762 instead of 11.844 for news 1015; heard on 6.23 with native programs 1115-1200. (Ridgeway, South Africa)

Panama - HO50, 5.996, noted in Australia 0145 with Spanish program of music and news. (Sanderson) HOJA, 9.645, noted 2140 with commercials in

Spanish. (Pelegri, N.Y.)

Paraguay - Radio Encarnacion, ZPA5, 11.945, noted at good level from 1500 onwards. ZPA1, 6.278. Asuncion, is high level 2100 to close at 2200; features dance music 2100-2200. (Ridgeway, South Africa)

Peru-Radio Central, Lima, has moved from 9.522 (listed 9.545) to 9.550; weak level; uses call of OAX4K and Andalusian Spanish. (Stark, Tex.)

Philippines Radio Free Asia, 6.11 Manila, noted closing 0920 when announced channels of 11.94 and 6.11 for Manila. 9.49 for Guam. (Balbi, Calif.) DZH4, 6.000, Manila, noted in English 0900, CWQRM. (Flynn, Calif.)

The Far East Broadcasting Co., Manila, has brought into use a 16-m. channel of measured 17.805; is reported opening 0300; has been heard by Sanderson, Australia, also around 2300 when signal strength was especially good in Melbourne, also with news 0500; call is DZ16. The 16-m. outlet is heard by Ridgeway, South Africa, at good strength in parallel with 9.73, 11,-855, 15.300, and from 0900 on 6.030; heard from around 0800 to closedown 1200, English from 1000. DZI6 has been heard in Sweden by Engberg 0500-0600.

Poland-Warsaw lists English (presumably for Europe) as 0130-0200, 6.140, 7.155, 5.995; 1200-1230, 7.175, 9.555; 1230-1300, 6.115, 9.555, 7.145; 1400-1430, 6.115, 9.555, 7.145; 1430-1455, 6.140, 7.155, 5.975; 1730-1800, 6.140, 7.155, 5.975. (Pearce, England)

Portugal-Lisbon, 6.360, noted 1754-1800 when signed off with "A Portuguesa." (Machajewski, N.Y.)

Portuguese Guinea-CQM sent QSL card and mentioned only 5.838 at 1630-1800. (Pearce, England)

Portuguese India-Radio Goa, 9.61. heard in Hindi 0930, in Portuguese 1000; in English 1030 (Mondays has "Old Fashioned Revival Hour" transcription); has guitar interval signal; is in foreign language 1130 and closes 1230, good level in South Africa. (Ridgeway)

Reunion-Radio St. Denis, 7.168, has strong signal in South Africa opening 0915 with announcements in French; 0930 light music, French songs; calls "Ici Reunion, Radiodiffusion Francaise" by man; woman also an-

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lish daily 1000-1100A. (Pearce, England) Noted signing off 1631. (Kary, Pa.)

Liberia — ELBC, 6.022, Monrovia, noted 1830 to 1845 sign-off; announced would be back 1025. (Ferguson, N.C.)

Madagascar — Tananarive, 9.515, noted opening 2230 with "La Marseillaise." (Bellington, N.Y.; Kary, Pa.)

Malaya—Radio Malaya's Blue Network, 7.200, Singapore, noted signing off 1030 with "God Save the Queen;" on a Saturday was noted to 1100 closedown. (Pearce, England) Kuala Lumpur, 6.025, is heard well from 0900 with programs in English; has dance music 1000-1030 closedown. (Ridgeway, South Africa)

Manchuria—Mukden, 7.660, has been noted 0500-0855. (WRH)

noted 0500-0855. (WRH)

Martinique — Nattugglan, Sweden, says FNRI, Radio Martinique, Fort-de-France, has been heard on 9.680 at 1935-2000; not confirmed; may have been confused with Paris on 9.685 which runs to 2000 closedown.

Monaco—Radio Monte Carlo, 6.035, 9.785, bas English program, "Hour of Decision," Thursdays 1730-1800A signoff, and "Back to the Bible" 1730-1800A sign-off Fridays. (Bellington, N.Y., others)

Mozambique—The English commercial service of Lourenco Marques is now using 11.742 instead of 11.765 as formerly. The Portuguese service is now using 6.14 at 0400-0630, and also 1030. (Ridgeway, South Africa) Heard signing off 1515 on 15.285A with "A Portuguesa"; fair to good level in N.Y. (Bellington) CR7BE, 9.810A, noted 0030 in Portuguese session. (Patterson, Ga.) Is heard 0000-0100. (Rosenauer, Calif.)

New Zealand — Revised schedules have just been received via airmail from Radio New Zealand—to Australia 1300-1515. ZL.2, 9.540; 1530-0145, ZL10, 15.220; 0200-0545. ZL2. 9.540. To Pacific Islands 1300-1515, ZL9, 11.810; 1530.0145, ZL4, 15.280; 0200-0545, ZL3, 11.780.

Nigeria - Nigerian Broadcasting Service, 32 Marina, Lagos, Nigeria. verified reception of "7.083," stating frequency is actually 7.079; this is a 250-watt regional transmitter at Enugu in the Eastern Provinces; another regional station-low powered-is at Kaduna in the Northern Provinces on 4.925 during "hours of darkness" and 7.165 during "daylight hours" (local time). Officials said Lagos operates on 9.650, 7.5 kw., 0100-0215, 0530-0800, 1200-1500; channels of 6.100 and 7.255, low-powered, broadcast 0100-1700 with one break 0345-0530. Relays many BBC programs. Has been heard on 9.655A by Bellington, N.Y., and Kary, Pa., however, as late as 1700 closedown.

North Korea—Radio Pyongyang, the Korean Central Broadcasting Service, now broadcasts in Japanese on 4.400, 6.250 at 0800-0900. (Japanese Short-Wave Club)

Pakistan—Radio Pakistan is now on regular transmission (after completing

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Indo-China (Vietnam)-Radio France-Asie, 9.954AV, Saigon, noted ending English session with "Knightsbridge March" 1754. (Pearce, England) This one is at fair level some days around 0740. (Stark, Texas) Heard on 15.430 with English session 0500. (Sanderson, Australia) "Voice of Vietnam" is noted on 7.2882 and 9.620 with English 0930-1000 closedown; schedule is 1800-1930, 2215-0030, 0500-1000. Radio Hue. 7.205, is now scheduled 1830-1900, 2300-0015, 0500-0800. Radio Dalat, 7.265, broadcasts 0530-0630 (Sat. 0630-0700) in French. Radio Hanoi is now on 9.670 at 1800-1900, 2230-0015, 0500-0830. Radio Hirondelle (Swallow Radio), "Voice of the French Army in Indo-China," broadcasts on 7.408 from Hanoi at 2300-0130, 0530-1000, all-French. Radio Laos, 7.215, broadcasts news in French 0800-0815. Radio Cambodia relavs French from Saigon 1815-1845 on 6.090, has its own news in French 0700. (Wada, Japan)

Israel-Tel-Aviv, 9.009A, now has news 1515; has English session ("Voice of Zion," relayed from Jerusalem) now 1615-1700 closedown. Announces news for 0645 over 6.830, 9.000 (actually 9.009A); has "Voice of Zion" session in French 1530. (Pearce, England; Mar-

Italy-Rome, 9.630, noted opening 1245 and announcing for 9.63, 11.81; had news for Great Britain. (Ferguson, N.C.)

Jamaica — Radio Jamaica, 4.950, Kingston, noted opening 0600. (Ferguson, N.C.) And closing 2300 on 3.360. (West, Va.)

Japan-JKI4, 11.800, Tokyo, relaying Home Service, is strong level in New Zealand 0400; before 0345 has bad QRM. (N. Z. DX Times) JBD4, 15.235. noted 0400 with program in Japanese and Western music; is "N.H.K." outlet JK16. 11.825, noted 0400 with world and local news, then music. (Sanderson, Australia) JKL, 4.860, noted 0850 with popular music; JKI, 4.910, heard 0830 in Japanese, along with JKM, 4.940. (Flynn, Calif.) AFRS, 4.-860, is noted in English to 1000 signoff. (Gaylord, Wn. State) Radio Japan now uses JOA3, 9.675, and JOB, 6.069. to North America 0000-0100; the 0600-0700 beam to North China is radiated over JOA2, 7.180, and JOB, 6.069. Other transmissions are unchanged. (Kary, Pa.)

Kenya Colony-VQ7LO, 4.852, Nairobi, is now on this measured frequency, heard from 1200 to close 1500; the South African Broadcasting Corporation says Nairobi is also using 6.060 in parallel. (Ridgeway, South Africa) Forces Broadcasting Service, East Africa Command, 7.265. Nairobi, noted with music 2248; has BBC news relay 2300. (Ferguson, N.C.)

Lebanon-Beirut, 8.036A, has Eng-

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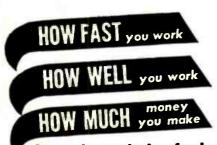
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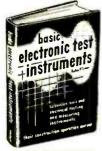
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too close to frequencies used by the government and marine services. However, the marine services have now arranged for the adoption of higher standards for auto-alarms* on shipboard, and the interference difficulty which prevailed earlier will no longer be a problem.

Canada has been using 540 kc. as a clear channel for many years, and XEWA, San Luis Potosi, in Mexico, is also operating on this band, with a power of over 100 kilowatts.

The first American station to use the new frequency may be KMBC, at Concordia, Missouri, who has been seeking that channel for years.

COMPATIBLE COLOR TV, as developed by the National Television Systems Committee, is expected to be ready for submission to the Commission next summer, according to Art Loughren, vice prexy of Hazeltine and chairman of the color video standards committee of NTSC.

The forecast was made during a meeting of the Society of Motion Picture-TV Engineers in Washington recently.

Before the FCC receives the petition to review the new color system, industry will be asked to review carefully, during a series of tests, all of the aspects of the system on the receiving as well as transmitting fronts. Then, one company will enter a plea for a hearing; NTSC will not be able to request the hearing since it represents most of industry and its views would probably be judged as biased, and thus not admissible before the Commission.

A FLEET OF 26 aircraft, operated by the Swiss Air Lines, will soon have complete visual omni-range very-high facilities for communications. system features the use of instrument-panel navigation and is said to be useful on any course up to 200 miles to or from an airport.

Auto-alarms serve to sound a call when a signal is received on 500 kc.

The airlines, operating out of Zurich, Switzerland, serve principal European points, the Near East, and provide transatlantic flights to New York City.

THE COUNTRY lost one of its foremost broadcasting legislators during the late fall, when Harold A. Lafount, member of the former Federal Radio Commission, died.

As a crusading Commissioner, he sought means to improve reception through the use of higher power for key outlets. Over twenty years ago he studied the possibilities of TV development.

The nation will miss the talents of this pioneer whose mature wisdom played so vital a role in creating the sturdy base on which modern broadcasting is built today. . . . L.W.

International Short-Wave (Continued from page 86)

To Central Europe, United Kingdom 0230-0330, 17.705, 15.160; 0345-0415, 17.-850. 15.160; 1000-1030, 11.780, 7.250. To East, Southeast Africa. Mauritius 2300-0010, 17.705, 15.130, 11.870; 1045-1215, 15.290, 11.780. To Burma 1945-1955, 9.720, 7.170; 0615-0700, 17.850, 15.160. To China 0430-0545 (to only 0530 Sat., Sun.), 17.850, 15.160; 0530-0600 (Sat., Sun. only), 17.850, 15.160. To Indonesia 1745-1800, 7.125, 5.960; 0700-0730, 17.-850, 15.160. To Fiji 0200-0320, 21.700, 15.190. To West Indies 1830-1930, 11.-850, 9.630, 7.170, 5.980. To Pakistan 2245-2320, 9.630, 7.125, 5.970; 0745-0815, 5.990, 3.945; 0815-0915, 7.170; 0945-1000, 3.945. To Afghanistan and adjacent areas 2215-2230, 7.125, 5.960; 0845-0930, 3.945. To Afghanistan 0030-0130 (Fri. *only*), 9.670, 7.170; 1130-1230, 7.170, 5.980, 4.940, 3.945. To Persia, Afghanistan 1230-1330, 7.170, 5.980, 4.-940, 3.945. To Saudi-Arabia, Egypt, Lebanon, Syria, North Africa, Jordan, Sudan 2330-0030, 11.760, 9.720; 1230-1430, 7.125, 5.960. To Europe, United Kingdom 1445-1545, 11.780, 9.565, 7.115.

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grams was discounted by spokesmen for the film exhibitors and producers. Only special presentations, prepared for theater audiences and particularly adapted to large-screen reproduction. would be offered, the film moguls de-

Complete briefs on behalf of others who will be involved in this new form of videocasting will be offered during the first weeks of the new year, and an extensive cross-examination period will follow. In view of the complexities of the issues involved in theater TV, many believe that there'll be no final decision from the Commission for quite awhile.

LOUDSPEAKER MANUFACTURERS have been cautioned by the NPA

against a quick return to the production of electromagnetic speakers, in view of the present uncertainties in

the copper supply situation.

The steel situation, disturbed by the recent strike, was also posed as a current difficulty by the government. Both issues were presented at a special meeting in Washington. In reply, an industry committee reported that speaker manufacturers are faced with a problem of seasonality and tie-in with radio and TV production. Declaring that loudspeaker steel allotments for the fourth quarter of '52 and advance allotments for the first quarter of '53 have been inadequate, manufacturers stressed that these quarters are the period of highest demand for their products. It was pointed out that speakers are the last component to be incorporated in chassis, and thus set makers do not order far in advance of their peak selling season. Therefore, it was noted, the speaker industry loses civilian business if it does not have a concentration of production material in the fourth and first quarters.

NPA officials stated their awareness of the situation and desire to alleviate the problem as soon as defense needs

for steel are met.

Among those who attended the conclave in the nation's capital were H. S. Morris (Altec Lansing), George Cromartie, Jr. (Best), Austin Ellmore (Crescent Industries), Russel S. Fenton (Permoflux), Matt Little (Quam-Nichols), Stuart W. Bell (Quincy), A. I. Abrahams (Racon) and Laurence A. King (Rola).

THE SIZZLING AM-BAND EXTEN-SION debate has finally come to an end. A few weeks ago the Commision issued a finalized rule approving the use of the 540-kilocycle band. The AM broadcast band now extends from 535 to 1605 kc, instead of from 550 to 1600. The extension of the band had been approved at the Atlantic City conference in '47, and on December 1 of this year the extension had been officially supplemented by a Geneva agreement.

For years, broadcasters have been trying to win approval of this band. but were told that this channel was FOR THE BEST COVERAGE

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Among the subjects included on the agenda were the technical requirements and standards for theater TV, involving the video signal (bandwidth, signal-to-noise ratio, linearity of electrical transducers and standards); audio signal; and the radio-frequency transmission of the video signal (r.f. bandwidth per channel, allocation principles for co-channel and adjacent channel operation, number of channels required per system, summary of standards, technical limitations on choice of frequencies, and possible location of theater TV service in spectrum). Also up for review were the possible systems of microwave distribution which might be used for intercity relay, intercity multiple address and intracity distribution. Methods which might be employed for projection were also up for analysis, kinescope projection, film storage, and Eidophor. Costs were also debated.

Quite a slice of the spectrum was asked for by the motion picture interests; a 360-mc. band in the 5925-6875 megacycle range, a hand now allocated for fixed common carrier services. To assure quality transmission of 35-mm film, film engineers said that the FCC should provide 10-mc. wide video channels, radio-frequency channels 30mc. wide, two-channels for a single system, and room for six systems for competitive reasons. It was also noted that an additional 60-mc. would be required for mobile pickup services. The Commission was told that if the channel initially requested could not be set aside, then there were two alternatives. Theater TV could be reclassified as an industrial service and be allowed to operate in the 6575-6875mc, band, with the band being widened to accommodate the necessary 360 megacycles, which would mean that the industrial service band would have to be extended down to 6425-mc. The second possibility lay in the allocation of the band at 10,700-11,700 megacycles, now also assigned to fixed carrier circuits. If this microwave band were used, then radio-frequency channels of 55 megacycles would be required, instead of 30-mc. stated in the original specifications.

Theater TV may require an entirely new set of standards, it was disclosed at the meeting. Recommended for such a new engineering setup were a scanning rate of 735 lines; a signal-tonoise ratio of 46 db for black and white, and 42 db for color; a frequency-modulated video signal, an 8kc. wide audio signal, multiplexed on the carrier, and a linearity not to exceed 10 per cent variation between the black and white levels.

The cost of building an intercity and intracity microwave net covering nine cities and about 1500 theaters between New York and Washington was estimated at between fifty- to sixty-million dollars, while operational expenses would run to about \$2-million.

The fear that theater TV would deprive home viewers of top-flight pro-



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Spot Radio News (Continued from page 18)

charged the normal calm of Commissionland. For his arrival is expected to cause some broad changes, particularly in the chairmanship of the group and the nomination of a new Commissioner to replace the recess appointee, Eugene Hyde Merrill, former director of the Materials Branch in the Defense Production Administration, who succeeded Robert Jones.

The naming of a new chairman may not be possible until June 30, when Walker's term expires. Actually, the present headman is serving on a special appointment from the President, having been asked to take the chair even though he had passed the retirement age; the late President Franklin Roosevelt had named Walker as a Commissioner in 1934. According to the established mode of procedure, the chairman is expected to be of the same political party as the President. Accordingly, two members of the Commission have appeared as possibilities for the appointment: Rosel Hyde, now serving as vice chairman, and George Sterling, both Republicans.

The appointment of Merrill was quite a surprise and was made public during an address by President Truman at Brigham Young University in Salt Lake City. Said the President: "This morning I signed a paper appointing to the FCC a distinguished resident of your state, Eugene H. Merrill. I thought you might be interested in that, because I understand that Mr. Merrill's father was a member of the board of this university. Of course, that was a good recommendation for him, as far I was concerned .

Merrill's tenure, technically, will expire when Congress convenes in '53; his name must then be submitted to the Senate committee for confirmation. It is believed that the name of another candidate for the post, a Republican, will prohably be sent to the Senate for such confirmation.

THEATER TV, shelved and reshelved on a dozen occasions, received a brief airing a short time ago during a special hearing in Washington which featured testimony by the Motion Picture Association of America and the National Exhibitors Theatre Television Committee.

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January, 1953



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Complete information on the calculator is available from Mr. Phil Jeffries, the general sales manager of the firm.

IMPEDANCE MATCHER

Rytel Electronics Mfg. Co., Inglewood, California, is now in production on a new unit which is engineered to balance the impedance between any antenna and the lead-in with which it is used.

Tradenamed "AIM", the new unit takes care of the impedance matching automatically. According to the company, the new unit will increase signal strength to the receiver on all channels (2 through 84), it will help eliminate snow and provide clear, sharp pictures in any reception area, it will give 3 to 7 additional db gain on all channels, and will prevent standing waves on the line.

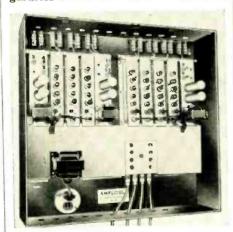
The junction box measures $2\frac{5}{6}$ " x $1\frac{3}{6}$ " x 1". It weighs 8 ounces complete with the U-clamp and approximately 47" of wire.

Full details on this new product are available from the company at 9820 Irwin Avenue in Inglewood.

AMPLIFIED SYSTEM

Amplitel, Inc., 360 W. 57th Street, New York 19, New York, is currently offering a new master amplifier TV antenna system which has been designed especially for large apartment buildings, hotels, hospitals, institutions, television dealers, etc.

The new unit is an amplifier system, designed to produce peak reception on each channel in an area—on every television set in the building regardless of location. According to the



company, there is no interference between sets and no cross-modulation between channels.

Complete technical specifications on this new antenna system are available upon request to the company.

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picture tubes, both magnetic and electrostatic deflection types. It will also analyze oscilloscope, radar, and other special purpose CR tubes without removal from the chassis or car-

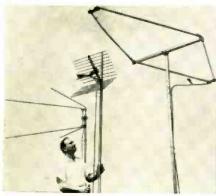
Four classes of tests are made with the analyzer. The beam current test is made to the final anode rather than to the grid or any other element. The beam current scale of the meter not only indicates sufficient or insufficient beam current, but also gives an accurate forecast of remaining tube life.

A grid test, a gas test, and interelement leakage test are also performed by the unit.

Full data on this new Model 707 is available from the company.

JFD ANTENNA LINE

JFD Manufacturing Company, Inc., 6101 16th Avenue, Brooklyn 4, New York, has developed a complete line of antennas for u.h.f. television reception.



Included in the new line are rhombics, single and stacked "V's", corner reflectors, and a combination "JeTenna-u.h.f." antenna.

This latter unit, the Jet 283, is designed for areas where both u.h.f. and v.h.f. stations will be in operation. It combines the features of the company's "fan-front" unit with a broadband triangular dipole u.h.f. antenna. A single lead-in wire delivers signals to the set through use of the company's unique coupling device.

Literature on the Jet 283 and other u.h.f. antennas produced by the company can be obtained by writing direct to Mr. Edward Finkel, sales manager of the firm.

TV COVERAGE CALCULATOR

Pioneer Electronic Supply Company, 2135 Prospect Avenue, Cleveland 15, Ohio, is now offering a new television signal-range calculator to the trade.

Designed as an easy-to-use slide rule, the new unit will quickly show the approximate grade "A", grade "B", and city coverage for all v.h.f. and u.h.f. television channels. Practical design permits coverage radius to be read directly on the scale, with one rule setting, for stations operating with effective radiated powers from 10 kw. to 1000 kw., and for antenna heights up to 3000 feet.

While useful to television transmitter engineers, the rule was designed especially as a handy TV service and

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Money Makers NEW TV PRODUCTS on the Market

SYLVANIA 1953 TV

Among the new receivers being introduced by Sylvania Electric Products Inc., is "The Lexington", a 21" deluxe combination, AM and FM radio,

and 3-speed phonograph.

Designated as the Model 178, the new console features "HaloLight" and the company's "Stratopower 508" chas-The cabinet is of hand-rubbed veneer with rosewood mahogany grained doors. The model is available with built-in all-channel u.h.f. recep-

Two wood finishes are offered, with the mahogany finish being designated as the Model 178M while the blonde finish is known as the Model 178B.

"PICBOOST"

C-B-C Electronics Co., Inc., P. O. Box 1556, Philadelphia 5, Pa., has introduced a new series of picture tube brighteners which have been trade-named the "Picboost Pacemaker".

The new unit is said to restore new tube brilliance, for periods up to several years, to any size or type picture tube. Other models in the series will permanently relieve heater-to-eathode shorts, thereby restoring brightness control, according to the company.

The "Pacemaker" can be installed within a few minutes, just by plugging in. No soldering is necessary and no 117 volt a.c. lines are used.

The four models currently available include the Models 1F and 2F, which



restore brightness to dim picture tubes in parallel and series circuits respectively, and the Models 3F and 4F to relieve heater-to-cathode shorts only, in parallel and series circuits respectively.

STANCOR TUBE BOOSTER

Standard Transformer Corporation, 3580 Elston Avenue. Chicago 18, Illinois, is in production on a CR tube booster, a compact, self-contained de-

vice designed to add months to the useful life of a television picture tube.

The tube booster, P-8192, can be used with all electromagnetic picture tubes irrespective of size, where dimming is due to low cathode emission.

Easy to install, the new booster measures only 3½" high and 1½" in diameter. It does not require a.c. line connection and is equipped with a "high-low" switch providing two levels of brilliance. Of autoformer construction, it has 18-inch leads between the booster and connector plug, allowing the booster to be placed anywhere in the set.

U.H.F. ANTENNAS

Technical Appliance Corporation of Sherburne, New York, has announced the availability of a complete u.h.f. antenna line.

Designed to meet the specific needs of various localities, the new line includes parabolic-reflector types, yagis, modified "X", and "V" type antennas. With the exception of the modified "X" design, all are of the sharp directivity type. The modified "X" will be marketed in areas where reception from channels in opposite directions is required. Tuning of all antennas is such that all operating u.h.f. channels will be within the antenna's band-

Catalogue 83 covering this new line of u.h.f. antennas is available on re-

"SUPER AUTOBOOSTER"

Production of a new four-stage "Super Autobooster" has been announced by Industrial Television, Inc., 369 Lexington Avenue, Clifton, New

The Model IT-102A utilizes the new 6BK7A dual-triode in a multiple resonant circuit which provides a uniform 18 db gain over both bands.

Designed for general booster applications requiring uniform high gain at moderate cost, the new unit has a low noise factor resulting in high usable gain even with the new "low noise" TV receivers.

The wideband booster has automatic "on-off", heavy-duty transformer-type power supply, and a metal cabinet. It is operated by a thermal "on-off"

CR TUBE ANALYZER

The Jackson Electrical Instrument Company. 18-46 S. Patterson Blvd., Dayton 2, Ohio, has introduced a new test unit, the Model 707 dynamic cathode-ray tube analyzer.

The new instrument is designed to completely and accurately test all TV

Vibration Pickup (Continued from page 49)

been completed, the unit may be tried by holding it against a safe or piece of machinery. Power should be on, and volume turned up.

Any noises within the equipment should be readily heard in the earphones (as the combination lock is manipulated, or as machinery is operated). The tone control is manipulated for easiest interpretation of the vibrational sounds heard. The ability to interpret the various sounds heard and to properly adjust the "Volume" and "Tone" controls will be gained with practice in using the instrument.

If the instrument seems to be weak, first check the batteries. Also check tubes and all connections for possible errors.

Check the operation of the amplifier alone by disconnecting the pickup cartridge and holding your finger on the input grid. Hum, clicks, and other noises should be heard in the earphones.

If the amplifier is operating properly, but the unit still seems to be weak, check the condition of the cartridge used. Also experiment with the exact location of the probe along the case of the crystal-sometimes the sensitivity may be doubled by taking care in locating the probe position with respect to the cartridge. There are no general rules for selecting the best location—this will vary with the type of cartridge used, and must be determined experimentally by trial and error.

When the unit is used to listen to vibrational sounds, it is often possible to select the particular sounds desired by experimenting with the way the probe is held against the machinery being checked. In some cases better results are obtained when the probe is held at right angles to the machinery housing; in other cases, holding the side of the probe against the housing will give better pickup. The pressure exerted in holding the probe will also affect the pickup. Again, experience and practice will best enable the user to develop the proper techniques.



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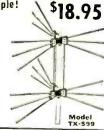
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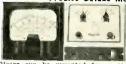
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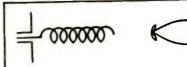


Fig. 14. Helical antenna radiation pattern.

end of the coiled helix and the outer conductor attaching to a reflecting screen. For reception the same type of response curve obtains.

Helical antennas can also be center fed with a balanced transmission line, and now the radiation pattern extends in more than one direction. As might be expected, the number of turns in the helix, the distance between turns (i.e., the pitch of the helix) and the circumference of each turn all will affect the response pattern of the antenna. In general, increasing the number of turns causes the beam width to become narrower; increasing the pitch or increasing the turn circumference will have the same effect, within limits.

The response pattern for a helical antenna shown in Fig. 14 holds true when the circumference of the helix turns are on the order of 1 wavelength at the operating frequency. If the helical antenna becomes small and compressed, the radiation pattern closely approaches that of a half-wave dipole. This latter application is not desired for TV reception.

The helical antenna has a broadband characteristic, enabling it to be used over a 2 to 1 frequency range. By the same token, the input impedance remains fairly constant over the same range.

It might be of interest to note in passing that when the helical antenna is used for transmitting, it radiates a circularly polarized wave. Now most technicians are familiar with vertically polarized waves and horizontally polarized waves. In the former the electric lines of force extend up and down and in the latter they extend in a horizontal direction, or from side to side. In a circularly polarized wave, electrical lines of force may be considered as existing vertically, horizontally, and at all angles in between. This can be readily demonstrated by taking a dipole antenna, holding it in front of a transmitting belical antenna, and then slowly rotating the dipole. The amount of signal picked up will remain constant as the dipole is rotated through a complete revolution of 360°

For reception, a helical antenna will receive any signal, no matter what its polarization. (There are several exceptions to this but they are not of interest in commercial television.) This is frequently advantageous because while television signals are radiated with horizontal polarization, this may change before the antenna is reached. A strictly horizontally or vertically polarized antenna might therefore not adequately receive all the available signal. A helical antenna, however, will.

(To be continued)

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U.H.F. Antennas

(Continued from page 38)

nected as shown in Fig. 8A to the end of a transmission line and power is fed to these stubs by the line, very little radiated signal is obtained. This is due to the fact that currents of opposite phase flow in the stubs (as indicated by the arrows) and their fields effectively cancel each other. Only in the small end sections (labeled Y) are currents in-phase and these radiate. However, the lengths of these end wires are small and very little effective radiated power is obtained.

It has been found, however, that if a half-wave slot is cut out of a metal sheet, as shown in Fig. 8B, that the non-cancelling currents in the Y ends of the slot circulate about the entire plate and now we have a fairly efficient radiator. With a horizontal slot we get a vertically polarized wave. Since television has standardized on horizontal polarization, a vertical slot would be required.

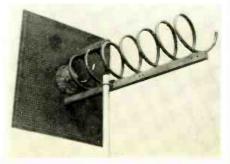
While the discussion has centered about the slot as a radiator, identical results will be obtained when it is employed as a receiving antenna.

The impedance across the center of the slot is on the order of 500 ohms. This gradually decreases to zero at either end. Hence to properly match a 300-ohm twin-lead line to the slot, it would have to be attached to the slot by connecting one wire to one edge of the slot and the other conductor to the other edge. One conductor may be bonded to the metal sheet, if desired.

The radiation pattern of the slot is similar to a dipole antenna. However, if the slot is cut out of the side of a cylinder, as in Fig. 8C. rather than out of a plate, the radiation pattern tends to become non-directional.

B. Helical Antennas. The helical antenna, Fig. 13, may be looked upon as a form of loop antenna. In fact, Kraus points out that it is related to the straight wire (or linear) antenna on the one hand and to the loop antenna on the other. If the helical antenna were employed for signal transmission, the energy fed in at one end would be "fired" out at the other end. This is shown by the radiation pattern in Fig. 14. The energy is brought to the antenna by a coaxial cable, with the center conductor connecting to the

Fig. 13. A helical television antenna.



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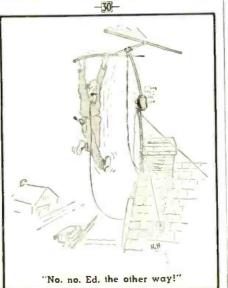


200 ma. power transformer, dual chokes, and two 8 #fd., 600 volt condensers, with a VR-150 (0D3) for the regulated 150 volts to the oscillator. A recommended supply is shown in the diagram, with pin connections shown as used by the author. A five-wire cable handles things nicely, and we simply soldered the wires directly to the socket on the rear chassis drop, using a Cinch plug for the power supply chassis end of the cable.

If any difficulty is encountered in resonating the final with your particular antenna set-up and loading condenser capacity used, short out approximately five turns of the pi-net tank coil. The final resonating condenser will then work nicely. To those not familiar with this type tuning net. a review of the pertinent chapter in current "Handbooks" is recommended. Briefly, the input condenser is the resonating one, by which the plate current of the 1625's is dipped, and the output condenser is the loading one, by which the current drawn from the 1625's is placed at a desired value. It is a simple, efficient means of power transfer, and has the happy faculty of giving a wide range of impedance matching.

It has been found in practice that almost any setting of the final pi-net will deliver an almost constant power to the antenna, with a wide frequency range covered on the oscillator tuning condenser, giving virtually one dial control, but allowing any loading desired on the final-a desirable condition.

The rig packs quite a wallop, the rule-of-thumb light bulb test showing a full 40 watts going into the antenna, which can make quite a noise. We feel the equivalent rig, if built from scratch by the bam, would entail a considerably larger monetary outlay, and much more work. So all in all the SCR-274, in its modern garb, has proven to be, for us, the answer to a long-felt problem. For a small auxiliary rig it is ideal, and for the beginner or confirmed low-power c.w. man we feel it is pretty hard to beat.



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course, the possibility of two signal sources maintaining a precise phase relationship for more than a few seconds is remote. Therefore the figure will apparently rotate, changing from a circle to an ellipse, to a straight line, and back again. It is the straight line that provides the desired criterion: any harmonic distortion greater than 1% will appear as a bump or loop in the straight-line pattern.

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BIBLIOGRAPHY

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-30-

Modernizing the SCR-274/N

(Continued from page 59)

for the final. The use of a stand-off insulator-type r.f. choke makes this easy, using the existing hole between the 1625's for the mount, and the existing plate "B-plus" feedthrough mica insulator for power connections.

Connect the parallel-feed as shown in the top chassis photo and the diagram, forming a conventional pi-type network system, after soldering the top of the coil to the top-chassis lefthand condenser, and the bottom of the coil to the top-chassis right-hand condenser. (Positions as viewed from front of panel.) Use bits of the former tank coil wire for all this, since that silver is hard to beat for r.f.

The hole in the lower right-hand side of the front panel, due to the removal of the dial assembly, etc., is an ideal spot for the midget closed circuit jack J, to which is wired a lead from the final amplifier cathodes, for keying the rig.

A % in punched hole, to the right of the meter, provides for a coaxial fitting, to carry the pi-tank output to the antenna, which can be almost anything, from a short whip to a fancy array. (With some type of antennas, it may be necessary to solder a .0001 μfd., 2500 volt mica condenser in parallel with the loading condenser, RH pi-net condenser, to get proper and adequate loading.) In our case, we can load to a hundred-and-fifty mils, with approximately 450 volts on the final, which was considered good enough.

The former neutralizing condenser, shown on the chassis lip in the under chassis photo, was not used in our case: it can be left disconnected.

Power for the rig is from a typical junk-box job, using a husky 500 volt,



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The action of the lamp in automatically adjusting its magnitude or resistance to maintain the amplitude of oscillations at a constant level may be seen by the characteristic curve of such a lamp, shown in Fig. 2. In this curve resistance is plotted as a function of impressed voltage, and clearly shows the nonlinear nature of this function. The dashed vertical line indicates the approximate limit of voltage that may be applied to obtain regulator action. Don't expect any light from the lamp-even the faintest red glow of the filament indicates improper adjustment. The characteristic that permits the use of a lamp for regulation is that the voltage developed across it increases more rapidly than the current sent through it. It is the slope of the curve, that is, the incremental resistance, at any point rather than the resistance value at that point that governs the action (Fig. 4). An amplifier with such an element as the negative feedback resistance becomes a very nonlinear device. No matter what magnitude of signal is applied, the output is nearly constant. The range of input is, however, limited by the range of the nonlinear element.

Calibration of the dial involves a known frequency (from a standard oscillator, or the 60 cps power line) and a CRO. With the oscillator feeding the vertical amplifier and the reference signal feeding the horizontal amplifier, Lissajous figures will be produced. Any stationary pattern indicates an integral relationship between the two frequencies. The ratio may be calculated by counting the number of tangent points to a rectangle enclosing the figure. Let the number of tangent points along the top be H; similarly, the number of tangent points along one side is V. Then H/Vis the frequency ratio, and H/V multiplied by the reference frequency gives the frequency of the oscillator. In this manner 10 cps division marks can be made on the lowest band using the 60 cps power line for reference. If the condenser decading is within 1%, no further calibration is necessary up to 200 kc.

A method of checking distortion content of any waveform was mentioned. This requires a CRO and an oscillator with very low distortion. A Lissajous figure of unity ratio is formed. Of



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Audio Oscillator

(Continued from page 64)

power supply shown be adopted as all parts are standard and the over-all cost is low.

The theory of tuned RC nets has too many ramifications to be discussed here; those interested are referred to the bibliography at the end of this article. However, a brief description of oscillatory action in this circuit will be given. As stated before, the circuit is essentially a two-stage RCcoupled amplifier, with the output of the second stage brought back to the input of the first. There are three necessary components for oscillation: a gain-producing element, a phasecontrolling element, and a frequencyselective element. The two-stage amplifier represents the gain-producing element. However, the output is fed back negatively through the lamp in the cathode circuit of the first stage, which limits the gain of the amplifier to slightly more than three times. Simultaneously, positive feedback is coupled through the RC net to the grid. This net is frequency selective due to its transfer-phase shift characteristic. At some frequency, depending upon the values of R and C, the voltage at the grid will be in-phase with the voltage impressed across the entire net and equal to 1/3 of the impressed voltage. At any other frequency, for the same RC values, the grid voltage will either lead or lag the impressed voltage by some angle. Thus for only one frequency will the second stage output and the first stage input be in phase. At this frequency the grid and cathode voltage are in phase, and the negative feedback voltage developed across the lamp must be just slightly less than the voltage developed between grid and ground, i.e., a slight net positive signal, for oscillation to occur at this frequency. At all other frequencies the negative feedback voltage is greater than the positive feedback voltage; hence oscillation will occur at one and only one frequency.

Although single-frequency oscillation is assured with sufficient positive feedback, good waveform is not. It is with the greatest of ease that this circuit can and will produce almost any desired waveform. Continuous sine waves are only one of a great variety, and are the result of critical damping, to borrow a mathematical term. Over-damping produces a damped wave train, usually sinusoidal in form; under-damping is multivibrator action. For continuous sine waves, the negative feedback must be adjusted so that an over-all gain of unity results. This is the condition where the energy fed back positively just cancels the circuit losses. While it is relatively easy to make this adjustment for one frequency, to do so for a wide range of frequencies requires another variable element.

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154 155 174 104 117 117 117 117	.65	6BJ6 6BQ6 6C4	-55	12AT7 12AU6 12AU7 12BA6 12C8 12H6	1.10
1T4	65	600		12406	.75
104	.67	6C8G	86	12806	.88
1V	.65	606	.72	1208	.69
1X2	.96	6D8	.85	1286	60
2A3	1.10	6E5	.79	12K8	.72
2X2 2X2A 3A4 3A5 3B7 1291 3D6/1299	.50	GES GES GES GES GHGCT GJS GJS GJS GJS GJS GJS GJS GJS GJS GJS	.85	125A7GT .	.79
304	6.5	CHC	.85	125C7	.85
3A5	85	SHECT	-65	12567	-85
3B7 1291	.42	615	.75	125 K7CT	.65
3D6/1299.	.43	6JSGT	.55	125L7GT	. 50
3Q5GT 3S4 3V4	.63	616	.95	125N7GT	85
3QSGT	.79	6.17	.95	125Q7GT	.72
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pickup differential of approximately 15 db, which makes the microphone, for all practical purposes, dead to extraneous noise and drone, according to the company.

The internal dynamic element is floated in rubber to help insure stability. An impedance selector switch provides operating impedance of 50, 200, 500, and high impedance. The switch is located at the back of the microphone housing, flush with the surrounding grillework to prevent accidental turning. It has a center slot for easy turning with coin edge or screwdriver.

Output level is -54 db (1 volt-permicrobar) and the range is 40 to 10.000 cps. Standard equipment includes an *Amphenol* cable connector and 18 feet of two-conductor shielded cable.

PROGRAM EQUALIZER

Production on a new program equalizer, the Type 4031-B, has started at the Burbank, California plant of Cinema Engineering Co.

The new instrument has wide applications in sound and electronic laboratories for research and control; broadcasting, recording, and motion picture



uses include providing corrections for frequency response in audio equipment, sound pickup, and transmission lines.

Easy operation of two control knobs allows wide range of over 395 available curve combinations. Controls provide for independent adjustment of the high and low frequencies in 2 db steps. Input level minimum is -70 dbm and maximum +20 dbm.

The equalizer uses standard RTMA rack mounting and is available either from the company's New York representative, Audio & Video Products, 730 Fifth Avenue, or from the manufacturer direct.

RCA SHOWS EXPERIMENTAL TRANSISTOR GEAR

DCA recently demonstrated a series of electronic gear in which a wide range of transistor applications useful to radio, television, and the industry were incorporated.

Each development was in the form of a laboratory model which, it was emphasized, is still in the preliminary and experimental stage. None of the units is commercially available at the present

Among the equipment demonstrated at the David Sarnoff Research Center of RCA in Princeton, N. J., was a portable public address system, a personal radio which was transistorized except for one tube, an all-transistor personal radio, a portable FM receiver, a transistor portable phonograph, a wireless phono jack, a roving microphone, a toy piano, a transistor ukelele, and a portable television receiver.

Ten types of RCA developmental and experimental transistors, three of the point-contact variety and seven of the junction transistor family, were used in the equipment. The three point-contact types and one of the junction types are to be offered on a limited sampling basis for engineering advanced development to industry representatives. The other six junction-type transistors are still classed as experimental.

Among the experimental items which attracted considerable attention was a portable, battery-operated television receiver, tribeless except for the picture tube. In another approach transistors were introduced in part of the circuits of a standard television receiver. Transistors were also employed in circuits of industrial TV equipment and the "Walkie-Lookie" portable TV gamera equipment to point up savings in weight, size, etc.

In summarizing the demonstration, Dr. E. W. Engstrom, vice-president in charge of RCA Laboratories Division,

"These demonstrations highlight the fact that transistors are today no longer entirely a research concern. They are, in the fields of radio and television, an immediate problem for advanced development by industry engineers who can learn how to put them to work in evolving more versatile, smaller, sturdier, and eventually lower cost equipment for industry and the public,"

D. D. Holmes, staff member of the David Sarnoff Research Center of RCA at Princeton, N. J., demonstrates the simple replacement of a junction-type transistor in an autoreceiver operating solely from 11 developmental and experimental transistors instead of the customary electron tubes. The use of transistors makes it possible to eliminate the usual high-voltage power supply. The transistors operate directly from the car's 6-volt storage battery so that the receiver has only 10 per-cent of the usual drain on the automobile battery.



RADIO & TELEVISION NEWS

Three tips, 1/8", 1/4", and 1/16" diameter, are available for use with this unit.

A brochure describing the Model XK-72 and other units in the company's line is available without charge upon request.

H.V. TEST JACK

Alden Products Company, 117 North Main Street, Brockton, Massachusetts has introduced a new, skirted test point jack, the 110BCSH, which permits safe circuit voltage readings up to 3000 volts a.c. peak from the front of equipment panels.

Its high collar protects the operator from flashover during high voltage checks. Actual flashover breakdownto-chassis occurs at 7-8000 volts a.c. (r.m.s.).

This new miniature test point jack has a heryllium copper contact, made to critical accuracy in progressive dies to insure resilient, long-life contact action. Its pre-tinned soldering tab is suitable for use with up to 14 gauge wire.

For complete information on this new product, address requests for additional data to Mr. Nelson Hearn at the company's address.

AUTOFORMER

Halldorson Transformer Company, 4500 Ravenswood Avenue, Chicago 40, Illinois, has announced the availability of a new "Varivolt Autoformer" which permits the adjustment of line voltages of 65, 75, 90, 100, 115, 130 and 145 volts to 115 volts, or to other voltage levels within the unit's range.

Voltage is set by means of a seven-



step rotary switch and indicated by a voltmeter having a red-line marker at 115 on its 0-150 volt scale. Each unit is equipped with a conventional sixfoot plug-in line cord and a standard output receptacle.

The line is currently available in four wattages (resistive load rating): 150, 350, 500, and 750.

UNIDIRECTIONAL MIKE

The Astatic Corporation, Conneaut, Ohio, has announced the addition of a unidirectional dynamic model to its line of microphones.

Known as the "Dynabar" Model DR-11, the new microphone employs the company's exclusive sintered metal method of acoustic phase shifting. This accomplishes a front-to-back

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bly permits the selection of any one of 10 crystal frequencies from the front panel, with an 11th position provided for use with an external v.f.o.

All stages are metered and dual power supplies are designed for econ-



omy and operating convenience. For novice operation, the final amplifier input may be reduced to 75 watts without transmitter modification.

The transmitter, TVI suppressed, is enclosed in a heavily copper-plated steel cabinet. The lid is bonded with silver-plated, phosphor bronze contact fingers. Special shields are included for the meter, dial window, and v.f.o. power socket

A free bulletin, No. 714, giving complete specifications on the new transmitter kit, is available on request.

COMPACT CONVERTER

The Terado Company, 1068 Raymond Ave., Saint Paul 8, Minnesota has introduced a compact d.c. to a.c. converter, the "Trav-Electric Super," Model No. 6-71160.

This unit converts 6 volts d.c. (car battery) to 110 volts, 60 cycle a.c. Capacity is 60 watts continuous and 75 watts intermittent. Suggested uses for the new unit include the operation of wire recorders, dictating machines, portable phonographs, radio receivers, small electric drills, hand vacuum cleaners, electric shavers, lights, and test equipment.

A catalogue sheet describing this and other converters in the company's line is available on request.

SOLDERING MACHINE

Sunrise Products Company, P. O. Box 173, Hawthorne, New Jersey, is currently featuring a new soldering unit, the Model XK-72.

This compactly-designed resistance soldering unit incorporates a sensitive interval timer (1/5 to 90 seconds) and an adjustable heat controller to per-



mit fast, precision soldering without overheating or warping of the parts to be soldered.

The electrode holder, L-14, measures 6" long and weighs just 31/2 ounces.



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enough to accommodate the piece to be stripped.

Attack on the coating begins immediately and parts are normally stripped clean in 1/2 to 4 hours. Overnight immersion will remove heavy coats up to 3" in thickness.

Further information and a free sample are available from the company.

TAPE RECORDER

Allied Radio Corporation, 833 W. Jackson Boulevard, Chicago 7, Illinois is currently offering a low-priced tape recorder which incorporates many new features for a variety of applications.
The "Knight" 96-485 has "automatic

keyboard" control. Five piano-key type push-buttons permit the quick and easy selection of the operating functions including "fast forward," "playback," "stop," "record," and "fast reverse." The "fast forward" speed enables the user to locate that portion of the recorded tape desired for play-

Two speeds and a dual-track recording head provide four recording times. At the speed of 3.75" per second, a 7" (1200 foot) reel records continuously for one hour, or two hours by recording on the second half of the tape width. At the 7.5" speed, the recording times are one-half hour continuously and one hour over-all. Frequency response is flat from 70 to 8500 cps at 7.5" and 90 to 6000 cps at 3.75".

The unit is housed in a sturdy, twotone green, luggage-type case which measures 14" x 12" x 7". It weighs less than 22 pounds. Ready for operation



from any 105-120 volt, 60-cycle a.c. outlet, the unit comes complete with crystal microphone. 8 feet of mike cable, a 600-foot reel of type "A" tape, a 5" take-up reel, and all tubes.

HAM XMTR. KIT

E. F. Johnson Company of Waseca, Minnesota, is now in production on a new ham transmitter kit known as the "Viking II".

Rated at 130 watts c.w. output, 100 watts phone, the new transmitter has been designed for operation on every amateur band from 10 to 160 meters, including the recently-assigned 15meter band. The pi-network amplifier matches a wide variety of antenna impedances. A crystal selector assem-

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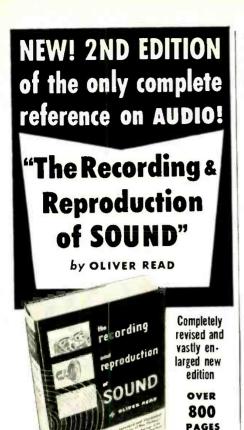
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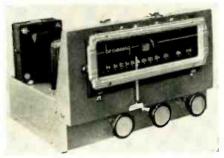
er. The cabinet measures 23 % wide, 30" high, and 1438" deep. It is available in either blonde or mahogany finishes. All the necessary mounting hardware is included, along with a mounting board for 12" speakers.

A data sheet on these new bass reflex cabinets is available from the company on request.

FM TUNER

Browning Laboratories, Inc., of Winchester, Mass., has recently introduced a new FM tuner which has been designated as the Model RV-31.

The new tuner features an all-triode r.f. section and follows the Armstrong receiving method with dual cascade limiters for most effective noise quieting. Input signals of 3 microvolts will



produce 20 db of quieting. An a.f.c. circuit locks the local oscillator into correct tuning but may be switched off if desired. A selector switch permits FM, phono. TV, or recorder playback to be fed through the tuner volume control to the main amplifier.

The RV-31 is suitable for custom installations where space is limited since it measures 11" wide, 9%" deep, and 61/2" high. Knobs and dial escutcheon are furnished in black and silver to complement the black dial background.

EXTENSION SPEAKER

Auto radio sales and service technicians will be interested in a recent announcement from Lowell Manufacturing Company, 3030 Laclede Station Road, St. Louis, Missouri that it is now in production on an easily-installed rear-seat auto extension speaker baffle

This "extra profit" item comes complete. It includes a 9" x 7" stamped metal louvre plate with tamperproof screening, a three-way switch, screws for mounting dial plate to car dashboard, complete mounting hardware, and detailed instructions.

The company will supply additional details on request.

VARNISH REMOVER

A non-inflammable, impregnating varnish remover that rapidly strips all types of impregnating varnish from baskets, jigs, etc. has been announced by London Chemical Company, 325 W. 32nd Street. Chicago 16. Illinois.

The new "Lonco" remover is designed for fast stripping, at room temperature, of all types of varnishes used in the electrical field. The only equipment necessary is a covered tank large

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	Int	ut	Out	put	Radio
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PE86	28	1.25	250	.060	RC 36
DM416	14	6.2	330	.170	RU 19
DM33A	28	7	540	.250	BC 456
PE101C	13/26	12.6	400	.135	SCR 515
1 21010	17/20	6.3	800	.020	
BD AR 93	28	3.25	375	.150	
23350	27	1.75	285	.075	APN-1
ZA0515	12/24	4/2	500	.050	ALM-T
		9.4	275	.110	MARK 11
B-19 pack	12	9.4	500	.050	WARK II
D 101	10				
D-104	12		225	.100	
	00	3.0	440	.200	CCD FOO
DA-3A	28	10	300	.060	SCR 522
			150	.010	
			14.5		
5053	28	1.4	250	.060	APN-1
PE73CM	28	19	1000	.350	BC 375
CW21AAX		12.6	400	.135	
	26	6.3	800	.020	
			9	1.12	
PE94	28	10	300	.200	SCR 522
			150	.101	
			14.5	.5	
17					

RECTIFIER TRANSFORMERS

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Stock	Description	Price
CH-366	20H/.3AS	6.95
CH-322	.35H/350 MA-10 Ohms DCR	2.75
CH. 141	Dual 7H/T5 MA. 11H/60 MA 5KV DC Test	4.69
CH-119	8.5H/125 MA	2.79
CH-69-1	Dual; 120H/17 MA	2.35
CH-8-28	2 x .5H/380 MA/25 Ohms	1.79
CH-776	1.28H/130 MA/75 ohms	2.25
CH-344	1.5H/145 MA/1200V Test 10HY/15 MA-850 ohms DCR	2.35
CH-43A CH-917	10H. 450 MA. 10KV TEST	12.95
CH - 366		69.55
CH-999	15HY 15 MA-400 ohms DCR	1.95
CH-511	6H 80 MA-310 ohms DCR	2.45
CH3-501	2x5H 400 MA	2.79 1.79
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CH-932	SWING 9-60H .105A. 10KV	7.95
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Write Dept. RN-1 for literature and complete specifications on Model 511-C and others.



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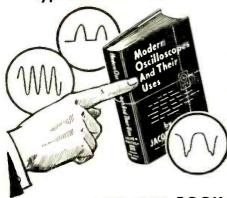
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WHAT'S MOW in Radio

For additional information on any of the items described herein, readers are asked to write direct to the manufacturer. By mentioning RADIO & TELEVISION NEWS, the page and the issue number, delay will be avoided.

RC OSCILLATORS

Hewlett-Packard Company, 395 Page Mill Road, Palo Alto, California, is currently introducing two new widerange RC oscillators which are small in size and simple to operate.

The new instruments, Models 200AB



and 200CD, have high stability and quickly resettable tuning circuits. Operation is simplified and only three front panel controls are used. They are small in size, lightweight, and are mounted in an aluminum case with carrying strap for maximum portability.

The Model 200AB, for general audio tests, offers a frequency range of 20 cps to 40 kc. and a full watt output. The Model 200CD, for wide-range measurements at lower power levels, provides constant voltage output from 5 cps to 600 kc.

The company will supply additional details on request.

OIL-FILLED TUBULARS

A complete line of easy-mounting, single-stud tubular oil-filled condensers is now being offered by the *Industrial Condenser Corp.*, 3243 N. California Ave., Chicago 18, Illinois.

The new units are oil-impregnated and filled with Indco Oil "A." Pyroteen filled units are also available. Standard capacity tolerance is $\pm 20\%$ $\pm 10\%$. The temperature range with the Indco Oil is ± 40 degrees to ± 70 degrees C. and with Pyroteen ± 70 degrees to ± 90 degrees C. Power factor is $\pm 4\%$ with the Indco Oil and $\pm 2\%$ with Pyroteen.

A four-page illustrated catalogue, containing complete data on the new G and H types, is now available from the company.

PUSH-BUTTON SWITCH

Grayhill. 4524 West Madison Street, Chicago 24. Illinois, has developed a new push-button switch which meas-

ures only 1.047 inches from the end of the plunger to the end of the terminal tips. It is ½" in diameter at the widest point.

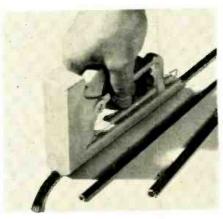
Designated as the Catalogue No. 23-1, the new switch is normally open and has a s.p.s.t. momentary contact arrangement. It is rated at ¼ amp., 117 volts, noninductive. The bushing, providing single hole panel mounting, has a ½16-32 thread.

Complete information on this new push-button switch is available from the company. Address letters to Mr. B. Doran.

FASTENING GUN

Of interest to service technicians is the newly-developed, hand-held automatic fastening gun which has been introduced by *The Heller Stapler Company*, 2153-E Superior Avenue, Cleveland 14, Ohio.

This compact unit is operated by just one hand, leaving the other hand free to guide the cable or hollow tube lines being installed. The force of the machine will drive bands around cables and tubes into hard or soft woods, plaster walls, flooring, joists,



and even mortar joints and cinder or mineralite building blocks.

An extra-size band, with leg lengths varying from $\frac{1}{16}$ " to $\frac{1}{2}$ ", is used with the new fastening gun.

BASS REFLEX CABINET

Argos Products Co., 310 Main Street, Genoa, Illinois, is now offering a new bass reflex cabinet to the trade.

Featuring a solid mahogany front and matching leatherette top and sides, the new cabinet has a single grille cloth covering the entire front panel, thus concealing the two separate sound openings and giving a more modern appearance.

more modern appearance.

Known as the "Deluxe Model DBR-15," the new cabinet is designed to accommodate either a 12" or 15" speak-

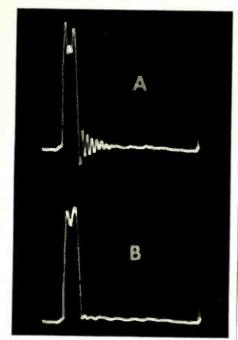


Fig. 15. Horizontal pulse as seen with high-voltage probe at high side of yoke connection. (A) Additional damped wave due to open condenser across half of yoke. (B) Normal waveform with new condenser.

Fig. 14 depicts the waveform associated with a common cause of trouble in the yoke circuits, a shorted neutralizing condenser, and subsequent burnt series resistor across half of the horizontal windings of the yoke. Three principal signs of distortion are evident. 1. The pulse, severely reduced in amplitude, indicates excessive loading of the horizontal deflecting system. 2. The bent baseline is associated with reduced damper-tube conduction, which is concurrent with insufficient pulse power, 3. The rapid decay in pulse shape agrees with other examples of excessive loading across part of the horizontal yoke winding.

If the yoke-neutralizing condenser is open-circuited instead of shorted, it causes no noticeable change in the waveform at the plate of the horizontal-output tube. Open yoke condensers, however, are known to cause "ringing," which is a condition easily recognized by the presence of a series of vertical bars at the left half of the raster. Fig. 15A shows a waveform distinctly associated with this condition. This waveform exhibits the ringing as a damped wavetrain immediately following the pulse. Connection for this test was made by probe contact at the yoke terminal connected to the high side of the horizontal winding.

Although waveforms may differ somewhat with various makes of TV receivers and detailed symptoms may not agree because of circuit or component design differences, high-voltage signal tracing can be universally applied to horizontal-deflection, pulsetype, high-voltage power supplies.

The author wishes to extend a note of appreciation to Mr. B. V. Venderschmitt for his helpful suggestions.



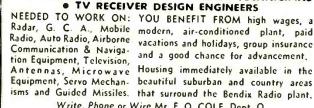
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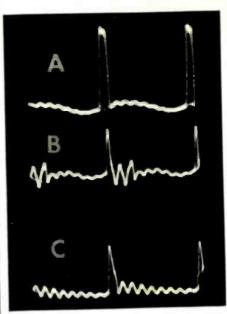


Fig. 13. Waveform at plate of horizontal output tube. Short between horizontal and vertical yoke windings. (A) Low side "H" to "Center V." (B) High side "V" to "Center H" and (C) Low side "V" to "Center H."

by controls the return trace or flyback time. The repetition rate of the pulse is determined by the 15,750 cycle horizontal-oscillator frequency.

Weaknesses in pulse forming circuits, such as open yoke windings, cause the pulse to become broad at the base and round at the top, as shown in Fig. 9B. Pulses having little change in base width but showing deformed peaks indicate trouble in the resonant pulse-forming circuit. Because the tuning of this circuit depends on the proper operation of a number of components, a change in any one of them, or a change in their distributed capacitance, can be responsible for pulse-peak distortion.

Defects in the yoke, the output transformer, the width control, the high-voltage condenser, the horizontaloutput tube, the damper tube, or the high-voltage rectifier tube, or even in the associated leads, can individually be the cause of detuning the pulseforming circuit. With such defects, the pulse shape suffers as shown in Figs. 9A, 11, 13B, 13C, and 14.

Short circuits between horizontal and vertical yoke windings produce different reactions depending upon the sections involved. Fig. 13A shows little change in pulse shape due to a short at the low end of the horizontal winding. When half of the horizontal yoke is involved, however, rapid pulse decay occurs as pictured in Figs. 9A, 13B, 13C, and 14.

Fig. 14. Waveform at plate of horizontal output tube. Condenser shorted and series resistor across half of horizontal yoke winding subsequently was burned.



tube cathode, shows zero voltage at the base or lower line, the "B+" voltage above it, and boosted "B+" voltage and pulse waveshape at the top. The "B+" voltage alone remains when anything happens to eliminate the high-voltage pulse.

Typical Waveforms

As previously mentioned, deviation from the normal waveform at the plate of the horizontal output tube indicates failure of components in the high-voltage section of a TV receiver. The series of examples that follows is typical of modern high-voltage circuits. An RCA 17T153 television receiver chassis was employed during waveform photography. In receivers with different circuits, some modification of waveforms can be expected.

Although the normal waveform in Fig. 7A is not entirely clear of crosstalk, it is typical of waveforms found to be satisfactory as a reference for signal tracing. Subsequent illustrations each show singular changes from this normal state. The testing arrangement employed to obtain the normal signal indication of Fig. 7A was retained for all other pictures in the group.

Baseline Distortion

Figs. 7B and 7C illustrate the bent baseline caused by reduced dampertube emission. In the previous exhibit of this condition in Fig. 6, the general bend in base line is lost because of trace expansion. It can be seen, therefore, that it is advantageous to examine at least a complete cycle of the waveform, digressing only temporarily to observe detail by trace expansion.

Fig. 8 indicates loss of pulse amplitude due to damper tube heater-tocathode leakage. Usually such leakage is quickly checked by tube replacement but may even be traced to paths external to the tube.

Short-circuited or leaky components place undue loading on the entire deflection circuit and result in loss of pulse amplitude and base-line warping. Various degrees of such conditions are illustrated in Figs. 7B, 7C, 8, 10, 12, 13A, and 14.

Distortion of Pulse Shape

Analysis of the cause of a distorted waveform should also include inspection of the pulse shape. The shape of the pulse is closely related to the proper performance of the deflection output components, such as the horizontal output transformer, the yoke, or the damper tube. The pulse-forming circuit which includes these components has a resonant frequency of approximately 65 kilocycles and there-

Fig. 12. Waveform at plate of horizontal output tube. This pattern is obtained when there is a shorted condenser be-tween "B+" and boosted "B+" circuit.







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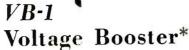
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TV Signal Tracing

(Continued from page 51)

of the horizontal-output tube, its effect can be reduced to an insignificant level by both direct contact of the probe tip to the tube cap and manipulation of the probe body for minimum capacitance pickup. Actually, direct contact lowers the probe input impedance, making it less sensitive to the crosstalk field.

The small short ripple, which follows the pulse in Fig. 2B but is not apparent in Fig. 2A, is a characteristic found at the deflection voltage level. It is referred to by design engineers as the "Spook". (The spook may be noticed on television screens as a fine vertical line very close to the left edge of the raster.)

Hum

Hum also presents a continuous but not too serious problem in high-voltage signal tracing in that it spreads the horizontal lines of a high-voltage waveform vertically, as shown in Fig. Very little hum interference comes through the probe-tip contact because a rather high ratio of high voltage to hum voltage exists at that point. Hum introduced near the handle of the probe, however, mixes with the highvoltage signal after the signal level is reduced by the probe resistor. Fig. 3 shows amplitude expansion of horizontal lines due to hum voltage originating in the field of a Variac placed near the probe handle. If the source of hum cannot be removed, movement of the probe to a different angle of approach will usually reduce the hum effect to an insignificant level. As a matter of note, strong video signals or vertical-deflection signals, or either of these mixed with hum, will cause distortion similar to hum alone.

Effect of Reduced Voltages

Low supply voltage (low line voltage, low "B+" voltage, or low boosted "B+" voltage) is another possible cause of waveform distortion, particularly because it affects pulse shape and amplitude. The three exposures in Fig. 5 are expanded trace views showing how pulse amplitude diminishes with decreasing supply voltage. These pictures, obtained by probe contact at the plate of horizontal output tube, show a simultaneous reduction of the wavetrain following the pulse.

Reduction of heater voltage at the damper tube may also cause reduced pulse amplitude along with distortion in the wavetrain as shown in Fig. 6. Reduced cathode emission within the damper tube produces a similar effect.

The use of a d.c. oscilloscope for examination of these waveshapes has one special advantage; three standard conditions of "B" voltage can be rechecked conveniently when desired. The triple exposure in Fig. 4, made with probe contact at the damper-

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TRANSFORMER CATALOGUE

Milwaukee Transformer Company, 5231 North Hopkins Street, Milwaukee 9, Wisconsin, has just released a new, 16-page catalogue to the electronic trade.

Designated as catalogue MTR-1, the new publication describes a varied line of transformers, reactors, filter networks, and similar components which have been specially engineered to the rigid requirements of commercial and government agencies.



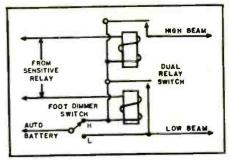
Headlight Dimmer

(Continued from page 35)

second stage because without heater excitation no plate current can flow. The current drain on all the batteries is very low and they should provide almost shelf life. The circuit could be designed to use the auto battery as one of the bias cells as well as for heater power but this is not advisable because the grid voltages are quite critical and the 6 volt system in an automobile varies considerably with engine speed.

A 0.01 μ fd. condenser is connected from grid to cathode of each stage to prevent any a.c. voltages from appearing at those points. If this precaution were not taken, the circuit might oscillate and would surely pick up ignition noise and possibly even r.f. It is the combination of C_1 and R_2 in the first stage that gives the circuit the slow reaction to changes of light intensity. This reaction can be slowed even more by increasing the value of C_2 .

The sensitive relay in the plate circuit of the second stage of the amplifier has a 10,000 ohm coil and can be adjusted to close at about 2 milliam-



Wiring diagram for a conventional auto headlight system. See text for details.

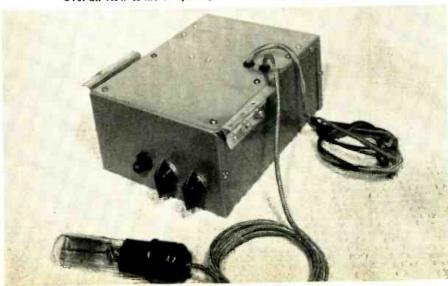
peres. The contacts form a single-pole. double-throw switch. The armature of the relay is grounded. The normally-closed contact goes to the relay switch operating the "high" lights and the normally open contact goes to the relay operating the "low" lights.

The unit was constructed in a small aluminum box 8" x 6" x 4". Care must be taken to mount the sensitive relay in a horizontal position so the vibration of the auto cannot interrupt its operation. Also, the resistance between the grid and cathode of the first stage of the amplifier should be kept as high as possible because a resistance of less than 10 megohms will cause considerable loss of sensitivity. Four wires are brought out of the box one for filament power, two for the headlight relay switches, and one for the phototube. The wire for the phototube is shielded to prevent any stray pickup. The entire unit is mounted on two aluminum flanges beneath the dash panel of the automobile. phototube can be mounted behind the windshield in any convenient place.

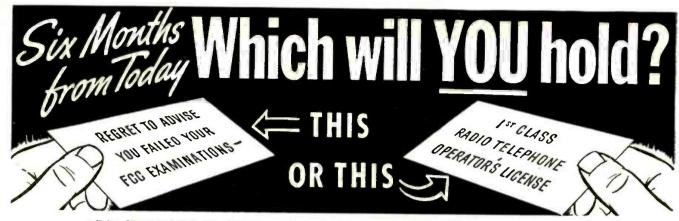
This unit was installed on a 1946 Chevrolet and a dual headlight relay had to be installed on that car. The wiring of the headlight control system would have to be adapted to the particular car. of course. In any case, the foot dimmer switch should be wired to override the photoelectric dimmer as a safety precaution.



Over-all view of the complete photoelectric headlight dimmer unit.



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ready for distribution, according to word received from the company.

The new 1953 listing describes and illustrates over 30,000 products. This 224-page edition is the largest in the company's history and includes a new 32-page rotogravure section devoted to the components of high-fidelity custom music systems.

Although primarily designed for the industrial and laboratory user of electronic parts, the new catalogue includes sections on public address systems, amateur radio gear, hand tools, books, intercoms, kits, and emergency communications equipment.

The new catalogue is available from the company at 167 Washington Street, Boston 8, Massachusetts.

WRL CATALOGUE

World Radio Laboratories, Inc., 744 West Broadway, Council Bluffs, Iowa, has announced the issuance of a new catalogue covering electronic compo-

Comprising 130 pages, the new WRL catalogue lists many new items of interest to the purchasers of all types of amateur and other electronic equipment and components. Copies are available on request.

AUDIO CATALOGUE

Harvey Radio Company, Inc., 103 West 43rd Street, New York 36, New York, has issued a new catalogue devoted exclusively to high-fidelity audio equipment.

Designated as Catalogue No. 54, this new 36-page publication lists hundreds of items for the audiophile. Included are AM-FM chassis and tuners. amplifiers, baffles, cabinets, cartridges, changers, disc recorders, equalizerpreamps, high-fidelity speakers, pickups. phonographs, tape units, etc.

In order to insure maximum usability, the company has not only listed and illustrated each piece of equipment but provided technical data and performance information.

MAGNETIC DOOR LATCH

A catalogue sheet which describes all of the features of its new magnetic door latch is now available from Heppner Sales Company, Round Lake, Illinois.

The product described in the sheet is suitable for either wood or metal doors, retains its magnetic properties, and since it incorporates no working parts, will last indefinitely.

HAM BOOKLET

The Allied Radio Corporation, 833 West Jackson Boulevard, Chicago 7, Illinois, in cooperation with the ARRL, is distributing a free booklet to radio clubs, radio classes, and all other groups of radio or electronic students or hobbyists.

The booklet, "You Can Be There," is a dramatic story of the romance of amateur radio and the thrills that come with the hobby of operating a ham station.

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MANUFACTURERS' LITERATURE

Readers are asked to write directly to the manufacturer for the literature. By mentioning RADIO & TELEVISION NEWS, the issue and page, and enclosing the proper amount, when indicated, delay will be prevented.

UTC TRANSFORMERS

United Transformer Company, 150 Varick Street, New York 13, New York, has released a new catalogue which lists over 600 stock items covering the entire scope of electronic transformer applications.

The new publication is fully indexed, giving complete technical descriptions of all items. In addition, a center insert gives circuit details for high-fidelity amplifier equipment.

Transformers for high-fidelity systems, hermetically sealed units for military applications, special transformers for hams, and a replacement line are covered along with listings of high "Q" filter coils and complete audio filters.

CRYSTAL CATALOGUE

James Knights Company of Sandwich, Illinois, has issued a completely new catalogue covering its line of stabilized quartz crystals.

The catalogue lists 45 different crystals for use in communications equipment, laboratory instruments, medical and industrial equipment, etc.

Development engineers and others will find the new catalogue of interest. Copies may be obtained by writing the company direct.

SOUND SYSTEMS

Mark Simpson Manufacturing Co., Inc., 32-28 49th Street. Long Island City 3, New York, has issued its new general catalogue of 1952, revising its catalogue No. 50.

A complete line of school and institutional sound systems using control amplifiers with microphone, radio, and phonograph inputs for up to 40 locations is only one of the many groups of modern equipment featured.

Other items listed include highpower amplifiers, high-fidelity amplifiers, transcription equipment, mobile, and preamplification equipment.

ALLIED'S 1953 CATALOGUE

Allied Radio Corporation, 833 W. Jackson Boulevard. Chicago 7. Illinois, has released its 1953 general catalogue which contains 236 pages—the largest catalogue in the company's history.

Among the 18,000 items listed in the new publication are sound systems, television chassis, boosters, rotators and u.h.f. converters, table model and portable radio sets, professional and home recording equipment, public address amplifiers and complete systems. amateur receivers, ham transmitters and other gear, industrial v.h.f. radio and radiotelephone

equipment, as well as tools, books, hardware, kits, and other supplies.

The high-fidelity section has been expanded to include many units for custom installation: amplifiers, tuners, changers, speakers, preamps, and cabinets.

Copies of the new catalogue No. 131 are available on request to the company.

SOUND EQUIPMENT

A new eight-page, two-color catalogue illustrating and describing the fifteen 1953 models of *Califone* phonographs, transcription players, and sound systems has just been released by *Califone Corporation*, 1041 North Sycamore Avenue, Hollywood 38, California.

Accompanying the catalogue is a combined specification and price sheet for easy selection of equipment to fit the customer's requirements.

Copies of the new publication are available from the company direct.

ANNIVERSARY CATALOGUE

Burstein-Applebee Co., 1012-14 Mc-Gee Street, Kansas City, Missouri, is currently distributing copies of its 25th Anniversary catalogue. No. 531.

This 148-page catalogue lists thousands of parts and equipment items for dealers, technicians, schools, broadcasters, public utilities, experimenters, factories, engineers, laboratories, and hams.

A comprehensive index has been included to facilitate locating the part or unit desired.

Copies of the new catalogue are available without charge on request.

TRADE-IN GUIDE

Publication of the first television set trade-in guide, the "1953 NARDA TV Blue Book," has been announced by the National Appliance Guide Company, 2132 Fordem Avenue, Madison 1. Wisconsin.

The manual provides authentic, detailed, up-to-the-minute information on all popular TV sets of over 30 leading manufacturers and covers models produced from 1947 through 1952. The annual guide tells the dealer how to evaluate trade-ins, how to service them, and how to resell them to his and his customer's satisfaction.

Details on how copies of this manual can be obtained will be supplied by the company on request.

RADIO SHACK CATALOGUE

Copies of Radio Shack Corporation's 30th Anniversary Catalogue are now

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As you know, our reception produced down here that has come along the fringe area position. that has come along has been tried.

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155	.64	6AH6 1.05		6L6GA . 1.05	12AT776	25L6GT54
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1U4	.69	6AL554	6BJ661	6SC776	12AU765	358561
105	.61	6AQ554	6BL798	6SF558	12AV788	35C561
1X2A	.79	6AO6 49	6BN672	6SH765	12BA654	35L6GT61
304	.75	6AR554	6BQ6 1.08	6SJ754	12BE658	
305GT .	.72	6AS562	6BQ7 1.08	6SL7GT65	12BH782	35W441
354	.65	6AT646	6C449	65N7GT73	125A7GT .62	35Z5GT39
3V4	.65		6C557	6507GT49	125G761	50B561
	1.31	6AV5GT. 1.09		65R749	12SH7 49	50C561
5U4G	.54	6AV646		6T887	12SK7GT .63	50L6GT59
5V4G	.98		6E576		12SN7GT .73	117Z354

Many other types equally low priced—include all your tube needs with y
One of the largest stocks in the country!
Min. Order \$25.00. Terms: 25% with order, balance C.O.D. All prices subject to change without notice, F.O.B. New York City. Mail order division.

ision Materials Corp. 125 Cedar St., New York 6, N. Y. Cortlandt 7-4307

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CRYSTALS



in FT 241-A Holders—½"
Pin SPC, Marked in 54th OR 72nd
Harmonic MC Freq. Listed below
by fundamental frequency with
fractions omitted.

500 KC Crystals. ..ea. \$1.95 1000 KC Crystals \$3.95

		e a.	90,30
407	444	476	509
408	445	477	511
409	446	479	512
411	447	480	513
412	448	481	514
413	450	483	515
414	451	484	516
415	452	485	518
416	453	486	519
418	454	487	520
419	455	488	522
420	456	490	523
422	457	491	525
423	458	492	526
424	459	493	527
425	461	494	529
426	462	495	530
427	463	496	531
429	464	497	533
430	465	498	534
431	466	501	536
433	468	502	537
434	469	503	538
435	470	504	540
436	472	505	-
437	473	506	\$ 00
438	474	507	4
440	475	508	Each
441			
442			
	4 0 8 4 0 9 4 1 1 4 1 2 4 1 3 4 1 4 4 1 5 4 1 6 4 1 8 4 1 9 4 2 0 4 2 2 4 2 3 4 2 4 4 2 5 4 2 6 4 2 7 4 2 9 4 3 1 4 3 3 4 3 4 4 3 5 4 3 6 4 3 7 4 3 8 4 4 4 0 4 4 1 8	408 445 408 445 408 446 411 447 412 448 413 450 414 451 415 452 416 453 418 455 420 456 422 457 423 458 424 459 425 461 426 462 427 463 430 465 431 466 433 468 434 469 435 470 436 473 438 474 440	407

406 443 10 for 58.00. Pastpaid

FOLLOWING CRYSTALS AVAILABLE IN FT 243 HOLDERS 1/2" PIN SPACING

7075	11 for 510.00	Postpaid		
6150		EACH		
6140	8025	\$100		
6075	8006.7			
3590	7350	8200		
3500	7150	8075		

PLEASE ENCLOSE FULL AMOUNT WITH ORDER QUANTITIES AVAILABLE WRITE FOR YOUR REQUIREMENTS

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Box 356-JT. East Pasadena Sta. . Pasadena 8, Calif.



THE AUDIO PERFORMANCE OF



\$20.00 Amplifier 2

(Continued from page 45)

The critical point here is that excessive feedback cannot be used, due to the phase shift of the circuits and the transformer, dependent on the instantaneous frequency. The attenuating resistance in the loop has been chosen to develop optimum feedback within the limits of the transformer.

Power was taken from an existing supply, but could as easily have been drawn from a radio or other source. Power supplies are all similar, and any discussion here would be redundant. All that is needed is 350-400 volts at 110-120 ma. The entire circuit is stable, as regards frequency response, and will operate as well with 350 volts as 400, with hardly noticeable loss of power under normal demands.

The cost of all the parts in this amplifier is \$20.00 or less.3 This sum can be flexible since almost endless variation is possible in the actual construction, limited only by the needs and ingenuity of the constructor.

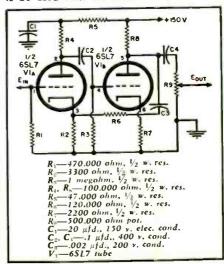
Preamplifier

Because six different preamplifiers tried in the past year have been unsatisfactory, the circuit shown in Fig. 6 was built for use with the amplifier. The preamplifier is quite simple, and without complications. Immediately apparent is the absence of tone controls. Distortion created by tone controls is apparent to most listeners only when all tone controls are bypassed, and the sound is heard through a familiar system. The circuit is designed to develop sufficient voltage to drive the amplifier to peak undistorted power when used with a G-E RPX-040. or similar type, variable reluctance cartridge.

REFERENCES

1. Tele-Tech, January 1952, pages 90-94. 2. Audio Engineering: "An Ultra Linear Amplifier!" November, 1951. 3. Allied Radio Corporation: Catalogue No. 127.

Fig. 6. Diagram of preamplifier designed to be used with the author's amplifier unit.



RADIO & TELEVISION NEWS

Write for complete technical data, and be sure to listen to the new BEROIK at your local dealer's Sound Department.

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GENUINE STANDARD COIL T.V. BOOSTER Not Surplus, But Right From the Factory

NOT SUPPIUS, BUI RIGHT From The Pactory

Latent Model P-51 Standard Coil Television Booster. McGee
makes another pelvy jurchase and as usual, passes the saving
on to you. The fact process of the particle of



\$11.95

McMURDO SILVER BOOSTER \$10.95

Sensational value. Continuously variable inductance type tuner, from channel 2, including 1671 and, through channel 137 from channel 2, including 1671 and, through channel 137 from channel 2, including 1671 and, through channel 137 from the corporates a 646 tube. Input for 1300 ohm, output to the TV set. Single knob tuning. Attractive plastic case, McMurdo-Silver Super Sonic TV:FM booster, State No. 61-61, Shipping weight 5 lbs. McGee's terrific and price, \$40.95 cmb, two for \$20.00.



1952 MODEL ASTATIC \$19.10

New Astalle "Scanafar" TV booster with mapposement to match the newer model TV receivers, Michael Commission and the seven model TV receivers, Michael Commission and the seven masking the seven masking of the seven mask

1952 MODEL REGENCY S19.10

14-17-20 INCH CONV. KITS AT SCOOP PRICES 20 IN. CONV. KIT \$29.95

Our 20" conversion kit includes a 6-month guaranteed 20HP4, 20" reclangular blackface picture tube, plus a 14,000 will 6.E. 20 plus a matched 700 plus a p

14-INCH CONVERSION KIT \$19.95 | 17-INCH CONVERSION KIT \$24.95

Our 14° conversion kit includes an RCA 1-16P4, 14° rectangular blackface tube, plus a 1-1.000 volt (19° costine yoke, plus a 14° ilestifas gold trimmed misk, Offered at the very low price of only \$19.95. Sugested diagram furnished. Ship, weight, 20 lbs. Via express of truck only. Stock No. RC-14X, net price, 519.95.

RED HOT INTERCOM VALUE!

3-STATION INTERCOM MASTER, \$14.95

Jacob Nitercom Master, \$14.95

USE UP TO 3-SUB STATIONS, \$4.49 EACH

A red-hot intercom master value. A full 3 tube. 110 voit ACDC master, with 3 station selector switch and easy necessible
volume control. Small compact size. 5"x6"x61½" high. Makes
an attractive intercom installation. May be used with from one to
tirree of our G-4T substations described below. Intercom master
is quiet at all times, except when press-to-talk switch or callstock No. 83 one of the subs is pressed. Shipping wt. 5 lbs.

Kock No. 83 one of the subs is pressed. Shipping wt. 5 lbs.

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Substation, with Affice of the substation of call-inack switch. May be purchased with
or without master station. Shipping weight 2 lbs. Net \$4.95 ca.

3 wire plastic intercom cable. 100 (t. \$1.85.55 tool ft. \$8.95.



TERRIFIC VALUES IN SPEAKERS AND BAFFLES

8" PM AND LEATHER-ETTE BAFFLE, \$4.95 LOTS OF 10, \$4.75



12" PM AND WALNUT BAFFLE, S9.95 LOTS OF 3, 58.95

The finest built 12" Walnut plywood wall baffle we know of Factory cost of the plant of the plan



RCA 201E1 T.V. TUNER \$7.95

Terrific buy on this RCA tuner. We have a limited quantity of the famous original 201E1, 13 channel completely wired and tested TV front end tuners. Ready to connect to your TV video I.F. strip. Offered at a sacrifice. Price was \$44.00. Now only \$7.95 each, with tubes. Each tuner in good condition but has been repaired. Stock No. RCA-13P. TV front end tuner. Convertor coll type for separate sound as used in the famous 630 chassis. Complete with 3-636 tuhes. \$7.95. Specify shaft length desired, either 2" or 4".

RCA 201E-1 T.V. TUNER
Same as pictured above only new-with tubes. Stock No. 2701. Sale Price, \$11.95.

3-TUBE SARKES-TARZIAN T.V. TUNER

This popular Sarkes-Tarzian Type 3 tuner is widely used. 13 channel rotary type switch with individually tuned coils. Price is complete with diagram and three tubes: 624 osc., 6BH6 R.F. and 6AG5 mixer. Regular factory cost is twice our price. Each tuner is wired ready strip. May be used with either inter-carrier or separate descent of the strip. Say be used with either coil. built in fine frequency control. Sarkess flast built-on convertor coil. built in fine frequency control. Sarkess alan Ty tuner, with 59.95 each. Specify shaft length, either $2\frac{1}{2}$ or $4\frac{1}{2}$.



tubes.

RCA PRINTED CIRCUIT T.V. TUNER \$14.95

RCA Printed Circuit T.V. Tuner with 616 and aCB6 tubes. Similar mechanically to the standard coil (same knobs 61). Snap-in channel segments. Has 61/2" shaft. Used on late Hallerafters T.V. sets. Stock No. RC-A12. 12 Channel Tuner with Tubes. New, \$14.95. Knobs, \$9c.



T.V. TUNER FOR EMERSON \$12.95

STOCK NO. SC-947E

For Emerson 050D ETC. Has 21/2" insulated shaft and tubes 0BC5—filaments in series—shunted to .6 amps. Stock No. SC-947E. Sale Price, 512.95. Knobs. 59c.

T.V.-RADIO NEWS SPECIAL S9.95

T.V. COMPONENT DEAL #CGE

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3 Flybacks and 3 Ineflection Yokes, for \$9.95.
You get 3 deflection yokes, 2-70° yokes, and |-55° yoke and a horizontal tyback transformers. 2 General Electric 14.000 yolt ceramic core 70° and 1 carly modes yolt ceramic core 70° and 1 carly modes than our Price for the complete second of the price of the complete second yold with the price of the complete second yold you will be a standard 4-wire vertical nutruit transformer, yold a standard 4-wire vertical nutruit transformer, julia a 70° cosine deticion yoke (no tules) included). It's worth \$20.00. Our sale price, only \$12.95.



TERRIFIC COMBINATION CABINET SALE

Originally intended for an Admiral 14" TV combination. Made of walnut veneer, 32" wide, 35½" high and 20" deep. Offered at less than the factory production. Made of walnut veneer, 32" wide, 35½" high and 20" deep. Offered at less than the factory production of the second construction of the

CAPEHART CABINET FOR 1000 SET-ONLY \$995



The finest Leatherette Baffle we have ever offered. New self-supporting plastic grill material. baffle is covered tan with matching grill, Offered with a good heavy duty 8" Almico V PM speaker with 3.2 onm voice coil. Stock No. 818. Speaker and Haffle, \$4.95 ea.; lots of 10. \$4.75.
8", Haffle only. Stock No, NV-8, \$2.29 ea.; 101 of \$19.95. COMPLETE RADIO, TELEVISION

3-WAY PORTABLE KIT

\$1595



A NEW '52 MODEL

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New 1952 Model 3-way

Personal portable radio

kit. Operates on 110

Polis 11½ voit see contained hatterles.

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Receives broadcast 550 to 1650 kg. 4 A

conventional 2-gang supernet circuit with

456 KC fron core IF's. Incorporates the

new super gain stick loop antenna. All

plated chassis. Lal. approved circuit—

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Build Your Own \$795 Phono-Mike Broadcaster THE REAL PROPERTY.

Broadcaster River Broadcaster

8-Tube Hi-Fi Amplifier Kit S29.95

8-Tube Hi-Fi Amplifier Kit \$29.95

A comblete kit Including tubes: 3-7E5.
2-6.33 russ rectifier diagram and photos. Inputs for rar and photos. Inputs for rar and of Photon of P

10-Watt Hi-Fi Amplifier Kit \$14.95



of paris including of paris in gratuble in

AND AMPLIFIER KITS AT McGEE 10-TUBE RADIO KIT \$29.95



fer. d ta-gram an od-gram an od-linstructions. 3 gang superhet with 8" silde rule dial. Chassis size. 12½"x10"x61½" rule dial. Chassis size. 12½"x10"x61½" audio. Outjut marches 3 to gram of the coll speakers. Inputs for G.E. variable re-luctance or crystal phono bickup and crys-tal mike. Heavy duy power transformer. tal mike. Heavy duy power transformer. seight 18 lbs. Net 529, 95.

17, 20" T.V. Kit \$59.95 Less Tubes



6-TUBE 2-BAND KIT \$14.95



5-TUBE AC-DC KIT S12.95

Model RS-5. A 5 tube AC-DC straight broad-cast kit, housed in the same cabinet as ME6-2 above. Complete with tubes. Ship-ping weight 10 lhs., Net \$12.95.

AC POWERED BROADCAST TUNER KIT \$12.95



A self-powered, 3Sang superhet tuner
kit with R.P. stare.
This complete kit is
furnished with a
diagram, photos and
tubes, 6.4U.6 R.F.,
6ii.66 oscillator
R.F., 6.4U.6 p.F.,
ceter. 6Al.5 diode.
Ceter. 6Al.5 diode.
Chassis size, 9.42x444/c, high. Shiphing
weight, 7 hs. Broadcast uner kit Model
BT-38X. Net price, \$12.95.

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Prices F.O.B. K.C. Send 25% Deposit with Order, Balance Sent C.O.D. With Parcel Post Orders, Include Postage

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HOW TO ORDER: Send full remittance and you save the added C.O.D. collection fee, or if you wish include a 25% deposit and the shipment will be made C.O.D. for the balance. All prices F.O.B. Kansas City. Missouri. Specify whether you wish shipment to be made by Express or Truck. Amplifiers are not mailable.



28 WATT \$15000 LIST PORTABLE P. A.ON SALE \$6995

3-SPEED PHONO TOP-TWO 12-INCH SPEAKERS 7-TUBES PUSH PULL 6L6'S HEAVY LEATHERETTE COVERED PLYWOOD PORTABLE CASES CRYSTAL MIKE \$8.95 EXTRA

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STOCK No. AP-28X. Portable 28 watt public address system. You get a 7 tube heavy duty push pull 01.6 amplifier with inputs for 2 mikes, either crystal or dynamic with separate mixing volume controls. One phono input years are to encountrol high fidelity, wide range trequency respired to the property of the control high fidelity, wide range trequency respired to the property of the control high fidelity, wide range trequency respired to the control of the c

VIDZ.

OCK NO. AP-28X complete portable PA system with 3 speed phono and speakers pictured dess mike slip, wt. 71 lbs. \$69.95.

ectro Solo model PH \$25.50 lbs crystal mike with 20 feet of cable and desk out type mike stand instead of desk stand \$4.95 extra.

EF OFFERING TO THE RIGHT FOR WALL SPEAKERS INSTEAD OF THE PORT-BLE SPEAKERS.

28-WATT AMPLIFIER WITH 12-INCH WALL SPEAKERS



50 WATT \$25000 LIST PORTABLE P. A. ON SALE \$9995

3-SPEED PHONO TOP-TWO 12-INCH SPEAKERS

10 Tubes — 4 6L6's

Heavy Plywood Tan Leatherette Covered Cases

Heavy Flywood Tan Leatherette Covered Cases

STOCK No. AP-60x. Portable 50 wait public address system. You get a 10 tube amp with (4-61.6) push pull parallel 61.6 output tubes. Inputs for two mikes either crystal or dynamic, with separate mixing type volume controls. One phono input. Twin tone controls one for bass the other for treble high fidelity wide range frequency response. The heavy duty output trans, has taps for 4, 8, 16, 125, 250 and 500 ohm speakers with 25 foot cables and pluts. Each speaker is mounted in large separate cases, one is used to carry the amp. Each case is 21 x 21 x 11 linenes with removable stage of the property of the case is 21 x 21 x 11 linenes with removable size and weight are rated 60 waits, This supper speaker baffling. This is the most powerful portable PA system we have ever offered. Most 4-61.6 amps of this size and weight are rated 60 waits. This amp will put out 4 waits all day long and 50 to 60 waits with ease. Furtipped with a 3 speed phono motor and pick up to play all records. 313, 45, 78 mm. A \$250.00 list value. Ship, wt, Into His. \$100.00 to 10 waits all day long and 50 to 60 waits with ease. Furtipped with a 3 speed phono motor and pick up to play all records. 313, 45, 78 mm. A \$250.00 list value. Ship, wt, Into His. \$250 to 10 waits all ship with 10 with 20 feet of cable and desk stand \$11.95 extra.

If floor stand is desired instead of the deak stand and \$4.95.

If floor stand is desired instead of the desk stand add \$4.95.
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50-WATT AMPLIFIER WITH 12-INCH WALL SPEAKERS



trans.
STOCK No. 55-60X 50 watt amplifier
with 3 speed phono and 2 12 Inch wall
speakers. \$99.95. Flectrovoice 610
dynamic mike \$11.95 extra Floor
trand instead of desk stand \$4.95 ex-

extra 12 inch speakers and wail baf-fles \$14.95.



10 WATT \$9000 LIST PORTABLE P.A. ON SALE \$4295

STOCK NO. AP-11X. A 5 tube 10 watt (14 watts peak) push pull 7C5 U. L. approved amplifier with wide range frequency response. Inputs for one mike and one phono. Separate mixing volume controls. Fully variable tone control. Heavy plywood leatherette covered case is equipped with a heavy duty 10 inch Alnico V magnet PM speaker. The amp fits inside the speaker case. Case size 21 x 16 x 13 inches has removable snap on back, (note, this portable system has only one speaker whereas the 28 and 50 watt models shown above have two). The top of the amplifier is equipped with a 3-speed phono motor and pick up for all records, 3313, 45, 78 rpm—this portable PA system has a filst value of \$90.00. Offered by McGee at a terrific saving.

STOCK NO. AP-11X. 10 watt portable PA system with 3-speed phono. Ship wt. 41 lbs. Sale price as pictured best mike \$42.95. Crystal mike with non removable desk stand \$3.95

3-Speed Phono Top-Heavy Plywood, Tan Leatherette Case 10" Alnico PM Speaker—Crystal Mike \$3.95 Extra

The 10 watt portable PA system shown on the left is offered less the phono top. Specify stock the 10 watt portained to the phono top. Specify stock to AP-11NO. Sale price \$34.95 less mike.

Tystal mike with non removable desk stand \$3.95 extra.

McGEE'S \$62.50 LIST 15" COAXIAL SPEAKER, \$21.95 21 OZ. ALNICO V MAGNET-5" TWEETER

This is the finest 15" coaxial PM speaker vane that we have ever offered. New 1932 per property of the propert

music lover's amplifier. Stock No. P15-CR-shipping weight I3 lbs. Net price \$21.95.

12" JENSEN PM, \$15.95

12" COAXIAL SPEAKER, \$12.95



McGee Scant: Jenson Concert 12.
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Alto Vingraet PM speaker, G.I. 3-SPEED CHANGER WITH G.E. \$225

VARIABLE RELUCTANCE TURN-ABOUT CARTRIDGE

Another tremendans McGee Scoon: Brand new General Instrument
Senseria automatic record changes. Complete with RPN-050 G.E.
variable reductance cartridge with turn-about stvlus, Plays all 3
speeds automatically. 7". 10" or 12" records, Has relect button,
Repeats last record. Base size. 12"x12%". Nhipping weight 14
[bs. Stock No. 710-GE. Scoop price, \$22.58].

but with Webster flip-over twin needle cartridge.

ESPEY 12-TUBE FM-AM CHASSIS, \$59.95

- * BUILT-IN PRE-AMP FOR G.E. VARIABLE RELUCTANCE PICK-UP
- WIDE RANGE AUDIO
- WHY NOT ORDER WITH A COAX-IAL SPEAKER AND A RECORD CHANGER? SEE OUR SPECIAL OF-FERING

hecies's new 1952 model 12-tube FM-AM chassis, Latest design with phono imputs for all types of record players, crystal or G.E. variable refuctance. Receives standard broad cross of 1700 kc and FM standard broad cross of 1700 kc and 1700 kc and 1700 chassis size, FM antenna may be stapled in cabinet, Attractive lighted slad of 8840, 12AT7, 6817, 131 g x 9 high and 11 deed, Complex with 373GT rectifier. Shipping weight 20 lbs, Stock No. 72 kc and 1700 kc a



ESPEY DEAL (2), \$118.95

espey 7-C chassis cumplete with 12 coaxial PM plete with 12 coaxial pm

ESPEY DEAL (3) \$138.95

CGEE RADIO COMPANY

TELEPHONE VICTOR 9045. WRITE FOR FLYER 1422 GRAND AVE., KANSAS CITY, MISSOURI

Mac's Service Shop

(Continued from page 60)

to meet competitive prices and for not having limitless time at their disposal for working out every last bug from a new model. You do not seem to realize that you are second-guessing all of these errors. They might prove to be a lot harder to see if you were depending upon foresight instead of hindsight.

"And this prod is for your doing all your yelling where it will do no good. If you see a mistake has been made in the design of a chassis or a record-changer, why don't you sit down and write a courteous letter—not one of the smart aleck, how-can-you-be-so-dumb type—to the manufacturer telling him what you have found and making suggestions for correcting the trouble? You may be surprised at the apprecation he will show, and you can be certain he will not repeat the mistake in future models.

"I might suggest, too. O Bumptious One, that sometimes you are guilty of trying to blame your own lack of service skill and enterprise on to the setmaker. Time after time I have seen your kind try to persuade yourself that a poorly-operating set never did work any better, that it was made that way; consequently, nothing could be done about it. How you can make yourself believe anyone would pay his good money for a new receiver in that condition I'll never know. would concentrate more on improving your own knowledge and technique instead of always being so alert to catch the manufacturer off base, you'd be a better technician for it.'

"Hey, lemme see that techniciandoll of yours," Barney demanded as he grabbed it from Mae's hand. "Uh huh, it's just as I thought. Did you have to make him with red hair?" he asked plaintively.

"You know," he went on reflectively, "I'm beginning to think there is something in this voodoo stuff after all. I could have sworn that I actually felt some of those jabs you gave this little feller."

"Imagination—and a guilty conscience—can play strange tricks." Mac commented; "but let's get away from all this hoeus-pocus and talk a little sense. I ran aeross something yesterday I think may interest you. A fellow came in with the complaint that his radio-controlled garage door had suddenly become very erratic in its behavior. It opened and closed of its own accord while the car that had the controlling transmitter was miles away and the transmitter was shut off.

"I went over and checked the thing over carefully, but I couldn't find a thing wrong with it: a good healthy signal from the transmitter was required to trip the pilot relay; there were no gassy tubes to cause trouble; running the line voltage up and down made no difference. First thought of mine was that possibly a harmonic of a ham transmitter was getting into the receiver and making the relay trip, for I have read of that; but since Ten went dead none of the local gang are working the high-frequency bands; so I decided to look for something else. I asked the man if any new electronic equipment had been installed in the neighborhood lately, and after I explained what 'electronic equipment' was, he said all he could think of was a new TV set in the house across the street that had been in for a couple of weeks.

"Playing a hunch, I went over and asked the folks if they would mind turning on their TV receiver for a few minutes. As I stood in front of the receiver I could see the closed garage doors; and when I turned the channel selector to Channel 10, the doors opened up. I tried it two or three times, and every time the set was tuned to Channel 10, the doors worked, With the i.f. used in that set, the oscillator was on about 219 megacycles when the receiver was tuned to Channel 10, and that is squarely inside the 210-250 megacycle band in which the door-opener works. Fortunately, provision had been made for using any one of six different frequencies in the garage-door setup; so I just moved the transmitter to a different frequency and peaked up the receiver on that. When this was done the TV set could be switched to any channel without affecting the doors.

"That is one for the book," Barney said; "and it just goes to show you what a hefty signal is radiated from the oscillator of some of the TV receivers. No wonder we hams get the blame for a lot of blanking out and herringbone patterns that are caused by a neighbor's TV set tuned to a lower channel!"

Within the Industry

(Continued from page 26)

Transicoil Corp. has appointed DWIGHT W. BLOSER to the post of chief engineer in the manufacture of control motors, induction generators, gear trains, and servo amplifiers.

DR. JOHN RUZE has been appointed director of research of The Gabriel

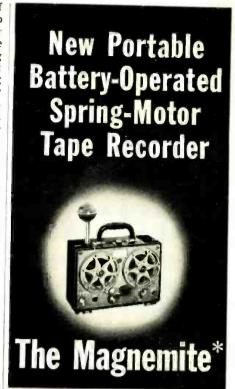
Laboratories, Division of The Gabriel Company.



He joins the company from the Air Force Cambridge Research Laboratories, where he was assistant chief of the antenna labora-

tory. During the war he headed the antenna design section at the Signal Corps Engineering Laboratories.

A native of New York, Dr. Ruze received his doctorate from the Massachusetts Institute of Technology after completing his work for his MS degree at Columbia.



For all field recording without AC power! Smaller and lighter than a portable type-writer, the Magnemite* actually makes field recordings that can be played on any studio console equipment. Completely self-powered, the Magnemite* does away with bulky and cumbersome generators, storage batteries and rechargers.

Just check these unusual features:

- Noiseless and vibrationless governorcontrolled spring-motor assures constant tape speed.
- 100 operating hours per set of inexpensive flashlight-type dry cell batteries.
- Earphone monitoring while recording, and earphone playback for immediate quality check.
- Operates in any position, and is unaffected by movement or vibration during operation.
- Warning indicator tells when to rewind, and shows when amplifier is on.
- Broadcast models weigh 15 pounds. Slowspeed models weigh only 10 pounds.
- Requires no more desk space than a letterhead, measuring only 11 x 8 ½ x 5 ½ inches.

There's a choice of 5 different models for any recording need. High fidelity units, meeting primary and secondary NARTB standards, which record and play back frequencies up to 15,000 cycles, are available for broadcast stations, critical music lovers, and scientific research. For investigation, missionaries, reporters, and general dictation while traveling, there are units which play up to 2 hours per reel of tape.

Write today for complete descriptive literature and direct factory prices.



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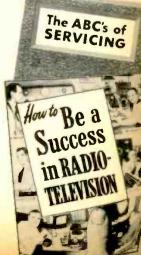
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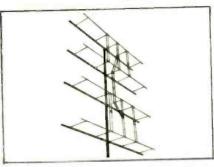
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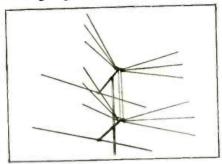
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777 2610 E. 16th Street Brooklyn 35, N. Y. 60 cycles for the vertical sweep system or 15,750 cycles for the horizontal sweep system). The rectangular pulse or saw-tooth waveforms in both systems have components that extend to the fifteenth harmonic (or so) and taking this into consideration only requires that the bandpass be uniform to a maximum of 240,000 cycles.

In the video amplifier stages, the full 4.0 mc. video signal is present, but in everyday servicing you are interested primarily in determining whether the video signal is present rather than accurately depicting its waveshape. Hence, any oscilloscope which possesses a uniform vertical frequency response in excess of 240,000 cycles will be quite suitable for television receiver servicing.

What about those scopes where the vertical response is less than 240,000 cycles? These units can still be used for TV servicing but, of course, the narrower their bandpass, the less accurate will be the reproduction of steep-sided waveforms. Frequently a compensating factor here is lowered cost and this can be very important to the man of limited means. The author has seen scopes with a bandpass of 100 kc. successfully used, but for the beginner the wider bandpass will lead to less confusion.

Oscilloscopes are not the simplest of instruments and individual eccentricities have a lot to do with the one best suited for you. Your best bet is to try to work with as many different scopes as possible and then buy the unit you find easiest to use.

S-38B IMPROVEMENT

By R. E. FRANKLIN. W2EUF

number of the popular Hallierafters S-38B receivers are known to suffer serious volume loss and frequency shift when switched from AM to e.w. These sets use regeneration in the i.f. stage to produce beat-frequency oscillation. Reducing the feedback voltage as follows will decrease the frequency shift and the c.w. volume will be stepped up tremendously.

Originally, the regeneration was obtained from an insulated wire wrapped around pin 4 of the 12SK7 i.f. amplifier tube. By cutting off about an inch of this wire and bringing it within an eighth-inch of pin 4 a point can be found, by trial and error, that will produce the desired results. This will take some care as the hand must be withdrawn each time the wire is moved to avoid body-capacity effects. The wire should be affixed in the correct spot with a generous amount of cement.

In one conversion, one end of a piece of 300-ohni ribbon about three inches long was suspended between pin 4 and a terminal strip anchored by the lug of the i.f. can. The "wrap-around lead" was brought to this terminal and soldered. There will be capacity between the two wires of the ribbon as between the plates of a condenser, and the feedback condenser thus formed can be adjusted to a suitable value by snip-ping off small pieces of the 300-ohm ribbon. Do not cut the ribbon until power is removed from the set.



A. C. Cossor Ltd., parent company of Beam Instruments Corporation of New York, offers the Model 1039B for the American market.

ers give the instrument user a choice between high sensitivity and wide bandpass by providing a suitable switching arrangement. This, for example, is true of the Jackson Model CRO-2 oscilloscope. The "Vertical Input" control has three positions where the vertical system possesses a wide bandpass (response uniform within 10% from 20 cycles to 4.5 mc.) with a fair amount of gain and three positions where the bandpass is reduced (uniform within 10% to 100 kc.), but the gain is up. For each of these positions, attenuation ratios of 100:1, 10:1, and 1:1 are available.

In the *Triplett* oscilloscope, there is a switch at the rear by means of which the bandwidth of the vertical system can be widened from its normal value of 2 mc. to a special value of 4 mc. However, in the 4 mc. position, the

system gain is cut in half.

This matter of bandpass is a source of confusion to many technicians. Just how wide should the vertical system bandpass be for suitable application to TV receiver servicing? The answer to this can be found by analyzing where (and how) the oscilloscope is employed. Broadly speaking, the scope is used in conjunction with a sweep generator to depict the response curve of a circuit or it is used for servicing to show whether or not a signal is present at a certain point in a circuit and, if so, what its shape is.

Oscilloscope use with a sweep generator requires that it be capable of depicting a waveform having a repetition frequency of 60 cycles—this being the rate at which the response pattern is swept out. Hence, the vertical system bandpass should extend down below 60 cycles, preferably 30 cycles or less. The lower this limit, the more linear the response will be at 60 cycles.

For servicing, the oscilloscope finds its greatest application in checking voltage waveforms in stages located beyond the video second detector. These include the video amplifiers, sync separator stages, and the vertical and horizontal sweep systems. In all but the video amplifier stages, the fundamental frequencies are low (either

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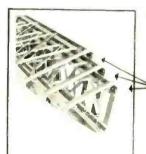
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observe the signal waveforms in these circuits, then an r.f. probe must be employed between the scope and the receiver. The probe contains a germanium crystal or a miniature diode which detects the received signal and then applies the low-frequency modulation of the signal to the vertical input terminals of the scope for screen presentation.

A second type of probe which is finding increasing favor is the low-capacity probe. This probe permits the proper observation of waveforms in circuits that are capacity sensitive and where use of normal test leads would result in a distorted pattern on the screen.

Both probes are auxiliary pieces of equipment and are usually not included with the price listed for the oscilloscopes in Table 1. However, they do serve useful purposes and are recommended. When purchasing these units, obtain those specifically designed for your instrument. This is especially important in the case of the lowcapacity probe.

Bandpass vs. Sensitivity

The function of the vertical amplifiers in an oscilloscope is to amplify applied signals in order that they may be sufficiently powerful by the time they reach the deflection plates to produce a sizable pattern on the screen. The greater the amplification available in this system, the smaller the input signal needed to produce a given vertical deflection. In other words, the oscilloscope becomes more sensitive as a measuring device.

Of importance, too, in the vertical system is its bandpass or its ability to amplify a range of frequencies. The signals whose waveshapes are portrayed on the oscilloscope screen are those found in television receivers, i.e., square waves, saw-tooth waves, and video signals, to mention the more common ones. Each of these waves contain a number of frequencies and to accurately depict their waveshapes. every frequency contained in the wave should be passed by the vertical amplifier system. For accurate television signal observation, this can mean a 4-mc. (or more) bandpass.

The objectives, then, in designing an amplifier for use in the vertical system of an oscilloscope are wide bandpass and high amplification. Unfortunately, for any given circuit, bandwidth X gain is a constant which means that if we increase the bandpass by a certain amount, we decrease its gain by the same factor. Thus, one works against the other and if we desire a wide bandpass, we must make up for the resultant gain reduction by adding more amplifier stages. This, in turn, raises the cost of the instrument.

Most manufacturers of moderately priced equipment resolve this conflict by designing the vertical system amplifiers to possess a nominal band-pass (top limit from 250,000 cycles to 1,000,000 cycles). A few manufactur-

accompany them, it will be found that the horizontal input terminals are sometimes called the "X" axis. This terminology was borrowed from mathematics where it is customary to refer to all horizontal axes as "X" axes. By the same token, the vertical input terminals are referred to as the "Y" axis. And, to complete the analogy, the intensity modulation terminal is known as the "Z" axis.

4. Self-Measurement of Peak-to-Peak Voltages. In servicing a television receiver, it is important not only to observe whether the wave possesses the proper shape but frequently also whether its amplitude is correct. The latter is especially critical in horizontal and vertical sweep systems. Inclusion of some means for measuring the peak-to-peak values of a wave is becoming increasingly popular in oscilloscopes. In its simplest form the manufacturer provides a terminal on the front panel which is internally connected to one of the windings of the power transformer. Usually this is the 6.3-volt winding. When this voltage is connected to the vertical input terminal, by means of a short jumper, the sine wave produced on the screen has a peak-to-peak value of 17.64 volts. This is because 6.3 is the r.m.s. value. When this is multiplied by 2.8 it becomes peak-to-peak.

For convenience, the height of the 17.64-volt wave is adjusted (by means of the vertical gain control) until it occupies one inch vertically on a ruled screen mask. Then the reference voltage is removed and the unknown voltage applied in its place to the vertical input terminal. The height of this wave is then compared to the height of the 17.64-volt wave and by means of a simple proportion, its peak-to-peak value is determined.

Reference voltage values of 1 volt, 3 volts, and 10 volts are also popular in place of 6.3 volts. Sometimes the values are given as r.m.s. and sometimes as peak-to-peak. If in doubt check the instruction manual before using,

Other oscilloscopes have more elaborate measuring systems, some using a selector switch with a series of different voltages available and some going so far as to include a voltmeter on the front panel. Generally, the more reference voltages there are, the more accurate the measurement of the unknown voltage.

When a scope does not contain provision for the self measurement of peak-to-peak voltages, there are voltage calibrators available. These are instruments providing reference voltages which are first placed on the scope screen to calibrate the instrument and then removed while the unknown voltage is exhibited on the screen. Since these units are specifically designed for this purpose, they are frequently simpler to use than the scope system.

5. Probes. Television receivers contain many circuits in which only r.f. signals are present. If it is desired to



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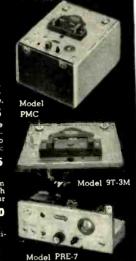
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Precise Development Corp.'s Model 300 oscilloscope incorporates such features as 7" tube, sweep magnifier, complete pushpull vertical from input through output, blanking amplifier, internal square-wave calibrator, gated output with cathode follower, reversible polarity, driven and non-driven sweep, astigmatism circuit, and illuminated scale, to mention just a few.

nal at the output which has the same phase (approximately) as the input signal. By the same token, pass a signal through one or any odd number of amplifiers and its phase will be reversed.

3. Intensity Modulation. This is a binding post on the front panel which is electrically connected to the grid (or cathode) of the cathode-ray tube. Its purpose is to permit a voltage to be applied to the cathode-ray tube so that portions of the trace may be made brighter or darker, as the case may be. This process of varying the beam intensity is known as intensity modulation and many oscilloscopes contain some provision for achieving it. Ordinarily the television technician has little need for this facility; however, it is employed in using the oscilloscope for frequency comparisons.

An application that several oscilloscopes have made of intensity modulation that can be of use to the television technician is the addition of a control known as the "Blanking Phase" control. This control, when turned from its "Off" position, applies a sine wave of voltage to the control grid of the cathode-ray tube. This has the effect of intensifying the trace during a portion of the sine wave cycle and of blanking it out during its most negative portion. The most useful application of this function is the elimination of one of the dual patterns obtained in the sweep alignment of TV and FM receivers. The 60-cycle sine wave applied to the grid of the CRT is so phased, by means of the "Blanking Phase" control, that when the second pattern should be traced out, the beam is blanked out. This results in one pattern, which is much easier to work with.

In working with oscilloscopes or in reading the instruction manuals that

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An open letter to young men of ambition from a pioneer in the field of radio-TV education

~ by ~

E. H. RIETZKE, Founder and President of CAPITOL RADIO ENGINEERING INSTITUTE

IF YOU HAD TRAVELED with me on my recent trip across the United States and Canada, you would have seen with me the proud, grateful, earnest faces of CREI graduates and students. Proud that they had converted ambition into success. Grateful for what CREI had given them. Earnest in their plea to you to study for success.

Personnel Directors and Chief Engineers thanked me for personnel we had sent them—and bombarded me with requests for more.

I received the same reaction in every electronics installation, TV and radio station and factory I visited. I was proud that the professional school which I founded could point to such a fine record of accomplishment.

But I realized that our job has just begun. The growth of the electronics industry thus far is just a trickle compared to the future.

There are already 111 television stations. The FCC, by its "unfreezing" action, makes way for 2000 more stations. Over 18,000,000 TV sets are in use—that is 5,000,000 more than experts predicted there would be in 1954. There are over 100,000,000 radios in operation—in 95% of America's homes—and served by over 2500 radio stations.

Billions in electronics contracts have been awarded in the defense build-up. By 1960, it is estimated that the radio-electronics industry should do no less than \$10,000,000,000 per year, not counting military orders.

This is but a fraction of the picture of expansion.

There is already a gaping shortage of trained men to accept the thousands of openings in development, research, design, production, testing, inspection, manufacture, broadcasting, telecasting and servicing. The best jobs, the highest rewards, the posts of leadership are going to the trained men. And the better the training—the better the results.



If you are a beginner, CREI is not the school for you. There are other schools equipped to do much more for you. In a year or two, they can bring you to the point where you can profitably enroll at CREI.

If, however, you are a graduate of one of these other schools—or if you have been gainfully employed in the Radio-TV-Electronics industry for one year, or more, CREI can help change your life.

I founded CREI more than 25 years ago to provide professional level advanced training for men in the field. 98% of all our students were employed in electronics at the time they enrolled.

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We have prepared a booklet called "Your Future in the New World of Electronics." In it you can find the breath-taking future of the industry, translated into your future. It contains an outline of the CREI curriculum that can transform your life from one of placid, plodding, ordinariness—to a full, happy, successful life of leadership in the fastest growing industry in the world.

Having expressed my pride in the past of the educational system and institution I represent, I make this pledge:

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May I hear from you soon?

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controls, not all of them use the same names. Thus, "Range Frequency" of Fig. 1 is also known as "Fine Frequency," "Frequency Vernier" or just plain "Vernier." Alternate names for this and other controls are listed in Table 2. This is often a big stumbling block to the novice and it would help him considerably if the industry agreed on a standard name for each control.

Other Controls

In addition to the foregoing there are other controls (and their circuits) which broaden the application of the oscilloscope. The more important of these are listed below, together with a brief description of what they do.

1. Phasing Controls. This control, generally designated as "60 C Phasing" or "Horizontal Phasing," is brought into play when the oscilloscope is employed in conjunction with a sweep frequency generator. The sweep generator feeds its signal into one end of the system and the circuit response pattern is developed on the screen of an oscilloscope placed at the other end of the system.

In order that the observed response curve have a linear frequency base, it is necessary that the beam move in step with the changing frequency in the generator. Since the sweep oscillator is driven by a 60-cycle a.c. voltage, horizontal beam deflection should follow suit. To accomplish this, the horizontal input is switched away from its internal saw-tooth oscillator and a 60-cycle sine wave voltage is substituted. Ordinarily, the sweep generator will supply this voltage. However, some oscilloscopes have a special circuit for supplying their own.

Besides the a.c. voltage, some means must be available for bringing the beam in phase with the a.c. driving voltage used to sweep the frequencies hack and forth. For this, a phasing network is employed. One of the elements of the network (a resistor usually) is made variable and this becomes the "Phasing" control. It is adjusted until a single response curve is visible on the scope screen.

2. Vertical Polarity Reversing Switch. This is usually a two-position switch marked "Normal" and "Reverse." When the switch is moved from one position to the other, the pattern on the screen is flipped over or reversed

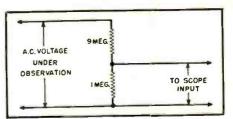


Fig. 3. Voltage divider which can be used when the applied voltage is too high.

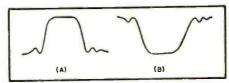


Fig. 4. Patterns for "Normal" (A) and "Reverse" (B) settings of polarity switch.

in the vertical direction. Thus, if the pattern appears as shown in Fig. 4A when the switch is in one position, it will appear as shown in Fig. 4B when the switch is turned to the other position. This is a useful device for interpreting TV video i.f. and sync or sweep waveforms, especially when the manufacturer's manual shows the pattern in one position and your scope shows it in the opposite position.

Reverse pattern on the screen is a source of confusion to many technicians. Why, for example, should the manufacturer's bulletin show the pattern pointing up when your scope has it pointing down? Does it mean that your equipment is hooked up wrong or does it indicate a defective circuit?

Actually, the answer is neither one. The polarity of the signal at various points in a television receiver is important and in general the manufacturer attempts to show the signal as it should be at each specific point. Now, this same signal, fed to your scope, may come out (at the screen) right side up or upside down, depending upon whether your scope has an even or an odd number of stages in its vertical amplifier system. Any voltage passing through an amplifier is reversed in phase by 180°. Therefore, if the signal shown in Fig. 4A is fed into the grid of an amplifier, it will appear at the plate as shown in Fig. 4B. Pass this second signal through one more stage and lo and behold, it is rightside up again.

As a general rule, two or any even number of stages will produce a sig-

Table 2. Alternate names frequently used for various oscilloscope controls. Common abbreviations, such as "Vert." for "Vertical," have been omitted from listing.

NAME OF CONTROL

Vertical Centering Horizontal Centering Vertical Gain Horizontal Gain Sync

60. Cycle Phasing Horizontal Attenuator Vertical Attenuator Fine Frequency Sweep Frequency

ALTERNATE NAMES

Vertical Position. V Center. Y Position Horizontal Position. H Center. X Position V Gain. V Vernier. Y Amplitude. Vertical Amplifier H Gain. H Vernier. X Amplitude. Horizontal Amplifier Sync Amp.. Sync Lock. Locking. Sync Signal Sync Gain.

Sync Control
Horizontal Phasing, Phase
Horizontal Sensitivity, Horizontal Input Control
Vertical Sensitivity, Vertical Input Control
Frequency Vernier, Vernier, Sweep Vernier, Range Frequency

Frequency Vernier, Vernier, Sweep Vernier, Range Frequency Sweep, Sweep Range Coarse Frequency, Steps, Saw-Tooth Sweep Frequency Range



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fiers and their function is indicated in Fig. 1. Just beneath the "Vert. Gain" control is the "Vert. Attenuator" switch. This is a voltage divider network which limits the amount of vertical input signal reaching the first vertical amplifier. There are four switch positions labeled: .5, 5, 50, and 500 volts. These figures indicate the maximum value of input signal that should be applied with the switch in each position. Thus, with the attenuator switch in the 5 position, no signal having an amplitude greater than .5 volt r.m.s. should be applied to the "Vert. Input" terminal (and ground). Excess voltage on any range may produce a distorted pattern or may possibly cause damage. On the other hand, setting the control pointer too high say at 500 volts for an input voltage of 30 volts-will produce a pattern which is too small. In other words, do not set the control too high or too low.

The "Vert. Attenuator" switch receives the applied signal before the "Vert. Gain" control. Hence, the attenuator switch may be considered as a rough adjustment with the gain potentiometer as its vernier.

The last remaining control on the front panel of this instrument (Fig. 1) is the "Horiz. Sens." switch. This 2-position switch is in series with the line from the "Horiz. Input" terminal to the horizontal amplifier. The "Horiz. Sens." is marked "High" for the closed switch position. At this setting the full signal is fed to the horizontal amplifier. The system is thus most sensitive with the switch in the "High" position and affords any applied signal maximum amplification (provided, of course, that the "Horiz. Gain" control is turned up, too).

The "Horiz. Sens." switch is marked "Low" for the open position of the switch and a 12-megohm resistor is placed in series with the input to the 'Horiz. Gain" control.

These markings of "High" and "Low" can be very confusing since they refer to the sensitivity of the horizontal amplifier system and not to the applied voltages. Actually, strong voltages are applied to this system

(Top right) General Electric's Type ST-2A 5" scope. (Center) G-E's Model ST-2B 5" unit. (Bottom right) The same company's Type ST-2C 5" model. (Below) G-E's YNA-4.

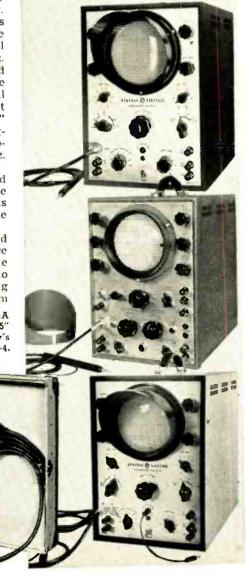
with the switch in the "Low" position since with a strong voltage, less amplification is required. On the other hand, with a weak applied signal, the "Horiz. Sens." switch would be set "High."

Not all scopes possess attenuator controls. In some instruments the applied voltage goes directly to its respective amplifier. When using these instruments be careful not to apply too much voltage otherwise distortion and possible damage may occur. The safe maximum voltage that the oscilloscope can handle will usually be stated in the instruction manual. If it is desired to view the waveform of high voltages, reduce them first to a suitable value by the use of a resistive network such as shown in Fig. 3.

At the bottom of the oscilloscope in Fig. 1 there are six terminal posts through which connections are made to the instrument circuits. Two are for ground; the functions of the other posts are indicated in the illustration.

Alternate Control Names

The foregoing controls have all been part of one instrument. While other instruments have essentially the same



RADIO & TELEVISION NEWS

5 Start This New Year RIGHT!

JANUARY

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2. "Int. Sync"-A linear (or sawtooth) sweep voltage is applied to the horizontal amplifier. At the same time, a portion of the "Vert. Input" signal is fed into the sweep oscillator through the "Sync" control. If the frequency of the applied (or "Vert. Input") signal is near sweep frequency, the pattern can be locked steady on the screen of the cathode-ray tube.

3. "Line Sync"-The saw-tooth sweep voltage is still applied to the deflection plates through the horizontal amplifier. However, now, the synchronizing voltage is not taken from the incoming signal, but from the 60cycle power line. The 60-cycle voltage is injected into the sweep oscillator through the "Sync" control and therefore locks the saw-tooth oscillator in sync with the line frequency. This is usable for applied signals having frequencies of 20, 30, 60, 120, and 180 cycles, and for other subharmonics of 60 cycles.

4. "Ext. Sync"-The saw-tooth sweep voltage is still active. However, now, a synchronizing pulse can be obtained only from an external signal injected into the sweep circuit through the "Ext. Sync" terminal. The setting of the "Sync" control still determines how much of this sync pulse reaches the saw-tooth oscillator.

5. "Horiz. Amp."—In this position the saw-tooth voltage of the oscilloscope's sweep generator is disconnected from the horizontal amplifier and the beam is stationary at the center of the screen in a small, round spot. To obtain any horizontal deflection of the beam, an external signal must be applied to the "Horiz. Input" terminal at the front of the oscilloscope. This signal will be amplified by the horizontal amplifier and applied to the horizontal deflection plates of the cathode-ray tube.

The most frequent use that the TV technician will make of the "Horiz. Amp." position will be in TV or FM receiver alignment. Nearly all sweep signal generators supply their own 60cycle deflection voltage for the oscilloscope and this should be used in preference to any 60-cycle saw-tooth or sine-wave voltage the oscilloscope may be capable of supplying. (An exception to this occurs when the oscilloscope contains specific provision, in the form of a phasing control, enabling it to develop a properly phased pattern.)
The "Function" switch is a con-

venience that is not universally employed. In a number of oscilloscopes, the turning on or off of the power is handled by a separate toggle switch. Another two-position switch might then govern whether the sync voltages are internally or externally obtained. Or, internal sync, external sync, and line sync might be combined in a three-position switch. There are a number of ways of handling this situation and they vary from manufacturer to manufacturer.

On either side of the "Function" switch in Fig. 1 are the gain controls for the vertical and horizontal ampli-

Oscilloscopes

(Continued from page 34)

instruments falls within 60 kc. to 100 kc. For most radio and TV service applications it is seldom necessary to go beyond 30 kc.

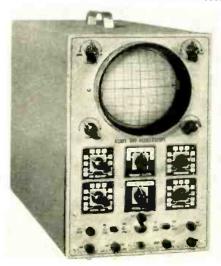
In order to work with any pattern presented on the screen, the pattern should be held stationary. With the "Range Frequency" control, it is possible with some patience to adjust the frequency of the saw-tooth generator until it exactly equals (or is an exact multiple of) the frequency of the applied vertical signal. But, unless this control is constantly adjusted, the frequency of the saw-tooth generator will change (even if only a few cycles) and the pattern will drift.

To keep the trace or pattern steady without constant adjustment of any control, a portion of the incoming signal is fed to the saw-tooth generator and serves to lock the generator in. The "Sync" control enables the operator to vary the amount of synchronizing signal fed to the sweep oscillator. The optimum position for this control is at that point where the smallest amount of sync signal causes the pattern to become stationary. Thus, you start with the "Sync" control at zero and slowly turn it to the right (clockwise) until the pattern locks-in. (It is important before using the "Sync" control to adjust the "Range Frequency" until the pattern is close to being stationary.)

The three controls just described, and especially the "Sync" control, are to be used in conjunction with the "Function" switch situated just below them. The "Function" switch is a 5-position switch which controls the power input and selects the desired horizontal deflection signal. The power is off in the "Off" position of the switch and is on in the remaining four positions. In addition, the switch makes the following connections in its 5 positions:

1. "Off"-Opens the circuit for the power input.

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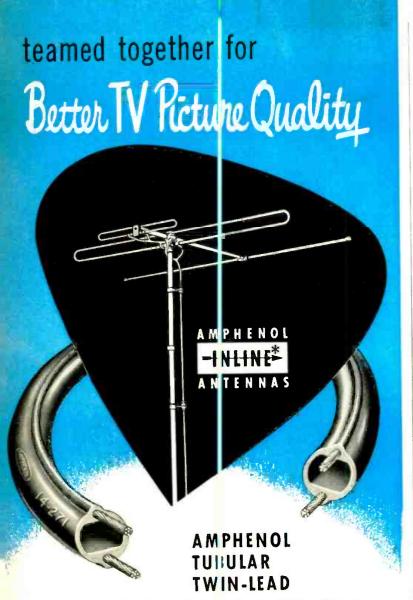
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his illustration clea oncentrated field of wo conductors, whi 128 copper weld wi	energy between ch are 7 strands	

Velocity of Prc pagation	84%
Attenuation d /100 feet	30 mc — .63
	60 mc — .93
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his illustration clearly shows that he oncentrated field of energy between he	200 mc — 1.82
vo conductors, which are 7 strands of	400 mc — 2.7
28 copper weld wire, is contained by	500 mc — 3.0
e tubular construction. This import int	700 mc — 3.6
eld of energy is unaffected by any :x- erior conditions.	900 mc — 4.2

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Dutch New Guinea-Radio Omroep Neuw Guinea, 7.126, Hollandia, lists schedule of 0430-0700, Saturday also 2100-

2300. (Scheiner, N.J.)

Ecuador—HCJB, 11.915, noted 2100-2130 with religious program. (Simpson, Kans.) HC4AS. 4.203, Bolivar, "La Voz de las Caras," is noted signing off weekdays 2330. (Robbins, Ind.)

El Salvador-YSASA, 11.95A, San Salvador, noted around 1830. (Bellington, N.Y.) Gives medium-wave call of YSAS; heard by 0930 and goes past 1700. (Stark, Texas) YSDR. 4.797. Santa Ana, noted with fair level signing off 2210. (Robbins, Ind.)

Ethiopia—The schedule of Radio Addis Ababa, 15.040AV, appears to be rather irregular; has been heard signing on in English 1102; on another day had a missionary program in English when tuned 1032; is identifying more frequently in English now, and some days has English news 1403A; sign-off varies. (Pearce, England) Was recently measured 15.036, but varies. Noted parallel on 6.42, latter quite good from 1230 onwards. (Ridgeway, South Africa) QRA is Box 1364, Addis Ababa, Ethiopia. (N. Z. DX Times)

Finland OIX2, 9.555, Helsinki, heard 2345 with Finnish news and music. (Sanderson, Australia) Noted on this channel opening 2200 with news. (Annala, Oregon)

France-Paris noted signing on in French with "La Marseillaise" 0915 on 15.400 and 17.850. (Pearce, England) Paris is scheduled to Britain daily 0245 on 7.240, 6.145; 1445 on 11.970; Sundays 0800-0900 on 7.240. (Catch, Eng-

Fr. Equatorial Africa-Radio Chad, Brazzaville, is noted on 15.596 at 0030-0130; Radio A.E.F. is heard on 9.96, 15.596, 6.024 at 1200-1500. (Ridgeway, South Africa)

Fr. Morocco Radio Maroc, 6.006, Rabat, is fair to good level around 0200-0300 with native session. (Saylor, Va.)

Fr. West Africa-Radio Francaise Africa Occidental, 9.560, Dakar, noted signing on in French after a march at 0200, then in native African talks and music; noted on 11.896 at 0230. (Pearce, England) The 11.896 outlet opens 1400 with French programs; high level to 1800 closedown. (Ridgeway, South Africa) The 9.560 outlet is heard as early as 1530 to 1730 when closes with martial tune. (Levy. N.Y., Kary, Pa., others)

Germany-Nordwestdeutscher Rundfunk, Hamburg, noted on 11.795 in parallel with 7.290 when tuned 0900, had choral concert from Hanover; was strong on 6.270 with orchestral music when tuned 0345. Berlin, 7.150, Democratische Republic, noted 0115 with news in German, call 0121, then dance and light music. (Pearce, England)

Greece-Kozani, 7.970, is heard in Sweden at 1335 with recorded music; CWQRM. (Malmo DX-aren, Sweden) Larissa, 6.760, relays news in Greek from Radio Athens 2330-2340. Athens Forces Station, 6.330, noted with recorded music 2357. (Kary, Pa.) Radio Athens, 7.300, heard with news 2300; on 9.607 with news (to North America) 1935-1950A. (Pelegri, N.Y.)

Guatemala—Officials list TGN, 580 kc.; TGNA, 5.9525; TGNB, 9.668, and TGNC, 11.850; say "for our English short-wave broadcast we use only the call TGNA." (Fer-

guson, N.C.)

Hong-Kong-ZBW3, 9.525, noted 0430 with "Cantonese by Radio," then musical interlude. (Sanderson, Australia) Noted 0900 at good strength relaying BBC's "Radio Newsreel." (Balbi, Calif.)

India-Latest schedules received airmail from Delhi for All India Radio's External Services are-To East and Southeast Asia 1930-2000, 11.850, 9.630; 2030-2200. 17.740. 15.160; 0600-0815, 17.740, 15.190; 0830-0945, 15.190, 11.780.

(Continued on page 136)

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3,000 Volts. D.C. CURKENT: 0 to 1.5/15/150 Ma. 0 to

D.C. CURRENT: 0 to 1.5/15/150 Ma. 0 to 1.5/15 Amperes.

RESISTANCE: 0 to 1.000/100.000 Ohms 0 to 10 Megohms

CAPACITY: .001 to 1 Mfd. 1 to 50 Mfd. (Quality test for electrolyties)

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with good signals from 1530. (Ridgeway, South Africa) PRL7, 9.72, Rio de Janeiro, leaves this channel daily 1730. (Bellington, N.Y.) PRL9, 6.147, the other Radio Nacional outlet, is usually good level around 2000, some QSB. (Gaylord, Wn. State)

Bulgaria Sofia has replaced 15.330 with 9.700A; has English for North America 2000-2030. (Niblack, Ind.,

Kary, Pa., others)

British Guiana — Radio Demerara, ZFY, 5.980A, has been heard with news 1945; good level in Indiana. (Hord) When this was compiled the Cable and Wireless, Ltd., transmitter ZJA6, 15.075, Georgetown, was being heard throughout the world with relay of sports events (cricket, racing) from ZFY from as early as 1000 to around 1600; may have ceased these special broadcasts by now.

Burma-Radio Rangoon, 4.775. is good level in New Zealand 1000-1015 with English. (N. Z. DX Times) Noted on 9.54 from 0930 with programs in English, recorded music; has news 1000 by man, followed by weather report and program preview for next day; closes 1015A; calls "This is the Burma Broadcasting Service." (Ridge-

way, South Africa)

Ceylon-Radio Ceylon, has strong signal 0100 with native vocal music; heard in English 0200. (Pearce, England) Still noted opening 2045 on 11 .-975. (Sanderson, Australia, others) This outlet normally closes 1145A but on Thursdays runs to 1215 closedown. (Fuller, R.I.) VOA relays are scheduled for 15.120 at 0730-0830 and on 11.975 at 1030-1100, both to India-Pakistan.

Chile—Punta Arenas, CE920, 9.200A. is heard with fair signal 2045; gives call 2100, closes 2200. CE1174, 11.74, Santiago, has very strong signal 2230 to close at 2400. Radio Mineria. 11.73. Santiago, is heard at 2300 to after 2330; gives call at 2300 and 2315; signal deteriorates after 2330. (Ridgeway. South Africa)

China-Radio Peking. 15.06V. noted with news 0400 and 0830, stronger 0400, (Pearce, England) Revised schedules for English periods from Radio Peking are 1730. 6.100, 7.500. 9.040. 10.260. 11.690. 15.060. 15.170; 0400. 10.260, 11.690, 15.060; 0830, 11.-690. 15.060. (N. Z. DX Times)

Colombia — Radiodifusora Nacional de Colombia en Bogota noted moved to 6.183 from 6.203. (Stark, Texas)

Curacao-PJC2, 5.010. Willemstad, noted at fair level with English session on Wednesdays 2000-2030. (Croston, Pa.)

Cuprus-Asharq-al-Adna, Limassol, noted 2255 on 6.790. 6.170. (Kary, Pa.)

Czechoslovakia-Prague is heard on 9.550 with Radio Moscow relay 1820-1930, with own program 1930-2030, and then resuming relay from Moscow; is directed to North America. (Grenell, Ohio) Has second period for North America at 2300. (Bellington, N.Y., others)

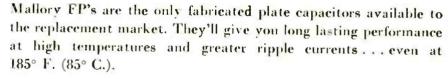
Denmark OZU, 7.26, relays Home Service on Mon. and Fri. 1315-1615, other days 1240-1615. OZF, 9.52. is



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